Seaman's Daily Affiftant new Modelled:

SHORT, EASY, AND PLAIN METHOD

OF KEEPING A

JOURNAL AT SEA.

IN WHICH ARE CONTAINED

for working the Cafes in Plane, Middle Latitude, and Mercator's Sailing. RULES

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RULES shewing how the allowances for Leeway, Variation, Heave of the Sea, set of Currents, &c. are to be made, and to correct the Dead-Reckoning by an Observation, in all Cases: And, also, all the TABLES that are any ways necessary for the Seaman's use in keeping a Journal.

RULES for finding the Latitude by the Meridian Altitude of the Sun, Moon, and Fixed Stars: And, also, the method of determining the Latitude by two Altitudes of the Sun, with the help of the Solar Tables,

A new Mercator's Chart of the Western Ocean. TO WHICH IS ADDED,

LATE TEACHER OF THE MATHEMATICS IN THE ROYAL NAVY. THOMAS HASELDEN.

SMYTH, MATHEMATICIAN. THE WHOLE REVISED

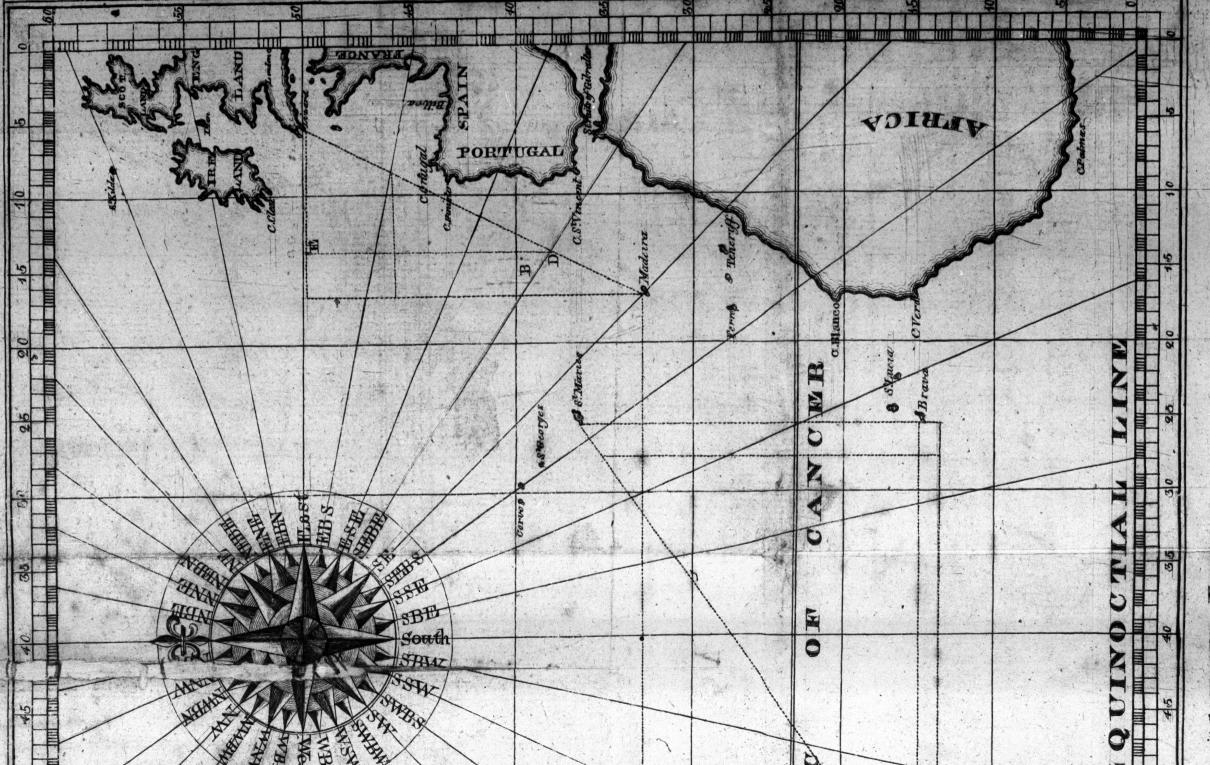
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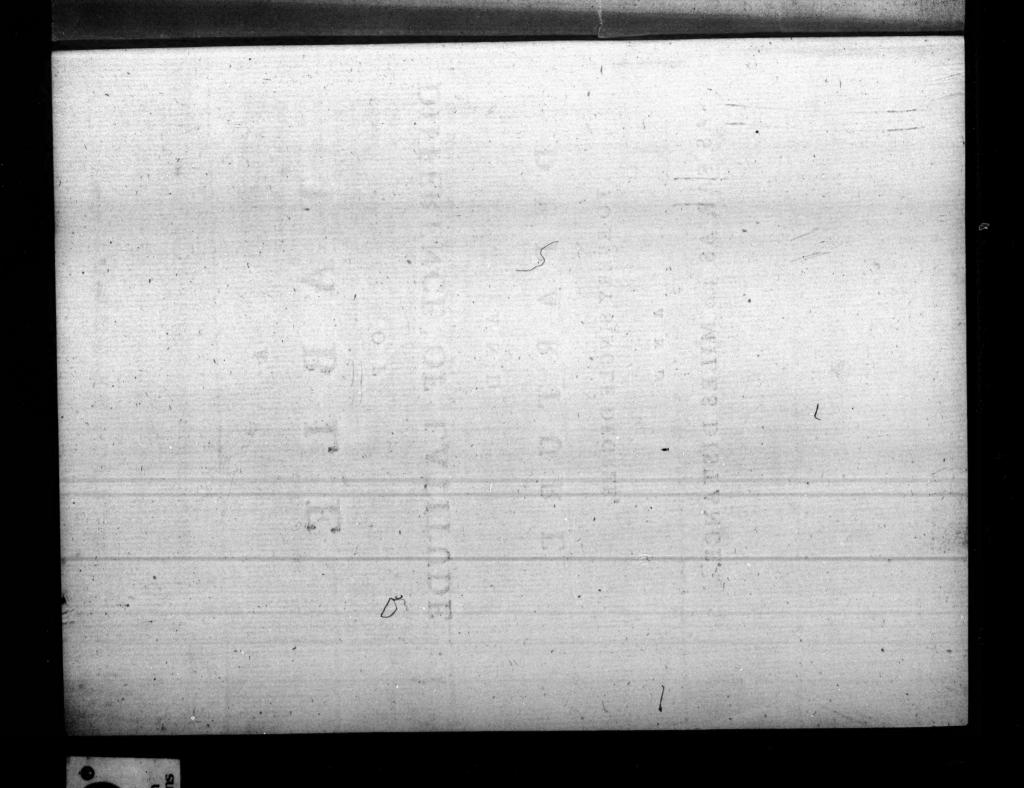
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AS FAR AS 300 MILES DISTANCE.



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eafy Rule) notwithstanding all the improvements that have been made Sun's Declination, which were become so very erroneous, that it was of the greatest importance, for the safety of men's lives and properties, that HE occasion of the Revisor being employed in improving and correcting the following pages, was on account of the innumeable errors that had crept into the Tables, and especially those of the they should be corrected; since, without accurate Tables of this kind, no mariner can, with certainty, determine his Latitude (at leaft by any for obtaining this important end. There are many useful things interspersed through the whole of this Affiltant which were not in any former edition, and fome things, of less importance, are lest out; so that the improvements of this edition are fo many, and fo obvious, that an enumeration of them would be unnecessary.

DIESEASOLTMEN

E A D E R.

ving, in the course of that time, made a general observation, that there are numbers of seamen who would gladly keep a Reckoning, had they any short, eafy, and plain method to do it by, but are dethat they have only got a fmattering of the theory, and a few terms of art by rote, which enable them to talk in fuch a manner as to de-HAVING been educated in the Theory of Navigation almost from my childhood, and having had about fixteen years experience of the practical part (at sea) both in the merchants' service, terred from it by the want of fuch a thing: And, also, that there are ceive those that go to learn of them; by having never been at sea, and also as teacher of the Mathematics in the Royal-Navy; and hamany who have thrown their money away to little or no purpose, by going to school to some Masters (of which sort there are too many) cannot know any thing of the practice. Therefore, for the use of fuch in particular, and of all other seamen in general, I have written the following Treatise, in which, I think, I have inserted all the Rules, and all the Tables, with their uses, that are necessary to be used in any Case at Sea: And also, particular Rules for keeping a Journal, with the manner of correcting the Dead-Reckoning, by an Observation, either for one Day, or for a longer Time; the first of which, viz. Correcting for one Day, has been treated of by several authors; but the latter, viz. Correcting for a longer time, I know has been barely mentioned in several, but none that I have read; and, for that reason, I have done it in the Journal at the latter end of this book, it being absolutely necessary not particularly explained in any author at all I believe, at leaft in for every man that keeps a Reckoning to know it, because they are

TO THE READER.

more likely to be out in their reckoning, when they have been fome days without an observation, than when they have one every day, and, consequently, more likely to have occasion to correct for three or four days, than for a fingle one.

and dividing, he will hardly be able to make any progress, either in arithmetic or navigation, by the help of books alone, without the af-fiftance of a mafter (fo that I think putting fuch things into books of this kind, ferves only to enhance the price, and is of no fervice to the duced me to publish this book (which I hope, and am pretty well affured, will be found the most useful book of its kind, now in print) for the daily practice at sea, I have nothing more to add, but to beg the readers' kind acceptance of my endeavours. I have not begun this book with arithmetic, as most of the books on this fubject do, because I think, that if any person has had so little education as not to be capable of adding, subtracting, multiplying

And am.

Their humble fervant,

THOMAS HASELDEN.

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CONTENTS THE

A table of numbers for the readier finding the course in the tables of difference of latitude and departure, when any two sides are given, page 46.

The use of the two foregoing tables in working the fix cases of plane failing, page Table of difference of latitude and departure to every fingle degree, and as far

The use of the tables of difference of latitude and departure in working a traverse,

page f.f.

To work any cafe in mercator, middle-latitude, parallel, or any right-angled plane triangle, page 53 and 54.

The first case of mercator (boing the most vierus case at the particularly explained,

A figure shewing how many points from the meridian any course steeredis, page 57.

A figure shewing how many points from the meridian any course steeredis, page 57.

A table of difference of latitude and departure to every 4 point, and to 300 miles

diffance, page 58 to 73.
Rules for flating the cafes in plane, middle-latitude, and mercator's failing, page 74.

A table of the moon's age, page 77 to 86.

To find the time of the moon's fouthing, and time of high-water, by the foregoing fable, page 87 to 99.

To find the fun's declination by the foregoing tables, page 97.

A table of the fun's right ascention, page 98.

A table of the right ascention and declination of some of the most noted fixed stars, The use of the table of times in finding the time of high-water, page 88. A table of times for finding the time of high-water, page 91. A table of the fun's declination to the year 1799, page 92. A table of the variation of the fun's declination for every 10 degrees, page 96.

page 99 and 100.

A table of the right afcention and declination of the crofiers, page 100.

The use of the tables of the sun and stars right ascension in finding what time any known flar will be upon the meridian on any given day, page 101.

To find the latitude by observation, page 102 to 106. A table of the refraction of the heavenly bodies, page 107.

To find the latitude by two altitudes, page 108 to 118.
A table for finding the latitude by two altitudes of the fun, page 119 to 126.
A table of corrections to be added to the moon's observed altitude, page 127. To find the latitude from the moon's meridian altitude, page 128 to 132.

To reduce degrees and minutes into time, page 132 and 133. A table of the latitudes and longitudes of places, page 134 to 141.

Rules for latitude and longitude, page 141 to 145.

A table of meridional parts, page 146 to 152.

A table of amplitudes, with its ule, page 153 to 161.

To find the fun's true amplitude by calculation, page 161 to 164.

To work an azimuth, with its ule, page 164 to 169.

Of the log line and half minute glafs, page 169.

Rules for finding the meridian diffance, page 174.

Rules for finding the dead-reckoning by an observation, page 175 to 178.

A journal of a voyage from England to Madeira, page 179 to 192.

How to prick off the place of the ship on the mercator's chart, page 192. To find the course or bearing from one place to another, page 193. To find the diffance of any two places in the chait, page 194 and 195.

Difference of Latitude and Departure for 1 Degree.

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10	03.00.2 53 54.9 023 7 03 101.9 05.3 52 151.8 08.0 03 202.7 10.6 53 251.6 03.00.2 53 54.9 023 7 101.9 05.4 54 153.8 08.0 03 202.7 10.6 53 251.6 03.00.2 54 53.9 023 8 03 102.9 05.4 54 153.8 08.0 03 202.7 10.7 54 253.6 03.00.2 54 53.9 023 8 03 102.9 05.4 54 153.8 08.0 03 202.7 10.7 54 253.6 03.00.2 55 55 55.9 02.9 05.8 03 102.9 05.4 54 153.8 08.0 03 205.7 10.7 54 253.6 05.0 00.3 55 55 55.9 02.9 106 105.9 05.5 55 154.8 08.2 06 205.7 10.8 25 55 55.5 05.0 00.3 55 55 55.9 02.9 106 105.9 05.5 55 154.8 08.3 08.2 206 205.7 10.8 25 55 55.6 05.0 00.3 55 55.9 02.9 106 105.9 05.6 55 15 15 15 15 10.9 10.8 10.8 10.8 10.8 10.8 10.8 10.8 10.8	03.0 00.1 53 55.9 03.7 10.1 10.0 0 95.4 53 151.8 08.0 03 20.7 10.5 53 13.5 0 03.0 00.2 53 54.9 02.8 04 103.9 05.4 53 154.8 08.0 03 20.7 10.5 53 13.5 0 03.0 00.2 54 53.9 02.8 04 103.9 05.4 54 153.8 08.1 04 203.7 10.7 54 23.5 0 03.0 00.2 54 53.9 02.8 04 103.9 05.4 54 153.8 08.1 05 204.7 10.7 54 23.5 0 05.0 00.3 56 55.9 02.9 02.8 04 103.9 05.5 156 155.8 08.2 206 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for 87 Degrees.

Difference of Latitude and Departure for 4 Degrees.

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04 103.8
03.0 106 105.7 07
07 106.7
1 00 108.7 07.5
NONTH 162
3 111 110.7
3 12 111.7
4 13.7
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6 116 115.7
7 17 110.7
or an annual service of
1400000000
.0 121 120.7
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12
2 24 123-7
19
1
4 28
6 20 126.7
7 32
33
.9. 34
5.0 130 135
06.1 38 137.
2 39
6.4 141 140.
6.4 42 141.
6.5 43 142.
06.6 44 143.7
6.6 45 144.
6.7 146 145.
6.8 47 I46.
06.8 48 147
-9 49
07.0 150 149.6
1000

for 86 Degrees.

Difference of Latitude and Departure for 5 Degrees.

100	100	1000		300				1600	Party.		SE CO	ALC: N	1	1000	Jones L	-	ALCOHOL:	4.55	LECUL	163/535	SERVICE S	A SHOOL	****	100				-	-		or southern al		-	-	-	455.10	2.1		201.00	460	100			40.00	-	-		10000	-
Dep	21.8	21.0	22.0	22.I	22.2	22.3	22.4	22.4	23.5	22.6	22.7	22.8	22.0	23.0	23.I	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.8	23.9	24.0	24.I	24.2	24.3	24.4	24.4	24.5	24.7	24.8	24.9	25.0	25.1	25.1	7.5.7	25.3	43.4	25.6	25.7	25.8	25.8	25.9	26.0	20.1	Lat
Lat	50.0	6.I.O	152.0	153.0	254.0	255.0	50.0	257.0	258.0	2,59.0	260.0	261.0	262.0	261.0	264.0	265.0	266.0	267.0	268.0	269.0	270.0	271.0	272.0	273.0	274.0	275.0	275-9	276.9	277.9	278.9	279.9	200.0	282.0	283.0	284.9	285.9	286.9	287.9	200.9	289.9	200.9	202.0	293.0	294.9	295.9	296.9	297.9	298.9	Dep
Diff	251 2	522	53 2	542	55 2		57	58	59	9	261				100,000,000				69	70	271	72	73	74	75	276	77	78	29	01	281	000			10	87	800		man Pine	291	7 60	04	9.5	296		00	-	300	Dit
Dep	17.5		17.7	17.7	17.8	17.9	18.0	18.1	18.3	18.3	18.4	18.4	18.5	18.6	18.7	18.8	18.9	19.0	19.1	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.7	19.8	19.9	20.0	20.1	20.7	20.0	20.4	20.5	20.6	20.7	20.8	40.7	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	41.0	Lat
Lat	00.1	201.2	202.2	203.2	204.2	05.5	2002	207.2	208.2	2.60%	110.2	11.2	112 2	113.2	114.2	15.2	2.917	217.2	118.2	119.2	120.2	121.2	2222	223.I	124.I	125.1	226.I	227.1	228.1	229-1	230.I	1,51.1	222.T	234.I	235.I	136.I	237.I	238.I	1,765	240.1	242.1	243.I	244.1	245.I	246.I	247.I	248.1	249.1	Dep
	201 2	02 2	03 2		05	6	reintaba?*	are lake	60	IO	211	12	13	142	IS	216	17	18	19	20	221	22	23	24	2.5	226	27	700	29		231	22	24	35	236	37	300		2	241	4.7	44	45	246	47	48	49	250	
Dep	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13-7	13.8	13.9	14.0	14.1	14.2	14.3	14.4	14.4	14.5	14.6	14.7	14.8	14.9	15.0	15.1	15.1	15.2	15.3	15.4	15.5	15.6	15:7	15.7	15.0	1.5.7	1.91	16.2	16.3	16.4	16.4	10.5	10.0	1.01	16.0	17.0	17.1	17.1	17.2	17.3	17.4	Lat
Lat	150.4	151.4	152.4	153.4	1544	155.4	156.4	157.4	158.4	159.4	160.4	161.4	162.4	163.4	164.4	165.4	166.4	167.4	168.4	169.4	170.4	171.3	172.3	173.3	174.3	175.3	176.3	177.3	178.3	179.8	180.3	182.2	182.2	184.3	185.3	186.3	187.3	188.3	109.3	190.3	191.3	IQ3.3	F94.3	195.3	196.3	197.2	198.2	199.2	Dep
	151	52	53	CHISPOS.	AND THE REAL PROPERTY.	156	57	20	59	-	Jones State	200		_	65	THE PERSON		and the same		Marie Control	171	13	73	_	75	-	77	ALC CORPORATE		8	181		30	8	186	87	000	60	3	191	7 6	0.40	9.5	1961	97	98	66	200	
Dep	08.8	08.0	0.60	0.60	1.60	2.60	09.3	09.4	09.5	9.60	09.7	09.7	8.60	6.60	10,01	Io.I	10.2	IO.3	10.4	10.4	10.5	9.01	10.7	10.8	10.9	11.0	11.0	II.I	11.2	611	11.4	71.6	11.7	11.7	11.8	11.9	12.0	12.1	77.7	12.3	12.4	12.5	12.6	12.7	12.8	12.9	13.0	13.1	Lat
	9.001	9.101	102.6	103.6	104.6	105.6	100.0	107.0	108.6	9.601	9.011	9.111	12.6	113.6	114.6	9.511	9.911	9.411	118.5	119.5	120.5	121.5	122.5	123.5	124.5	125.5	126.5	127.5	128.5	129.5	130.5	137.5	T 22.5	134.5	135.5	136.5	137.5	138.5	1.49.5	140.5	141.5	143.5	144.4	145 4	146.4	147.4	148.4	149.4	Dep
	IOI	02 1	03		05	Sweepand	and the same of the same of	anni ann	and the same	Io	III	121	Administration of the		15	116	17	_	161	20	25.2529	22	23	24	2.5	126	27	28	29		-	22	S DIRECTOR		136	-			41:	141	4 4 4 2	4	45	146	47	48	49	25	
Dep 1	4.4	34.5	9-40	24-7	8-40	6-40	05.0	1.50	05.1	2.50	05.3	05.4	05.5	05.6	05.7	05.8	05.8	05.0	0.90	1.90	2.90	06.3	06.4	06.5	00.5	9.90	2.90	9.90	6.00		07.1	01.0	7.70	07.4	07.5	02.0	07.7	07.0	0/2	02.0	0000	000	08.3	08.4	08.5	08.5	08.6	08.	I.at
Lat	50.8	8.1	2.8	53.8	\$4.8	200	20.0	27.0	200	29.8	8.09	8.19	00	00	8.4	11	7		_	2-69	70.7	71.7	72.7	73.7	74.7	75-7	76.7	77.7	78.7	1.67	2000	201.	82.7	84.7	85.7	86.7	87.7	88.7	7.60	90.7	9.20	03.6	94.6	95.6	9.96	92.6	986	0.66	Dep
	513	-	53	54	55	56	57	50	59.	9	19	62	63	64	65	99	67	89	69	70	71	72	73	74	7.5	94	77	78	100000	3	200	80%	200	8	86	87	∞ ∞	68	3	91	92	0.40	9.5	96	97	98	99	001	
Dep	1.00	00.2	00.3	00-3	90.4	00-5	9.00	00.7	00.00	6.00	0.10	0.10	01.1	01.2	01.3	01.4	01.5	01.6	01.7	01.7	8.10	01.0	07.0	02.I	02.2	02.3	02.4	02.4	02.5	02.0	02.7	0.70	0.20	03.1	03.1	03.2	03.3	03.4	3:	03.0	0000	Co. Committee	-	04.0	04.1	04.2	04.3	04.4	Lat
Lat	0.10	02.0	200	04.0	0.50	0.90	ASSESSED S	0.80	0.60	10.0	11.0	12.0	12.0	13.0	14.9	15.9	16.9	17.9	18.9	661	20.0	21.9	22.9	23.9	24.9	25.9	26.9	27.9	28.9	29.3	30.9	32.0	22.0	34.9	35.9	36.9	37.9	38.9	37.0	40.0	42.8	43.8	44.8	45.8	46.8	47.8	48.8	4400	Dep
DIE	1	- CONTRACTOR	3	CONTRACT OF	5	_				10	II	12	13	14	15	91	17	18	19	20	21	22	23	24	25	26	27	28	29	श	31	300	35	3.5	36	37	300	39	145	41	44	44	45	46	47	48	49	श	訓

for 85 Degrees.

Dep					- 1	20.8			27.2	200	\$05-355	27-4			27.7		27.9						200.5	28.0	20.7	280	29.1		200			29.0	29.7	20.0	30-0	30.1	30.2	30.3	30.4	30.5	30.7	30.8	30.0	31.0		31.2
Lat		250.6	251.6	252.6	253.0	254.6	255.0	450.0	257.0		259.0	20000	201.0	262.5	263.5	264.5	265.5	266.5	267.5	268.5	269.5	270.5	271.5	272.5	273.5	275.5	276.5	1000000		279.5			282.4	284.4	285.4		287.4	288.4	289.4	290.4	292.4	293.4	294.4	295.4	296.4	297.4
Dift	251		53	54	2	256	57	50	550		201	07	63	64	65	4	67	89	69	12	27I	72	-73	74	75	4/0	78	79	80	281	87	83	× × ×	286	87	80	89	워	291	92	2 4	95	296	97	98	99
Dep	2007	2I.I		21.3	21.4	21.5	21.0	41.7	0.1.0		22.0	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	23.0	23.1	23.2	23.3	23.4	23.5	2.2.7	23.8	23.9	24.0	24.1	24.2	24-3	24.5	24.7	24.8	24.9	25.0	25.1	25.2	25.4	25.	25.6	25.7	25.8	25.9	26.0
Lat	6-661	200.9	201.9	202.9	203.9	204.9	205.9	6.007	× × × × ×		209.0	210.6	211.8	212.8	213.8	214.8	215.8	210.8	217.8	218.8	219.8	220.8	221.8	222.0	223.0	225.8	226-7	227-7	228.7	229.7	230.7	231.7	232-7	234.7	235.7	236.7	237.7	238.7	239.7	241.7	242.7	243-7	244.6	245.6	246.6	247.6
Dift	20I	02	03	SIGP NAME	NAMES AND ADDRESS OF THE PERSON NAMES AND ADDRESS OF THE PERSO	Section 1	000	8 6	5 6				13	14	15	912	17	81 81	19		221	22	23	7.4		240	787	100 TOOLS	30	231		33	34	236	37	300	39	91	241	4 4 4 4 4	44	4.5	246	47	48	49
Dep	15.8	15.9	16.0	1.01	10.2	16.3	10.4	244	16.7	10 7	0.01	10.9	17.0	17.1	17.2	17.3	17.5	17.6	17.7			10.0	18.1	10.2	10.3	100	18.6	18.7	18.8	18.9	19.0	19.1	19.2	10.4	19.5	19.6	19.8	19:9	20.0	20.2	20.3	20.4	20.5	20.6	20.7	20.8
Lat	150.2	151.2	152.2	153.2	164.1	155.1	120.1	157.1	150.1		1001	101.1	102.1	163.1	164.1	165.1	1.991	167.1	1.891	109:1	170.1	171.1	172.0	173.0	174.0	176.0	177.0	178.0	0.641	180.0	181.0	182.0	183.0	186.0	186.0	187.0	188.0	189.0	6-681	190.9	192.0	193.9	194.9	195.9	6-961	197.9
Diff	ISI	52	-	54	5	156	50		200		and the same of					Character .					171	72	73			-	78		man Director			83	0 0 X	186	POSTER PROPERTY.	88	\$	श	161	92		95	196x	97	98	99
Dep	10.6	10.7	10.8	10.9	il.º	II.I	11.2	2	TT.	2	11.0	7.1.	0.11	6.11	12.0	12.1	12.2	12.3	12.4	12.5	12.0	12.7	12.9	13.0	13.5	12.3	13.4	13.5	13.6	13.7	13.8	13.9	14.0	14.2	14.3	14.4	14.5	14.0	14.7	14.0	15.0	15.2	15.3	15.4	15.5	15.0
Lat	100.4	IOI.4	102.4	103.4	104.4	105.4	100.4	407.4	100.4		110.4	111.4	112.4	113.4	114.4	115.4	116.4	117.4	118.3	119.3	120.3	121.3	122.3	123.3	24.3	126.2	127.3	128.3	129-3	130.3	131.3	132.3	133.3	135.3	136.2	137.2	138.2	139.2	140.2	141.2	143.2	144-2	145.2	146.2	147.2	148.2
Diff	IOI	Total Control	-	MAY SHOW			500		-	-		7 7	13	14		116	171			4000000	2000		23	7.4	125	27	28	29	30	131	32	33	34	136		38		4	141	44	4	45	146	47	48	49
Dep	05.3	05.4	05.5	05.0	05:7	05.0	0 4	3 4	06.3		4.00	200.5	0.00	00.7	80	6.90	02.0	07.1	2.70	67:3	27.4	07.5	02.0	07.7	0.70	08.0	08.1	08.3	8.4	08.5	08.0	00.0	0.00	100	1.60	09.2	09.3	89:4	00.5	0000	8.60	6.60	10.0	Io.I	10.2	10.3
Lat	50.7	51.7	52-7	7	54.7	55.7	50.7			No.	manager to	NAME OF THE OWNER, OWNE	-	63.6	0.40	65.6	999	02.0	0	OIV	20.07	- Alexandria	1100000	0 4	014	9.94	-	78.6	9.67	80.6	31.5	PERMIT	83.5	25.5	86.5	87.5	88.5	2000	30.5	91.5	03.5	94.5	95.5	96.5	97.5	98.5
Dift	SI	NAME OF TAXABLE	53	54	55	56		000			NAMES OF TAXABLE PARTY.	MANGRED	referende		5	99	67			2	71	72	73	74	75	77	700		80		85	033	200	86	87	000	60	श	91	2 2	0.4		96	97	98	99
Dep	1.00	00.2	00.3	4.00	8:5	00.0	00.7	3	01.0		1 5	5.10	01.4	01.5	01:0	01.7	0I.8	6.10	07.0	02.1	02.2	02-3	02.4	02.5	2 2	02.8	02.0	03.0	03.1	03.2	03.3	03.4	03.0	03.8	03.0	04.0	04.1	04.2	04-3	04.4	04.6	04.7	04.8	04.0	05.0	05.1
Lat	0.10	07.0	03.0	0.40	05.0	0.00	02.00	0 0		-			-	-								0	-	23.9	25.0	26.0	000	28.8	29.8	30.8	31.8	32.0	33.0	35.8	36.8	37.8	3000	39.0	40.0	2 00	43.8	44.8	45.7	46.7	47.7	48.7
Diff	I	7	3	4	2	0	0		To			77	13	1	15	91	17	Action 2010		2	21	22	23	77	الراج	27	78	29	30	31	32	33	34	36	37	38	39	9	41	42	44	45	46		48	49

for 84 Degrees.

	9	7	.00	0	0	1 12	~	2 4		2.7	7	20	0	0		3	1		200	00	0	10	1	7	4	8	9	7	6	0	H	7	33	50	0 1	Va	0	H	7	3	4	5	70	00	0	0	7 11	4	3	B
Dep	30.	30.	30.8	30.	31.	31.	31.	31.	21.		3	31.	31.	32.0	32.	32.	32.	12.	32.	32.	32.0	33.0	33.	33.	33.	33.	33.	33.	33.	34.	34.	34.	34.	34.	34.	34.	34.	35.	35.	35.	35.	35.	35.	35.	35.	36.	36.	36.	36.	1
lat lat	16.I	1.0	251.I	252.I	253.I	4.1	1:3	256.1	257.I	. ~	:	250.0	260.0	261.0	262.0	263.0	64.0	6.0	0.0	267.0	8.0	0.6	0.0	1.0	6.1	2.9	3.9	4.9	5.9	6.9	7.3	6.8	6.6	6.0	6.1	,	, 4 , 00	200	286.8	87.8	×. ×. ×.	289-8	290-8	291.8	2.8	3.6	0 00	296.8	97.8	200
	77	25					255	.4	2,0	3 6	श			50	126	76	26	4	126	126	268		7	27	127	27	27	127	27	27	31	127	127	75	2 7	100	1 24	3 28	28	0 287	37	728	3 29	25	262	57	8 20	9 20	70	15
اةً	251	52	53	2	55	256	Ü	200	, 2	ŝ	3	261	62	63	9	65	266	67	68	9	70	271	7	7	7.	7.5	276	77	78	75	∞ 	281	~ ~	× 0	000	9	00	· 80	8	6	291	92	9		9	29	90	0	300	1
Dep	4.5	24.6	4.7	24.8	5.0	.5.I	25.2	25.3	25.4	9		5-7	25.8	15.9	26.1	26.2	6.3	6.4	26.5	16.7	26.8	6.93	27.0	17.2	27.3	27.4	27.5	27.6	27.8	6.2	0.8	1.87	28.3	4.00	20.5	28.7	28.9	29.0	29.1	29.2	29.3	29.5	29.6	29.7	29.0	29.9	30.2	30.3	30.4	١,
	(8'5'A			1016	2	1 20								4	4		7	7				3.1	3	3	3	3	3	3	3	3	(C)	3	23	8	7 0	110	1 6	7	7	71	7	7	7	2	12	н .	1 14	1	н	
Lat	199.5	200.5	201.5	202.5	203.5	:04.5	205.4	206.4	.07.	208.	000	7-601	210.4	III.	212.	213.4	14.	214.	216.	217.4	218.	.61	.20	22I.	222.	223.	224.	225.	226.	127.	228.	229.	430	231.	232.	200	235	236.	237.	238.	239.	240.	241.	242	243	244.	246	247	248.	1
-	OI	02	03	esanove.	05	-	07	24	Marketon	100	31	II	12	13	14	15	16		18	19	20,	221 2	22	23	24	25	26	27	200	29	30	31	32	33	34	3	37	38	39	40	141	43	43	4	45	246	48	49	250	ļ
الم	4.	.5	9.	.7	6.	0	7.	4	4	1	3	0.	.7	∞.	0	H,	.2	.3		9.	.7	100000		H.	.7	•3	4.	9.		200	8	0	7	3	4 .	21.	-00	6.	0	7:	•3	4	5,	0	7	6	1	64	1-3	1
Dep	18.4	18	18	18.7	81.	19.0	1.01	19.2	IO.4	101	3	61	19.7	61	20.0	20.	20.2	20	20	20	20.7	20.8	20	21	21	21.	21.	21.6	21	21	21.	22.	22.	22	22.	00	77	22	23.0	23	23.	23	23.	23	2	23.	27	7	à	1
at	6-0	150.9	F.9	152.8	153.8	154.8	155.8	156.8	2.8	200	000	159.8	0.0	161.8	162.8	163.8	164.8	165.7	166.7	167.7	8.7	9.7	0.7	1.7	2.7	3.7	4.7	5.7	6.3	7.7	8.7	179.6	180.6	181.0	182.0	18.4	4.6	186.6	187.6	188.6	189.6	190.6	9.161	192.5	193.5	194.5	195.5	197.5	198.5	
Tona Control	California	Cartificonta	DATE WHEN	PORTOR	-	15	I	H				1000000	ATT POST OF	COLUMN TO SERVICE		-	-			-	-	169.		17	172.	173.	17	17	_	177								18	18	MILES COMPA	18	5	61 8	61	<u>81</u>	61 6	2 19	51 6	0110	1
	ISI	52	53	54	55	156	, ,	200	202	200	31	191	62	63	64	65	166	67	89	69	70	171	72	7.3	74	75	176	77	78	79	8	181		800	0.4	184	00	8	8	8	191	92	6	9	6	19	ە «	0	200	1
Dep	12.3	12.4	12.5	2.7	12.8	12.0	2.0	12.1	2.2	0.01	3.4	3.5	3.6	3.7	13.0	14.0	4.I	14.2	14.4	4.5	14.6	14.7	14.0	0	15.1	5-2	15.3	5.5	5.6	15.7	5.8	0.9	1.91	16.2	16.3	0.5	16.7	8.91	6.91	7.1	7.2	17.3	17.4	17.5	7.7	7.8	2.0	8.1	18.3	1
88.		Helph,			185.5	20.9	Since	400			1			200							19 30	-				20.00		SHE	300	2 1						1		0.			_					_	~ (-	ļ
Lat	100.2	01.2	102.2	103.2	104.2	105.2	106.2	107.2	108.2		109:2	110.2	III.2	112.2	II3.I	114.1	III	116.1	117.1	118.1	119.1	120.1	121.I	122.I	123.1	124.1	125.1	126.0	127.0	128.0	129.0	130.0	131.0	132.0	133.0	34.5	35.0	37.0	-00	139.0	39.9	140.9	41.6	142.9	43.	44.	45	47.	48.	١
		02 1		04	and the same of	15/20/19A/A		de la constitución	-	-			IZ I	I3 I		1 5	1911		181		20 I			-		25 I	-			1 62	OR PERSONAL PROPERTY.	31 1			4 I	5	0 1	28 I	1 68	DESCRIPTION OF THE PERSON NAMED IN	H	12 I	13 1	14	1	1 9 t	, ×	40	20,7	İ
	IOI		83.	0	0	12	-	, 0		, ,	1	7					1,000	200			-	12	-		-	"	12	u	~	~	63	13		9.00				, it		B	1	7	~	7	71	T Y	0.0		H 2	1
Dep	06.2	06.3	26.5	9.90	2.90	8.90	0.90	07.1			97:3	07.4	07.5	07.7	07.0	07.0	0.80	000	08.2	28.4	80	08.6	8.80	08.0	0000	1.60	99.3	9.4	09.5	9.60	09.7	6.60	10.0	IOI	10.2		10.5	OH	10.8	11.0	H	11.2	11.	11.5	11.6	1	11.	12.1	12.2	1
Lat	50.6	9	2.6	53.6	4.6	6.6	6.6	7.6	28.6		01	60.5					92.50	9		68.5			71.5	2.5	4	-	4	6.4		-	79.4	80.4	4	4	83.4	4:4	86.2	87.3	88.3	89.3	90.3	91.3	92.3	93.3	94.3	95.3	903	08.3	99.3	
	315		535			\$65	244	,00	200	27		9 19	62 6	63 6	64 6	65 6	999			9 09	70 6	11	727	73	747	75/	767	77 3		797			87		84	95	87	88	89	90	916	92	93	2	95	96	97	000	00	
-		7	4		9	1	. 0	. 0	-	1 6	1		5	9	7	-00	10	H	1 7	4	4	19	7	.00	0	0	14	3	4	5	7	00	6	0	Η (्रा	+ ~	200	00	6	0	H.	R	4	15.	0	~ oc	0	H.	-
Dep	00	8	8	8	00	8	0	OIO	10	1	5	OI.	01.5	01.6	oi.	oI.	oi.	02	03	02.	07.	02	02.	02.	02.	03.0	03.	03.	03.4	03.5	3	03.8		9	40	3 3	4 4	9	9	9	05	05	50	S	8	05	200	9	1.90	1
Lat	0.10	0.70	03.0	04.0	5.0	0.90	0.90	07.0	000		6-60	6.01	611	12.9	13.0	14.0	100	6.0	17.0	8.0	19.0	0.0	8.I.	22.8	23.8	24.8	25.8	8.92	27.8	000	8.62	30.8	31.8	37.8	33.7	24:7	26.7	37.7	38.7	39-7	40.7	41.7	42.7	43.7	44.7	45.7	47.6	48.6	46.6	-
世	10	4	Name and Address	name of the	5	100	and the last	- 00	6			II	12	13	141	ICI	191	17	181	IOI		212	22	23	242	25	26	27	200	29	30	31	32	33	34	3	27	300	39	40	41	42	43	44	45	40	4×	49	50	Ì

for 83 Degrees.

								1		Contract Con			nesent.							Caki		40.00	1.000	100	2	-	1				1000		a bisson	200					-							and the		-00	1	-
Dep	34.9	35.I	35.2	35.4	35.5	35.0	35.8	35.9	30.1	36.2	36.3	36-5	36.6	36.7	36.9	37.0	37.2	37-3	37.4	37.6	37.7	37-9	38.0	38.1	38.3	38.4	38.6	38.7	300	39.0	39.1	39.3	39.4	30.7	30.8	40.0	40.I	40.2	40.4	40.5	40.6	40.8	40.0	41.1	41.2	4	41.6	41.8	Lat	
200220	248.6	249.6	250.5	251.5	252.5	15.3.5	154.5	155.5	150.5	257.5	258.5	259.5	260.4	261.4	262.4	262.4	V V V	265.4	266.4	267.4	268.4	269.4	3704	271.3	272.3	273.3	274.3	275-3	276.3	277-3	278.3	279.3	200.3	282.0	282.2	284.2	285.2	286.2	287.2	288.2	289.2	20002	291.1	292.I	293.I	294.I	206.1	297.1	Dep	
Diff	251 2		53 2		201	505	572	50	59	01	261		63	_	65	266	67	89	69	70	271	72	73	74	75	276	77	78	200	8			000	* ×	286	87	88	89	9	291	92	93	94	95	290	700	90	300	Dig	
Dep I	0	28.I	28.3	28.4	28.5	28.7	20.00	29.0	29.1	20.2	29.4	29.5	20.6	20.8	29.0	30.1	30.2	30.3	30.5	30.6	30.8	30.9	31.0	31.2	31.3	31.5	31.6	31.7	31.9	32.0	32.2	32.3	22.6	32.7	32.9	33.0	33.1	33.3	33.4	33.5	33-7	33.0	34.0	34.1	34.2	24.4	34.7	34.8	Lat	
Lat	1.661	20000								208.0	209.0		2 IO.0			213.0	214.0	215.0	6.91	6.71	6.81	8.617	220.8	8717	222.8	223.8	224.8	225.8	226.8	0.67.7	220.0	229.7	430.7	232.7	233.7	234.7	235-7	236.7	237.7	238.7	239-7	240.0	241.0	242.0	243.0	244-0	246.6	247.6	Dep	1
0000	and the same of	AND DESCRIPTION	Name and Address of the Owner, where	777 DVEC	FOTOY SUB	(429/230)		Minne		10	2112	12 2	132	142	15 2	216	17	18	19	20	22I	22		24	2.5	226	27	28	29	श्री :	231	35	200	3,7	236	37	38	39	40	241	42	43	44	45	240	47	40	3 250	Did	
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grade.	49.5	1200	25	10	153.5	54.5	2		157.5	58.4	1.59.4	160.4	161.4	162.4	163.4	164.4	165.4	166.4	167.4	168.4	169.3	170.3	1713	172.3	173.3	174.3	175.3	176.3	177.3	170.3	179.2	180.2	101.2	182.2	184.2	185.2	186.2	187.2	188.2	189.1	190.1	191.1	192.1	193.1	194.1	195.1	107.1	UCABBETTEN	THE PERSON NAMED IN	
	ISI		53 I			1201	57	Name and	59	MARKET !	161	MINERAL PROPERTY.	63			166	HARD PLANS	122-12-12	69	70	171	enter Para	73	74	75	176	77		79	STORE THE	181	0 22	000			87	88	89	90	161					196	200	8	u	Dia	
	I4.F		14.3	14.5	14.0	14.0	14.9	15.0	15.2	15.3	15.5	15.6	15.7	15.0	16.0	16.1	16.3	16.4	9.91	16.7	8.91	17.0	17.1	17.3	17.4	17.5	17.7	17.8	18.0	1001	10.2	16.4	18.7	18.8	18.9	1.61	19.2	19.3	19.5	19.6	19.8	19.9	20.0	20.2	20.3	30.5	20.	20.9	Lat	
Lat	0000		102.0					9	107.9		455							116.0		8.811	9980	120.8	8.121	122.8	123.8	124.8	125.8	126.8	127.7	120.7	129.7	130-7	131.7	122.7	I34.7	135.7	136.7	137.7	138.6	139.6	140.6	141.6	142.0	143.0	144.0	145.0	147.6	4	Dep	
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Lat	50.5	51.5	54.5	53.5	54.5	55.5		ed-	58.4	59.4	\$0.00	4	4	- 4	- Auditor	65.4	66.4	67.3	68.3	69.3	70.3	71.3	72.3	73.3	74.3	75.3	76.3	77.2			200	81.2	2.70	84.2	86.2	86.2	87.1	88.1	89.1	90.1	1.16	92.1	93.1	194	95.1	900	080		Der	
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for 82 Degrees.

Difference of Latitude and Departure for 9 Degrees. 9

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 | 41.1 | 41.3 | 41.4 | 41.6 | 41.8 | 41.9 | 42.1
 | 42.2 | 42.4 | 42.5 | 42.7 | 42.9 | 43.0
 | 43.2 | 43.3 | 43.5 | 43.6 | 43.0 | 43.9
 | 44.1 | 44.5 | 44.6 | 44.7 | 44.9 | 45.0 | 45.2 | 45.4
 | 45.5
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 | 45.8 | 46.0 | 46.1 | 46.3 | 40.5 | 46.8 | 46.9
 | Lat | 1 |
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 | 259.0 | 2000 | 201.7 | 262.7 | 263.7 | 164.7 | 265.7
 | 266.7 | 267.7 | 268.7 | 269.6 | 270.6 | 271.6
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 | 270.5 | 280.0 | 281.5 | 282.5 | 283.5 | 284-5 | 285.4 | 286.4
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 | 34.4 | 34.6 | 34.7 | 34.9 | 35.0 | 35.2
 | 35.3 | 35-5 | 35-7 | 35.8 | 30.0 | 30.1
 | 30.3 | 36.6 | 36.8 | 36.9 | 37.1 | 37.2 | 37.4 | 37.5
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ISON ST ST ISON ST | OLY ONE ST 50-4 OR ONE | OLIO COLOR \$1504 \$8.0 \$10.4 \$8.5 \$10.4 \$1.5 | OLOS STROW SEC TOI 99.8 IS BIN 149.1 23.6 201 198.5 31.4 35. 244.9 OLOS STROW SEC TOI 99.8 IS BIN 149.1 23.6 201 199.5 31.6 32 44.9 OLOS STROW SEC TO TOO TO THE STROW SEC TO TOO. TO THE STROW SEC TOO. TO TO. TO TOO. TO TO TOO. TO TO TO TO TOO. TO | OLOS STROWS OF TOTORY 160. \$2 190 199.8 \$1 \cdot 8 190 199.8 \$1 \cdot 8 190 190.8 \$1 \cdot 8 190.8 | OLO 00.2 \$1 \$0.4 0.8.0 \$1 \$0.8 \$ \$15.4 \$0.8.0 \$1 \$0.8 \$0.8 \$0.8.0 \$1 \$0.8 \$0.8 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$15.4 \$0.8.0 \$2 \$10.7 \$10.7 \$10.1 \$1.2 \$1.2 \$1.0 \$1.0 \$1.0 \$1.0 \$1.0 \$1.0 \$1.0 \$1.0 | OLO 00.00. \$150.40. \$150.40.00. < | OLO GOAR 1 50-40 & S. (18 19.8 15 149.1 23.6 20 199.5 31.6 52 245.0 23.0 23.2 23.2 24.9 23.0 23.2 2 | OLO GOA B 11 SOA4 0& 0 12 SOA 0& 0 13 SOA 0 13 SOA 0 13 SOA 0 14 SOA 0 14 SOA 0 15 SOA 0 | Q10 Q10 Q11 Q10 Q11 Q11 <td>Q10 Q20 Q20<td>Q10 Q20 Q20<td>00.00.00.00.00.00.00.00.00.00.00.00.00.</td><td>OCKOO N. S. STAM ONLOW N. S. /td><td>Octo St 1504 St 1007 1008 R.S. R.S.</td><td>Oncolor of St 15046 Oncolor of St 15047 Oncolor of St 15047</td><td>03.0 00.0 2 1 1 20.4 0.6 0 10 1 99.8 15.8 15.1 14.9 1 23.0 0 1 199.5 11.4 35.1 23.0 199.0 0.0 0.0 0.0 0.0 0.0 1 1 20.0 0.0 1 19.0 1 19.0 0.0 0.0 0.0 0.0 0.0 1 19.0 0.0 1 19.0 0.0 0.0 0.0 0.0 0.0 0.0 1 19.0 0.0 1 19.0 0.0 0.0 0.0 0.0 0.0 1 19.0 0.0 1 19.0 0.0 0.0 0.0 0.0 0.0 1 19.0 0.0 1 19.0 0.0 0.0 0.0 0.0 1 19.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0</td><td>03.0 00.0 3 3 3 4 0 0 3 0 3 0 3 0 3 0 0</td><td>010 0004 [11504 08] [101 998] [15, 815, 114, 11 32, 001 1995] [114 351 3479] [114 351 3479] [115 084 08] [115</td><td>04.0 00.0 11 15 0.0 0.0 10 10 10 10 10 10</td><td>Octo 512-50-8 50-10-10 99-8 15.8 15.4 15.4 20.1 99-8 15.8 15.4 15.4 20.2 10.0 31.4
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[115 084 08] [115 | 04.0 00.0 11 15 0.0 0.0 10 10 10 10 10 10 | Octo 512-50-8 50-10-10 99-8 15.8 15.4 15.4 20.1 99-8 15.8 15.4 15.4 20.2 10.0 31.4 |

for 81 Degrees.

10 Difference of Latitude and Departure for 10 Degrees.

Dep	43.5	43.7	43.9	44.0		44.4	44.6	44.7	44.9	45.I		he east	The state of	2	46.0	46.1	16.0	46.5	46.6	46.8	17.0	47.2	47.3	47.5	47-7	47.9	48.0	48.2	48.4	48.6	48.7	48.9	49.I	49.4	404	40.8				50.5	50.6	50.8	51.0	51.2	5 I.3	51.5	% I.8	toric y	
Lat	247.2	248.2	240.2	2 CO. I	25 I.I	252.1	253.I	254.1	255.I	256.0	257.0	2.8.0	2.60.0	2000	of T.	262.0	0 690	262.0	264.0	265.0	266.0	267.0	268.8	269.8	270.8	271.8	272.8	273.8	274.8	275-7	276.7	277.7	278.7	280.4	281	282.6	283.6	284.6	285.6	286.6	287.6	288.5	289.5	290.5	291.5	202.5	294.5		
	241		53		55	256	57	58	39	9	261					366	44			70	DP4600A	72	73	7.4	7.5	276	77	78	79		201	0 00	63		10	-	00	89		191	92	93	6	95	4	200		B	
	34.9	15.0	35.2	35.4	35.5	35.7	35.9	36.1	36.2	36.4	26.6	16.8	26.0	27.1	27.2	27.6	27.6	27.8	38.0	18.I	28.2	38.5	38.7	38.0	39.0	39.2	39.4	39.5	39.7	39.9	40.I	40.2	40.4	5 6	199	41.1	4I.3	41.4	4I.6	41.8	42.0	42.1	42-3	42.5	42.7	42.0	43.2	43.4	1
Lat	197.9	198.0	199.0	200.0	201.9	202.9	203.9	204.8	205-8	206.8	207.8	208.8	200.8	210.7	211.7	212.7	212.7	214.7	214.7	216.7	217.6	218.6	219.6	220.6	22I.6	322.6	223.5	224.5	225.5	220.5	227.5	226.5	229.5	22I.A	222.4	233.4	234.4	235-4	236.3	237.3	438.3	239.3	240.3	241.3	242.3	244.2	345.2	246.2	
	20I	02						80	60	IO	211	12	12	2.5	1	216		18							2.5				-	ကျ		32		34	2		-00			241	42	43	44	45	245	4 4	49	250	S
	26.2	26.4	26.5	26.7	26.9	27.I	27.2	27.4	27.6	27.7	27.0	28.1	28.2	28.2	28.6	28.8	20.0	20.1	20.2	20.0	20.7	20.8	30.0	30.2	30.3	30.5	30.7	30.9	31.0	31.2	31.4	31.0	31.7	32.1	22.2	22.4	32.6	32.8	32.9	33.1	33.3	33.5	33.6	33.8	97 TSA	34.4	34.5	34.7	Charles Charles
Tat	148.7	140.7	150.7	141.7	152.6	153.6	154.6	155.6	136.6	157.6	148.6	150.C	160.5	161.6	162.6	162.5	164.6	164.4	166.4	167.4	168.4	169.4	170.4	171.4	172.3	173-3	14.3	175.3	176-3	177.3	178.2	179.2	187.2	182.2	182.2	184.2	185.1	186.1	187.I	1881	189.1	1.061	191.0	192.0	193.0	105.0	196.0	197.0	The second second second
3	ISI		Na Stranstern	4	3	156	57	581	59		161	Marine Control	Data market	2 4		-		689		707	1 -	2	73	4	7.5	176	77	20					83		NIV		88	89		191	92	93	94	95	196	> °	96	4	
250	17.5	17.7	17.9	18.0	18.2	18.4	18.6	18.7	18.9	1.61	19.2	10.4	10.6	10.8	10.0	20.1	20.2	20.5	20.6	20.8	21.0	21.2	2I.3	21.5	21.7	21.8	22.0	22-2	22-4	22.5	22.7	22.9	4301	22.4	22.6	23.8	23.9	24.1	24.3	24.4	24.6	24.8	25.0	15.	25.3	26.7	25.8	26.0	
Tat	99.5	100.4	IOI.4	102.4	103.4	104.4	105.4	106.4	107.3	108.3	100.3	110.1	III.2	II2.2	IF2.2	114.2	II C.2	116.2	117.2	118.2	119.2	120.I	121.I	122.I	123.I	124.1	125.1	126.1	127.0	128.0	129.0	130.0	131.0	122.0	122.0	134.0	135.9	136.9	137.9	138.9	139.8	140.8	141.8	142.8	143.8	144.0	146.7	147.7	Same Contract
	IOI	0.2	-		-				60	10	H	****	I	17	J.E	116	day recent		IO					24	25	126	27			-			33		126		Department in	39	40	141	42	43	4 4	45)	140	4 2		H	82
Dep	08.8	0.00	00.0	7.60	09.5	200-7	6.60	IO.I	10.2	10.4	9.0I	10.8	10.0	1	11.2	11.4	971	11.8	12.0	I2.I	12.3	12.5	12.7	12.8	13.0	13.2	13.4	13.5	13.7	13.9	14.0	14-2	14.4	14.7	14.0	IS	15.3	15.4	15.6	15.8	16.0	1.91	10.3	10.5	10.0	7 7 0	17.2	17.3	
Lat	50.2	CI.2				55.1	56.1	57.I	58.I	59.I	1.09	9			64.0	65.0	66.0					70.0	71.9	72.9	73.9	74.8	75.8	-	77.8	78.8		000	201.7	82.7	100	85.7	00		88.6	89.6		6	0		94.5	2.90		9	
	IS		7.3		NE S	56	*	38	59	and -	19	62	62	2	9	99	6.9				11			74	7.5	16	77	78	29				003	0 00	8	8	88	89	90	16	92	93	9	25	0	780	20	H	Se proposed
Dep	00.2	00.2	00	0	0	0.10	01.2	P-FO	01.6	OI.8	0.10	02.1	02.2	02.4	02.6	02.8	Billion Co.	03.1	03.3	03.5	03.6	03.8	04.0	04.2	04.3	04.5	04.7	2.5	05.0	3	05.4	05.5	05.7	200	90	90	9.90	999	06.9	07.1	07.3	The state of	07.0	6	0000	No common			
Lat	01.0	02.0	03.0	03.0	04.0	05.9	6.90	07.9	08.9	6.60	10.8	11.8	12.8	12.8	14.8	15.8	16.7	17.7	18.7	19.7	20.7	21.7	22.6	23.6	24.6	25.6	26.6	27.6	28.6	29.5	30.5	31.5	32.5	33.5	25.5	26.4	37.4	38.4	39.4	40.4	41.4	42.3	43.3	41	4 ;	40.5			
5	F	2		7	5	9	1	00	6	IO	H	12	IZ	14	IK	191	17	18	OI	20	21	22	23	24	25	26	27	50	29	워	31	32	33	34	श्र	200	38	39	40	41	42	43	44	45	46	47	40	50	

for 80 Degrees.

Difference of Latitude and Departure for 11 Degrees. 11

Did	Lat	Dep	Diff	Lat	Dep	Diff	Lat	Dep	Did	Lat	Dep	Dia	Lat	Dep	Dift	Lat	Dep
1	010	00.3	51	50.1	7-60	IOI	1.66	19-3	Mary Street	148.2	28.8	100 100 100	197-3	38.4	251	246.4	47.9
a	03.0	4.00	52	\$1.0	6-60	00	1001	2.61	52	149.2	29.0	08	198.3	38.5	52	247.4	48.1
3	02.9	9.00	53	52.0	IOI	03	IOI.I	I9.7		150.2	29.8	63	109.3	38.7	53	248.3	40.3
4	03.9	00.8	54	53.0	10.3	8	102.1	19.8	54	151.2	29-4	8	20002	38.9	54	249.3	48.5
5	04.0	0.10	55	54.0	10.5	8	103.1	20.0	55	152.1	29.6	95	20I.2	39.1	53	250.3	48.7
9	05.0	oI.I	56	55.0	10.7	901	104.0	20.2	1.56	153.I	29.8	300	20202	39-3	256	251.3	48.8
7	6.90	01.3	37	56.0	10.9	07	9000	20.4	57	154.I	30.0	07	203.2	39.5	57	252.3	46.0
00	6-10	OI-5	58	26.9	II.I	80	1	20.6	58	155.1	30.1	8	204-2	39-7	58	253.2	49-2
6	8.80	01.7	59	57.9	11.3	8	SE-803	20.8	39	156.1	30.3	6	205-2	39-9	29	254.2	49.4
IO	8.60	OI.9	9	58.9	11.4	S)	108.0	21.0	8	157.1	30.5	S	206.I	40.1	8	255.2	49.6
11	IO.8	02.I	19	59.9	11.6	III	0.601	21.2	191	158,0	30.7	211	107.I	40-3	SERVICE TO	256.2	49.8
12	11.8	02.3	62	6009	11.8	12	109.9	21.4	62	159.0	30.9	12	208.I	40.4	62	257.2	50.0
13	12.8	02.5	63	61.8	12.0	13	110.9	21.6	63	160,0	31.1	13	209.I	40.6	63	258.2	50.2
14	13.7	02.7	64	62.8	12.2	14	111.9	21.8	64	161.0	31.3	14	LOIT	40.8	64	259.I	50.4
15	14.7	02.6	65	63.8	12.4	15	112.9	21.9	65	162.0	31.5	15	211.0	41.0	65	260.I	50.6
91	13	03.1	99	64.8	12.6	911	113.9	22.I	166	162.9	31.7	216	212.0	41.2	266	261.1	50.8
17	16.7	03.2	67	65.8	12.8	17	114.8		67	163.9	31.9	17	213.0	41.4	67	262.1	50.0
18	17.7	03-4	89	66.7	13.0	. SI	115.8			164.9	32.1	18	214.0	41.6	89	263.1	31.1
19	18.7	03.6	69	67.7	13.2	61	8.911	855 W	69		32.2	61	215.0	41.8	69	264.0	51.3
20	19.6	03.8	20	68.7	13.4	20	117.8	22.9		91	32.4	20	215.9	42.0	70	265.0	51.5
2.1	20.6	04.0	71	69.7	13.5	121	118.8	23.1	171	167.9	32.6	22I	216.9	42.2	271	266.0	51.7
22	21.6	04.2	72	70.7	13-7	22	8.611	23.3	72	168.8	Yes i	22	217.9	42.4	72	267.0	51.9
23	22.6	04.4	73	71.7	13.9	23	120.7	23.5	73	169.8		23	2.18.9	42.5	73	268.0	52.1
24	23.5	04.6	74	72.7	14.1	24	121.7	23.7	7	170.8		24	219.9	42.7	74	269.0	52.3
25	24.5	04.8	75	73.6	14.3	2.5	122.7	23.9	75	171.8	33.4	25	220.9	42.9	7.5	269.9	52.5
26	25.5	05.0	76	74.6	14.5	126	123.7	24.0	176	172.8	33.6	226	221.8	43.1	276	270.9	52.7
27	26.5	05.2	77	75.6	14.7	27	124-7	24.2	27	173.7	33.8	27	222.8	43.3	77	271.9	52.9
100	27.5	05.3	78	26.6	14.9	500	125.6	24.4	78	174.7	34.0	5	223.8	43.5	78	272.9	53.0
29	28.5	05.5	79	77.5	15.1	2,9	126.6	24.6	7	175-7	34.2		224.8	43.7	7.9	273.9	53.2
워	29.4	05.7	8	78.5	15.3	39	127.6	24.8	402203.13	170.7	34-3		225.8	43.9	8	274.8	53.4
31	30.4	05.0	81	79.5	15.5	131	128.6	25.0	H	177.	34.5	231	226.7	44.1	281	275.8	53.6
32	31.4	1.90	000	80.5	15.6	32	129.6	25.2			34.7	32	227.7	44.3	87	276.8	53.0
33	32.4	06.3	63	81.5	15.8	33	130.6	25-4		179.		33	228.7	44.5	83	277.8	54.0
34	33.4	00.5	× ×	82.5	16.0	34	131.5	25.0			35.I	34	229.7	44.0	× 0	278.8	54.2
35	34.4	00.7	100	03.4	10.2	35	132.5	25.0	0	74 B	35.3	35	230.7	44.0	05	279.8	54.4
36	35.3	6.00	98	84.4	10.4	130	133.5	26.0	180	182.0	35.5	230	231.7	45.0	286	280.7	54-0
37	30.3	07.1	00	05.4	0.01	37	134-5	20.I	000	103.0	35-7	37	232.0	45.2	87	281.7	54.0
200	2000	2	0 0	87.4	0 0	300	156.4	2.07	0 00	185	35.7	300	233.0	45.4	0 0	180 2	25.0
40	20.2	07.6	9 0	88	17.2	7 0	127.4	26.7	00	186.	26.2	200	225.6	45.8		286.7	55.3
41	40.2	07.8	10	80.2	17.4	141	128.4	26.0	101	187.5	36.4	747	2.26.6	46.0	201	285.6	25.5
42	41.2	080	02	900	17.6	42	130.4	27.1	02	188.5	26.6	42	227.5	46.2	020	286.6	55.7
43	42.2	08.2	93		17.7	43	140.4	27.3	03	189.4	36.8	4.2	238.5	46.4	02	287.6	6.55
4	43.2	08.4	4	-	17.9	4	141.3	27.5	94	190.4	37.0	44	239.5	46.6	94	288.6	56.0
45	44.2	08.6	95	93.3	18.1	45	142.3	27.7	95	191.4	37.2	45	240.5	.46.7	95	289.6	56.3
46	45.2	8.80	96	94.2	18.3	146	143.3	27.9	196	192.4	37.4	246	241.5	47.0	296	290.5	56.5
47	46.1	0.60	97	95.2	18.5	47	144.3	28.0	97	193.4	37.6	47	242.5	47.1	97	291.5	56.7
4	47.1	1 09.2	98	96.2	18.7	48	145.3	28.2	86	194.4	37.8	48	243.4	47.3	98	292.5	56.9
49	48.	100	66.	97.2	18.9	49	146.3	20.4	66 1	-	38.0	49	244.4	47.5	66	293.3	57.0
31	44	2.60	8	98.2		25	n.M.J	28.0	81	OLON S	38.2	250	245-4	47.7	300	294.5	57.2
Did	Dep	Lat	Did	Dep	Lat	Diff	Dep	Lat	Dig	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat
																	F

for 79 Degrees.

12 Difference of Latitude and Departure for 12 Degrees.

2000				100		200		1																		4	in.	198		der.	1				1											99,54								1
52.2	52.4	24.0	62.0	33.0	2000	53.5	53.7	53.9	54.1	54.3	2 4 4 4	24.0	54.7	54.9	\$5.I	56.3	2 1	33.5	55.7	20.0	56.2	56.4	26.6	2 93		2.70	7/:7	57.4	57.0	57.8	58.0	58.2	58.4	58.7	58.9	59.I	59.3	5.65	50.7	60.0	60.1	60.3	60.5	60.7	6009	61.4	61.4	61.6	61.8	62.0	62.2	62.4	Lat	s.
245.5	240.5	447.4	2.40.4		430.4	251.3	252.3	253.3	254.3	256.2	2000	450%	2.57.2	258.2	259.2	260.T	2 4 4 5	201.1	202.I	263.I	264.I	266.0	266.0	2620	0000	0.00%	209:01	26	27	271.9	272.9	273.8	274.8	275.8	276.8	4	4	19	280.7	281.7	282.6	282.6		285.6	286.6	287.5	288.5	280.5	200.5	29I.			Dep	egrees
H (4	53	1 2 4	25	430	57	50	59	9				03	64	65	266	14				26,	14	72	4.0	3:	4 ;		4											87	88	80		14	02			95	14			200	3	D.O.	De
41.8	42.0	42.2	19.64	0	44.0	43.1	43-3	43.5	43.7	42.0	1 1 1 1	44.1	44.3	44.5	44.7	44.0	, ,	45.1	45.3			,880					40.0	47.0	WES		47.0	47.8						10000					Lane.	50.3	50.5	20.8	5 I.C	\$1.2	51.4	51.6	of the	100	Lat	78
190.0	197.0	200.2	2000.5		401.5	402.4	203.4	204.4	205.4	206.4	202	200	200.3	209.3	210.3	211.2						216.F		2.18.1	1	1.614	5/1/2	22I.		223.0	224		4							222.8	222.7	234-7	226.7	226.7	237.7	228.6	239:6				243	9	ALC: N	for
SHIP COM	EURONATI		and the suppliers	machinest.c	Manual Scott	consumation of					7.2		13				44	2530	300			14		2.2	3	4 ,		4				3	4					14					14	42	4	44	45	246				-		
31.4	0	32.0	22.2	32.00	4.70	34.0	34.9	33.I	33.3	33.5	200	1.00	33.9	34.1	34.3	3.4.€	2 4 6	7-10	34-9	35.5	35.4	35.6	35.8	26.0	260	3,00	300	30.0	30.0	37.0	37-2			100	- 445	38.3	88.5											40.8	41.0	41.2	41.7		Lat	
47.7	ലയാ	60.6	9.1.5	9 00	2	.23.2	154.5	155.5	156.5	157.51	1.8.4	1001	159.4	100.4	161.4	162.2	2001	103.3	104.3	105.3	166.3	167.2	168.2	160.2	140.0	1110	7	172.1	173.1		175.1															180.7			19	19	19		Dep	
	-			77.	2	100			9		_				65	166	44			60	20	171	72		5.4	4/		H					1					dia.					H-			100		U.S.					Did	
21.0	41.0	21.6	27.00		1	0.44	24.5	22.7	22.0	23.I	0.2.2	0.00	2.3.5	23.7	23.9	24.I	0 0 0	44.3	24.5	24.8	25.0	25.2	25.4	2.6.6	200	25.0		20.2	20.4	20.0	20.0	27.0	27.2	27.5	27-7	27.9	-28.I	28.3	28.5	28.7	28.0	20.1	20.3	20.5	40.7	30.0	30.2	MARKET !	3 60	, es	31.0	31.2	Lat	
98.0	0.66	100.7	102.7	700	1.60	2000	105.0	10001	100.00	108.6	TOO. 5	2	5-0-1	III.5	112.5	112.4		114.4	115.4	110.4	117.4	118.3	110.3	TOO. 2	101	141.5	144.3	123.2	124.2	F25.2	120.2	127.1	128.1	129.1	130.I	131.I	132.0	133.0	134.0	135.0	135.0	126.0	127.0	1280	130.0	140.8	141.8	142.8	143.8	144.7	145.7	THE RESERVE	Dep	
IOI	3 6	Na Scotter	ARCO IN	14	SERVICE OF	MORAL PAR	OCAP CO	GEORGE ST	Segnio.	III	TZ	1 0	13	14	15	911	111	10	10	61	8	121	22	9.2	3.0	* 0	श	120	77	28	29	30	131	32	33	34	35	136	27	300		40	141	42	43	44	4.5	146	47	48	49	150	والم	
10.0	0 (17.2	11.4	1		70.1	1 007	12.3	12.5	12.7	T.2.0	7	1.64	13.3	13.5	12.7	T 2.0	4.0.4	14.1	14.4	14.6	14.8	15.0	15.2	TEA	7	200	15.0	DE DESCRIPTION	DUGITIES.	Marine No.	ZHIN-N	-	17.1	17.3	17.5	17.7	17.9	18.0	18.3	18.5	18.7	18.0	10.1	19.3	HOUSE.	Datable	20.0	20.2	3 20.4	20.6	20.8	Lat	*
6-64	2000	21.0	200	0	24.0	55.	50.7	57-7	58.7	40.0	66.6	7	0.10	62.6	63.6	64.5	2 - 2	6.03	00.5	07.5	68.5	69.4	70.4	11.1	70.7	4.7/	13.4	74.3	75.3	76.3	77.3	78.2	79.2	80.2	81.2	82.2	83.1	84.1	84.1	86.1	87.0	88.0	80.0	00.0	91.0	92.0			94.6	95.8	200	97.	Dep	10
51	25	Cavaraties	opiosité de	193	2	200	50	5	0	19	62		60	04	59	199	900	707	9	6	21	71	72	7.3	7.0	* ;	1	70	17	78	79	00	81	82		84	85	86	87	88	89	90	1		93	94	0	0	97	86	66	8	Dia	Personal an
00.2	3 6	000	0.10	01.0		2 4	/-10	6.10	02.1	02.3	0.2.5	7 6	1.70	05.0	03.1	03.3	02.6	3.50	03.7	04.0	04.2	04.4	0.40	8.70	0.50	300	3:5	05.4	500	05.9	0.00	00.2	06.4	2.90	6.90	07.1	07.3	07.5	07.7	07.0	08.1	08.3	08.5	08.7	-			8		IO	10.2	10.4	Lat	
X 2000		0000	7.00	7	19000	0	0 0	0	8.60	10.8	11.9	-	17.1	13.7	14.7	9.51	16.6	7 . Y	0./1	10.0	19.6	20.5	21.5	22.5	2.60	20.0	24.5	25-4	40.4	27.4	40.4	29.3	30.3	31.3	32.3	33.3	34.2	35.2	26.2	29.2		20.1	40.1	41.1	42.I	43.0	44.0	45.0	46.0	46.9	47.9	48.9	Dep	
H	4		+ "	79		-0	THE REAL PROPERTY.			11	-	1 5		-	15	191	1.9	701	01	61	20	21	22	22	200	+ + 0	1	20	77	20	29	39	31	32	33	34	35	36	27	200	30	40	TP	42	42	44	45	46	47	48	49	50	Diff	
	0000.2 5149.9 10.0 101 96.0 21.0 151147.7 31.4 201 190.0 41.8 251 245.5	000.2 5149.9 10.0 101 95.6 21.0 151147.7 31.4 201190.6 41.8 251 245.5	00.2 5149.9 10.0 101 96.6 21.0 151147.7 31.4 201190.0 41.8 251245.5 00.4 52 50.9 10.8 02 99.8 21.2 52148.7 31.6 02 197.6 42.0 52 245.5 00.6 53 51.8 11.0 03 100.7 21.4 53 149.6 31.8 03 198.5 42.2 53 247.4 00.8 54.2 54.1.2 04 10.1 31.6 54 150.6 22.0 04 10.1 54.2 54.4	.000.2 5149.9 10.0 101 96.0 21.0 151147.7 31.4 201 190.0 41.6 251 245.5 .000.4 52 50.9 10.8 02 99.8 21.2 52.148.7 31.6 02 197.6 42.0 52 246.5 .900.6 53 51.5 11.0 03 100.7 21.4 53 149.6 31.8 03 198.5 42.2 53 247.4 .900.8 54 52.8 11.2 04 101.7 21.6 54 150.6 32.0 04 199.5 42.4 54 248.4 .900.8 54 52.2 53 11.4 05 102.7 21.6 54 150.6 32.0 04 199.5 42.4 54 248.4	00.2 5149.9 10.0 101 96.0 21.0 151147.7 31.4 201190.0 41.6 251245.5 00.4 52 50.9 10.8 02 99.8 21.2 52 148.7 31.6 02 197.6 42.0 52 245.5 00.6 53 571.8 11.0 03 700.7 21.4 53 149.6 31.8 03 198.5 42.2 53 247.4 00.8 54 52.8 11.2 04 101.7 21.6 54 150.6 32.0 04 199.5 42.4 54 248.4 01.0 55 57.8 11.4 05 102.7 21.8 55 151.6 32.2 05 200.5 42.6 55 249.4	00.2 5149.9 10.0 101 90.6 21.0 151147.7 31.4 201190.0 41.6 251245.5 00.4 52 50.9 10.8 02 99.8 21.2 35148.7 31.6 02 197.6 42.0 52 246.5 00.6 53 51.8 11.2 04 101.7 21.6 54 150.6 32.0 04 199.5 42.4 54 24 8.4 01.0 55 52.8 11.4 05 102.7 21.8 55 151.6 32.2 05 200.5 42.6 55 249.4 01.2 55 53.8 11.6 105 105 155 155 155 155 155 155 155 155	00.2 5149.9 10.0 101 90.6 21.0 151147.7 31.4 201190.0 41.6 251245.5 10.0 10.0 10.8 02 99.8 21.2 55148.7 31.6 02 197.6 42.0 52 246.5 10.0 03 10.8 11.2 04 101.7 21.6 53 149.6 31.8 03 198.5 42.2 53 247.4 10.0 55 57.8 11.4 05 102.7 21.8 55 151.6 32.2 05 200.5 42.6 55 249.4 10.1 55 57.8 11.6 106 103.7 22.0 156 152.6 32.4 206 201.5 42.8 256 250.4 10.5 57 55.7 11.9 07 104.6 22.3 57 153.5 32.7 07 202.4 43.1 57 251.3	02.000.2 51 49.9 10.0 10.1 90.0 21.0 151 147.7 31.4 101 190.0 41.0 251 245.5 02.000.4 52 50.9 10.8 02 99.8 21.2 52 148.7 31.6 02 197.6 42.0 52 246.5 03.900.8 54 52.8 11.2 04 101.7 21.6 54 150.6 32.0 04 199.5 42.4 54 248.4 04.9 01.0 55 57.8 11.4 05 102.7 21.8 55 151.6 32.2 05 200.5 42.6 55 249.4 05.9 01.2 56 54.8 11.6 106 103.7 22.0 156 152.6 32.4 206 201.5 42.8 256 250.4 06.8 01.5 57 55.7 11.9 07 104.6 22.5 58 154.5 32.9 08 203.4 43.1 57 251.3	02.0 00.4 52 50.9 10.8 02 99.8 21.2 52 143.7 31.4 201 190.0 41.6 251 245.5 02.0 00.4 52 50.9 10.8 02 99.8 21.2 52 149.7 31.4 201 190.0 41.6 251 245.5 02.0 00.4 52 50.9 10.8 11.2 04 101.7 21.4 53 149.6 31.8 03 198.5 42.2 53 247.4 03.9 00.8 54 52.8 11.2 04 101.7 21.6 54 150.6 32.0 04 199.5 42.4 54 248.4 04.9 01.0 55 51.8 11.4 05 102.7 21.8 55 151.6 32.2 05 200.5 42.6 55 249.4 05.9 01.2 56 54.8 11.6 106 103.7 22.0 156 152.6 32.4 206 201.5 42.8 256 250.4 05.8 01.7 58 56.7 12.1 08 105.6 22.7 59 155.5 33.7 07 202.4 43.1 57 251.3 09.8 01.9 59 57.7 12.3 09 106.6 22.7 59 155.5 33.1 09 204.4 43.5 59 253.3	02.000.2 51 49.9 10.0 101 90.0 21.0 151 147.7 31.4 201 190.0 41.0 251 245.5 02.00.4 52 50.9 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110.5 23.5 63 159.4 33.9 13 208.3 44.3 63 257.2 12.7 02.7 63 61.6 13.1 13 110.5 23.5 63 159.4 33.9 13 208.3 44.3 63 257.2 12.7 02.7 63 61.6 13.1 13 110.5 23.5 63 159.4 33.9 13 208.3 44.3 63 257.2 12.7 02.7 63 61.6 13.1 13 110.5 23.5 63 159.4 33.9 13 208.3 44.3 63 257.2 12.7 02.7 63 61.6 13.1 13 110.5 23.5 63 159.4 33.9 13 208.3 44.3 63 257.2 12.7 02.7 63 20.2 20.2 20.2 20.2 20.2 20.2 20.2 20.	02-00-02 51 49-9 10-0 10-1 90-0 21-0 151 147-7 31-4 101 190-0 41.0 251 245-5 02-00-04 52 50-9 10-8 02 99-8 21-2 52 148-7 31-6 02 197-6 42-0 52 245-5 03-90-08 54 52-8 11-2 04 101-7 21-6 54 150-6 32-0 04 199-5 42-4 54 248-4 03-90-08 54 52-8 11-2 04 101-7 21-6 54 150-6 32-0 04 199-5 42-4 54 248-4 04-9 01-0 55 53-8 11-4 05 102-7 21-8 55 151-6 32-2 05 200-5 42-6 55 249-4 05-9 01-0 55 53-8 11-6 106 103-7 22-0 156 152-6 32-4 206 201-5 42-8 256 250-4 05-8 01-7 58 55-7 12-3 09 105-6 22-7 59 155-5 33-1 09 204-4 43-5 59 253-3 05-8 01-9 59-5 12-5 10 107-6 22-9 60 156-5 33-1 10 205-4 43-5 59 253-3 10-8 02-3 51 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Lat	ľ	244.0	245.5	240.5	247.5	248.5	4-642	250.4	25I.4	262.	4.2 4.4	253.3	254.3	2 4 5	4,23.3	250-3	257.2	258.2		*29.4	2000	26I.I	262.I	262.I	1 190	1.40	205.0	266.0	267.0	268.0	268.9	269.9	270.0	271.0	272.8	272.8	244.8	275.8	276.7	277.7	n se	270.7	279.0	280.0	201.0	202.0	283.5	284.5	285.5	286.5	287.4	288.4	289.4	290.4	202.3		Dep
Diff	1	251	25	53	54	55	256	57	88	, 2	2	8	261		Proper	63	64	9	199	200	0	89	69	70	1:40		72	73	74	75	276	77	78	70	80	2.8.T	8	200	3	t &	त्रव	200	000	000	60	श	291	92	93	94	क्ष	362	97	88	300		
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Lat	100	195.9	190.0	197.8	198.8	199.7	200.7	201.7	202.7	202.6	2	204.0	205.6	7 900		207.5	208.5	200.6	1	410.5	211.4	212.4	213.4	214.4	2.7.5.2	2.5.0	410.3	217.3	218.3	219.2	220.2	221.2	222.2	222.I	224.I	226.1	1 900	227.0	228.0	220.0	2000	230.0	230.0	231.9	232.9	433.9	234.8	235.8	230.8	237.8	238.7	239.7	240.7	241.6	243.6	36.36	Dep
Diff							300	07	80	00	CONTRACT	भ	211	101	1	13	14	Iç			17	18	19				777	23	24	2.5	226	27	28	20	30	221	,	222	24	35	1,	230	37	30	39	140	241	42	43	44	45	246	47	48	250		
Dep	. (34.0	34.2	34.4	34.6	34.9	35.1	35.3	35.5	25.8	22.0	30.0	36.2	26.4	4	30.7	36.9	37.I	200	31.3	37.0	37.8	38.0	38.2	28.6	2000	30.7	38.9	39.I	39-4	39.6	39.8	40.0	40.3	40.5	40.7	100	41.2		Y TEG	1	41.6	42.1	42.3	42.5	42.7	43.0	43.2	43.4	43.6	43.9	44.I	44.3	44.5	44.0		Lat
Lat	1,000	47.1	140.1	1.64)	[50.I	6,110	152.0	153.0	1540	64.0	1	155.9	156.0		40/6	158.8	159.8	160.8	1	/	102.7	163.7	164.7	165.6	19.991	7 - 7 -	107.0	108.0	169.5	170.5	171.5	172.5	173.4	174.4	175.4	176.4	144.0	178.2	T70.2	180.2	2	101.2	102.2	163.2	104.2	10501	180.1	187.1	188.1	189.0	19000	0.161	192.0	192.9	104.0		Dep
Dift		151	52	53	54		156	57	\$8	60			IÓI			03	64	9	1×	el cours	07	00	69	70	1:		12	73	74	75	176	77	78	70	8			000	300	100	देश	100	67	000		위	161	92	93	94	95	1961	97	86	99		
Dep		25200 N	22-9	23.2	23.4	23.0	23.8	24.1	24.3	24.6	2	24.7	25.0	2	#12.#	25.4	25.6	25.0	13	7.07	20.3	26.5	26.8	27.0	27.0	1	47.4	27.7	27.9	28.1	28.3	28.6	28.8	20.0	20.2	20.6	200	20.0	20.1	20.4	100	30.0	30.8	31.0	31.3	31.5	31.7	31.9	32.2	32.4	32.6	32.8	33 I	33-3	33.5	100	Lat
Lat	100	90.4	99.4	100.4	IOI.3	102.3	IO3-3	104.3	105.2	106.2		107.2	108.2	1001		I TO. I	III.I	I 12.1	1	113.0	114.0	115.0	0.911	0.911	15	6.7	110.9	119.8	120.8	121.8	122.8	123.7	124.7	125.7	126.7	12.7.6	108.6		120.6	121.6		132.5	133.5	134.5	135.4	130.4	137.4	138.4	139.3	140.3	141.3	142.3	143.2	144.2	145.2	1	neb
Dift	13	101	-			_	1001	07	80	and the	order Services	CI	III	-	*	13	14	Iç	1	PRODE	17	18	19	30	121		77	23	24	25	126	27	780	20	30				2 4	25	3	130	37	30	39	9	141	43	43	44	45	146	47	400	150		
Depil		11.5	11.7	6.11	12.1	12.4	12.6	13.8	13.0	T 2.2	-0.0	13.5	12.7	101	13.3	14.3	14.4	14.6	10	14.0	15.1	15.3	15.51	15.7	16.0	74.0	10.7	16.4	9.91	16.9	17.1	17.3	17.5	17.8	18.0	18.2	18	18.7	18.0	10.1		19.3	100	19.0	0.0	70.7	20.5	20.7	20.9	2I.I	2I.4	21.6	2I.8	22.0	22.5		Lati
Lat	1	49-7	Doctors.		52.0	53.0	54.6	55.5	5.95	27.5	2/0	58.5	4.03	200	4	6I.4	62.4	63.3		04.3	05.3	66.3	67.2	68.2	600	1	70.2	71.1	72.1	73.I	74.1	75.0	76.0	77.0	78.0	-	-	-		82.8	9	03.0		05.7		-				91.6	92.0	93.5			90.5	Children's	Dep
Dift	I	51	52	53	54	5.5	56	57	\$	60	27	8	19	4	3.	63	64	65	14	3	07	89	69	70	1:	'	72	73	74	7.5	76	77	78	70	8	2	8	8	3	~	3/2	000	000		0 (위	16	92	93	94	95	96	97		199		
Dep	1	00.5	90.4	00.7	6.00	i.i	01.3	9.10	8.10	000		02.2	02.5	2	1.70	03.0	03.I	03.4	1	03.0	03.8	04.0	04.3	04.5	100	7.40	04.0	05.3	05.4	05.6	05.8	1.90	06.3	90	06.7	100	0 20	4.70	7	0.70		000	00.3	00.5	00.0	6	2.60	4-60	2-60	6.60	Io.	10.3	10.6	10.8	11.0		Lat
Lat	1	01.0	6.10	6.20	03-9	6+9	05.8	8.90	07.8	00	THE REAL PROPERTY.	09.7	10.7	- 1	1.1.	12.7	13.6			-		-		100000	100		21.4	22.4	23.4	24.4	25.3	26.3	27.3	28.2	20.5	20.02	21.0	22.2	22.T	24.1	1	35-1	30.1	37.0	30.0	39.0	39.9	40.0	41.9	42.9	43.8	44.8	45.8	40.8	47.7		Dep
Diff	1	+	4	3	4	5	9	4	00	C		IO	11	1 0	1	13	14	I	1	07	17	18	19	20	10	1 1	22	23	24	25	36	27	200	20	30	1:	,	22	24	25	निरं	30	37	30	39	8	41	42	43	44	45	46	47	× 4	4 4 5	3	

for 77 Degrees.

14 Difference of Latitude and Departure for 14 Degrees.

del	60.7	6I.0	61.2	61.5	61.7	62.0	62.2	62.4	60.7	62.0		03.2	63.4	63.6	63.0	64.1	177	7 . 7	64.0	24.7	1.50	05.3	65.6	65.8	1.99	66.2	66.5	8.99	64.0	67.0	2 4 9	22.0		0.00	7 8 9	68.5	7009	2	7.60	60.7	000	70.2	70.4	70.7	10.0	71.1	71.4	71.6	71.9	72.1	72.4		Lat
Lat	43.5	44.5	45.5	140.4	47.4	448.4	249-4	250-3	7			2007	254.3			-	1.82.6		1.60%			202.0	6.292	263.9	20,300	265.0	8.997	8.192	8 89%		1.00.4	271.7	7	9 0 0 0	9 7 7 6	94/4	276.	7:	278.5	270.4	+ <	81.4	282.2	282.2	284.3	285.3	286.2	287.2	2882	1.682	290.1		Dep
뜅	25 I 2	522	532	543	55	2563	57.2	585	600	9			62 2	63 2	64	9		-	-			-	271	72	73	74	75	276	24	100	2 6	200		807	7 6	500	100	286			8	00	20T	0.0	020	94	95	296	97	86	99		Diff
Dep	48.6	48.9	49.I	46.4	49.6	49.9	50.I	50.3	40.6	80.0		51.1	51.3	51.5	\$1.8	\$2.0	600	2	24.0	24.0	53.0	53.2	53.5	53-7	54.0	54.2	54.4	1.4.7	24.0	24.2	33.	2004	7.55	55.7	26.	2004	200		27.7	67.6	000	28.4	28.2	28.6	000	50.0	59.3	59.5	59.8	0.09	60.3		Lat
Lat	195.0	0.961	197.0	197.9	198.9	6.661	200.8	20I.8	202.8	202.8		204.7	205.7	206.7	207.6	208.6	200.6	210	2 1	2	41%.5	13.5	14.4	215.4	216.4	217.3	218.3	110.3	220.2	221.2	22.2	222.2	1	12.5.1	1.92	12.7.T	228.0	2000	220.0	230.0	231.0	232.0	233.8	234.8	235.8	236-7	237-7	238.7	239-7	240.6	241.0		Depl
E I	CONTRACTOR	02	03		Int	206	07 2	80	00	IO	100	2112	122	13 2	142	IS	216		781				221 2	22	23		25.	226	0.0	78	2 0	200	नि	434	3 0	33	100	न	200	200	300	700	24.1	12	42	4	45	246	47	48	49	श	Diff
Dep	36.5	36.8	37.0	37-3	37.5	37.7	38.0	38.2	38.5	28.7		39.0	39.2	39.4	39.7	39.0	40.2		1 4	200	40.7	41:1	41.4	41.6	4I.9	42.I	42.3	42.6	42.8	42.1	42.2	42.6	0 0	47.0	44.0	44.5	244	1	45.0	45.5	45.7	46.0	46.2	46.5	46.7	46.9	47.2	47.4	47.7	47.9	48.2		Lat
estata.	146.5	147.5	148.5	146.4	150.4	£1.4	152.3	153.3	I C 4.2	156.2	1	150.2	157.2	158.2	1.651	160.I	Leri	200	16.00	200	104.0	104.9	6.591	6.991	167.9	8.891	8.691	170.8	71.7	72.7	172.7	74.6	1	9.94	944	100	70.6	200	181	182.4	182.4	184.4	184.2	186.2	187.3	188.2	189.2	190.2	191.1	192.1	193.1		Dep
	ISI	52	53	4	5	156	57	581	60	60	11	н	4	63	64	_	VIV	7	~ a			OI	171	73	73	4	7.5	176	3.2	100	2 6		0	8	3 6	200	×	182	-	000		000	12	02	03	94	95	961	97	86	99		Diff
Dep	24.4	24.7	24.9	25.3	25.4	25.7	25.9	26.1	26.4	26.6		20.9	27.I	27.3	27.6	27.8	28.1	000	200	000	0.07	29.0	29.3	29.5	29.8	30.0	30.2	30.5	20.7	3T.0	21.2	2 I.e.			22.2		7 -		22.2	33.4	33.6	33.0	34.1	34.4	34.6	34.8	35.I	35.3	35.6	35.8	36.1		Lat
Lat	0.86	0.66	6-66	6.001	IOI.9	102.8	103.8	104.8	8.001	106.7		107.7	108.7	9.601	9.011	9.111	112.6	2 6	0.01	A	115.5	200	17.4	118.4	119.3	120.3	121.3	122.3	122.2	124.2	2.5.0	26.1	1	186	100	1300	1	122.0	1220	T22.0	124.0	135.8	126.8	127.8	138.7	139.7	140.7	141.7	142.6	143.6	144.6	2	Dep
	ioi	07	03	MOT TOUR		-	071	80	00	IOI	V III	111	12	I3 1	14	151	191		100			m.l.i	121		-	24	-	126	-	-00		30	1:	122	22			126		300	30	40	141	42	43	44	45	146	47	48	150	1	Diff
Dep	12.3	12.6	17.8	13.1	13.3	13.6	13.8	14.0	14.3	14.5	10	14.0	15.0	15.2	15.5	15.7	16.0	16.0	7 91	5.7	1.01	6.01	17.2	17.4	17.7	17.0	18.1	18.4	78.6	0.81	10.1	TO.4		200	20.1	100	20.6	100	27.7	2T.2	27.5	21.00	22.0	22.2	22.5	22.7	23.0	23.2	23.5	23.7	24.0	F	Lati
rat	49.5	50.5	51.4	52.4	53.4	54.3	55.3	50.3	57.2	58.2		2.65	00.5	61.1	62.1	63.I	64.0	2	200	2 4	6-00	07.9	68.0	6.69	70.8	71.8	72.8	73.7	74.7	1.1	16.7	77.6	100	200/	80.0	2 2	82.5	82.5	200	85.4	86.4	87.2	88.3	80.2	00.2	91.2	92.2	93.1	94.1	95.I	96.1		Depl
	51	52	53	54	55	36	57	200	60	9	1	Į,	62	63	64	99	199	3 5	28	3 4	60	2	71	72	73	74	7.5	76	27	787	70	82	100	2 %	2 %	300	000	86	2 %	800	80	000	10	02	020	94	95	96	97		99		Diff
Dep	00.3	00.5	00.7	010	OI.2	01.5	01.7	01.0	02.2	02.4		02.1	03.0	03.I	03.4	03.6	03.0	200		***	0.40	04.9	05.1	05.3	05.0	8.50	0.90	06.3	999	06.8	07.0	07.3	13	07.7	000	2000	200	28.7	000	00.2	4.00	00.7	1000	10.2	10.4	10.6	10.9	II.I	11.4	9.11	11.9		Lat
Lat		610	05.0	03.0	04.9	05.8	8.90	07.8	08.7	00.7	1	10.7	11.6	12.6	13.6	14.6	16.5	16.5	2 2 2	20.7	10.4	19:4	20.4	21.3	22-3	23.3	24.3	25.2	26.2	27.2	28.1	20.I	100	21.0	22.0	22.0	24.0	24.0	25.0	26.0	27.8	30.00	30.8	40.8	41.7	42.7	43.7	44.6	45.6	46.6	47.5		Dep
Dit.	H	CONTRACTOR OF	3	4	بار	9	7	00	0	IO		1	12	13	14	15	191	12	127	9 6	44	20	21	22	23	24	25	26	27	700	20	30	4	32	300	3.6	24	श्र	3,5	200	200	37	: ;	17	42	44	45	46	47	48	49	न	Ditt

for 76 Degrees.

ATTENTA	-	1000	SEP SEA		0		100	200	-				~	200	-	5	~			77	1	7		-	7	0	7	1 4		. 6	. 4	V	N F	. 0	12	V	00	10	33	30	20	0	1 00	9	00	H	3	9	6	H	44	1	-
neb	65.0	65.2	65.5	65.7	66.0	66.3	66.5	8.99	67.0	67.	14	5./0	200	80	68.	68.0	68.8	60	90	, 09		3	70.	70.	70.	70.	71.	71.	71.	71.	72.	72.	72.	72.	73.	73.	73.	74.	74.	74.	74.	75.0	75.	75.	75.	76.	76.	76.	76.	77.	77.		Lat
rat 	142.4	143.4	244.4	145-3	246.3	247-3	248-2	249-2	250-2	25 I.I	100	434.1	453-T	254.0	255.0	256.0	2,56.9	247.0	000	2000	0000	200.0	201.8	262-7	263-7	264-7	265.6	266.6	267.6	268.5	269-5	270.5	271.4	272.4	273.4	274-3	275-3	276.2	277.2	278.2	279-1	280.I	281.I	282.0	283.0	284.0	284.9	285-9	286.9	287.8	288.8		Dep
šİ	251	52	53	545	55	256	37	58	66	9	Typ	707	70	03	64	65	266		• 00	3	3 6	श	271	72	73	74	7.5	276	11	78	79	80	281	82	8	84	85	286	87	88		90	291	92	93	94	95	362	97	98	966		
den	52.0	52.3		52.8	\$3.I	53.3	53.6	53.8	54.1	54.3	446	24.0	54.9	55.1	55.4	55.6	55.9	\$6.I	56.4	166.7	200	50.9	57.2	57.5	57.7	58.0	58.2	58.5	58.7	59.0	59-3	59.5	8.03	60.0	60.3	9.09	60.8	61.1	61.3	61.6	6.19	62.1	62.4	62.6	62.0	63.1	63.4	63.7	63.9	64.1	64.4		Lat
Lat	194.1	195.1	1.961	0.761	198.0	0.661	6.66I	200.9	201.9	202.8	100	0000	404.0	205.7	200-7	207.7	208.6	200.6	210.6	O.T.T.	2 2 2 2	414.5	213.5	214.4	215.4	216.4	217.3	218.3	219.3	220.2	221.2	222.2	223.I	224.I	225.I	226.0	227.0	228.0	228.9	229.9	230.9	231.8	232.8	233-7	234.7	235-7	236.6		238.6	63	240.5	SS, 89	Dep
	20I	02	03	04	05	300	COLUMN TO SERVICE	80	00		1	organization.	7	13			216		18					7	23	24	25	226	27	78.	29	30	221	32	3 65	34	35	236	37	38	39	40	241	42	43	OSCILLO VICE	45	246	4	4	49		Did
del	39.1	39.3	39.6	39.9	40.I	40.4	40.6	40.9	41.1	41.4	4 7 4	4	41.9	42.2	45.4	42.7	43.0	43.2	43.5	40.4	40.4	44.0	44.3	44.5	44.8	45.0	45.3	45.5	45.8	46.1	46.3	46.6	46.8	47.1	47.4	47.6	47.9	48.1	48.4	48.7	48.9	49.2	49.4	49.7	49.9	50.2	50.5	50.7	31.0	51.2	51.5		Lat
Lat	145.8	146.8	147.8	148-7	149.7	150.7	151.6	152.6	153.6	154.5	133	25.5	2000	157.4	158.4	159.4	160.3	161.2	162.3	T62.2	2007	104.7	105.2	1,991	167.1	1.891	0.691	170.0	171.0	171.9	172.9	173.9	174.8	175.8	176.8	177.7	178.7	179.7	180.6	181.6	182.6	183.5	184.5	185.5	186.4	187.4	188.4	189.3	190.3	191.2	192.2	- 22	Dep
1	ISI 1	52	53	54	55	CORPLETELS	MANAGEMENT AND ADDRESS OF THE PARTY AND ADDRES	00		900	-	CONTRACT		NO. CONTRACTOR		65	166	1	-00	0		श	171	72	73	74	75	176	77	200	70	8	181	82	00	84	85	186	87	88	89	8	161	92	93	2	95	196	97	86	99		
		26.4	26.7	26.9	27-2	27.4	27.7	28.0	28.2	28.5	200	1.07	29.0	29.5	29.5	29.8	30.0	20.2	20.5	000	300	31.1	31.3	31.6	31.8	32.I	32.4	32.6	32.0	33.E	33.4	33.6	22.0	24.2	34.4	34.7	34.9	35.2	35.5	35-7	36.0	36.2	36.5	36.7	37.0	37.3	37.5	37.8	38.0	38.3	38.6	3000	Lat
Lat	92.6	98.5	99.5	100.5	IOI.4	102.4	103.4	104.3	105.3	106.2	0 10	7.00	7.001	10601	110.1	III.I	112.0	112.0	114.0		644	115.9	6.911	117.8		8.611	120.7	121.7	122.7	123.6	124.6		126.6	SECTION 1	128.5	100,000	130.4	131.4	132.3	133.3	134.3	135.2	136.2	137.2	138.I	139.1	140.I	141.0	142.0	143.0	143.9	444.7	Dep
ij	IOI	02		MINISTER STATE	and the latest and th	901	07	80	8	IOI	PUBL	COLUMN TA	and the same	13	14	IS	911		1×1			~	121	22			25	. I Decision	- Constant	200	-		2002-1/10	-	000000000	3 4	35	a later	37	38	39	-	141	42	43	44	45	146	47	48	49	313	Diff
	13.2	13.5	13.7	14.0	14.2	14.5	14.8	15,0	15.3	15.5	100	2	000	10.3	16.6	8.91	17.1	17.2	17.6	12.0	· / ·	1001	18.4	18.6	18.9	19.2	19.4	19.7	19.0	20.5	20.4	20.7	21.0	21.2	21.5	21.7	22.0	22.3	22.5	22.8	23.0	23.3	23.6	23.8	24.1	24.3	24.6	24.8	25.1	25-4	25.0	٢٠٠٠)	Lat
T'at	49.3	50.2	5 I.2	52.2	53.1	54.1	55.1	26.0	57.0	8.0		-	6-6	0	20	00.	63.7	64.7	65.7	7 7 7 7	2 2 2		9.89	69.5	10	71.5	72.4	73.4	4	. 61	3 60	30	10	70.2	80.2	81.1	82.1	83.1	84.0	85.0	86.0	86.9	87.9	88.0	89.8	8.06	91.8	92.7	93.7	94.7	95.6		Dep
	WIND AND		-	54	55	56	57	58	20	30	TE	1 1		C3785-L	4		99	67	89	9	354.5	श	71	72	73	74	7.5	76	77	78	70		Į.	82	200	84	85	98	87	88	89	90	16	92	93	94	95	96	97	98	199	-	0:0
तेश	20.3	20.5	8.00	0.10	01.3	9.10	%.IO	02.I	02.3	02.0	000	2 6	1.50	03.4	03.0	03.9	04.1	4.40	04.7		4	25.4	05.4	05-7	0.90	06.2	06.5	06.7	07.0	07.2	07.5	07.8	080	08.2	80	80	1.60	00.3	9.60	8.60	IO.I	10.4	10.6	10.0	II.I	11.4	9.11	6.11	12.2	12.4	12.7		Lat
181	01.0	0.10	02.0	3.9	04-8						7	2	٥,	ō	3.5	14.5	15.5	16.4	17.4	T.	1 0	2	20-3	2.I.2	23.2	23.2	24.I	25.1	26.1	27.0	28.0	29.0	20.0	30.0	H	00	3.00	34.8	35.7	36.7	37.7	38.6	39.6	40.6	41.5	42.5	43.5	44-4	45.4	46.4	47.3		Den
ij	ī	77	3	4	5	9		00		IO	1		-		14		16	T7	00	-	61	8	21	22	23	24	25	26	27	200	0	30	15	6	7	2 4		36	37	38	39		41	42	43	44	45	46	47	48	49	١٩	1

for 75 Degrees.

16 Difference of Latitude and Departure for 16 Degrees.

													Ypi7											135			510		200		12/10	2000			2496												4			$\overline{}$	~	~~1		=		-	7	LIGHT.	*2004552
Dep	69.3	69.5	60.7	70.07	9 6		70.0	70.8	71.1	71.4		777	71.0	12.2		72.5	72.8	73.0	40.0	60,0	73.0	73.9	74.1	74.4		74.7	75.0	75.2	75.5	3,5	?	70.1	76.3	20.9	26.9	77.2	77-4	77.7			78.		70.0	79.	2 2			80.2	000	000	81.0	81.3	81.6	81.9	82.1	82.	82.	- Lat	S
Lat	41.2	42.2	42.2			: -	40.0	47.0	48.0	48.0		649.0	250.0	ST. S	0 - 0	22.0	253.7	254.7	1:	123.	2500	257.6	258.5	250.5		2000.5	261.4	262.4	262.2	6.60%	204.3	265.3	2992	267.2	268.2	269.I	270.I	2.7	1	1 6	7 5	1/3:3	274.9	27	270	277.0	276.7	279.7	280.6	281.6	282.6	283.5	284.5	285.5	286.4		288.3	Dep	Degrees
	251 2	522	53	649	2 2 2	3	2502	57 2	582	50	7	3	261	0010-1	September 1	50	-	65			07	100000	69	70		271	72	73	7.4	,	3	7	77	2			28I					ीं	700	00			10.0	291	92	93	94	95	362	97	86		300	Dia	De
Dep	55.4	55.7	65.0	56.2	2 4 2	200	20.0	57.0	57.3	57.6		57.9	58.2	* 8 3	1	50.7	59.0	50.3	2	24.0	59.0	1.09	60.4	9.09	1	6000	61.2	61.5	61.7	60.0	27	02-3	02.0	62.8	63.1	63.4	63.7	63.0	64.2	64.5	8.79		05.0	MAG	0.50	45.7		666.4	60.7	02.0	67.2	67.5	67.8	68.1	68.3	68.6	08.6	Lat	7.4
DESCRIPTION OF THE PERSON OF T	193.2	194.1	OC.T	1.901			198.0	199.0	100.0	200.0	0	201.0	202.8	300	2000	204.7	205.7	206.6	9 200	200	208.0	2005	210.5	21I.4		212.4	213.4	214.3	216.2	0.010	410.3		218.2	219.1	220.I	221.1	233.0	221.0	221.0	0000	205.0	100	220.0	227.8	220.7	449.7	230.7	231.6	232.6	233.6	234.5	235.5	236.4	237.4	238.4		240-3	Dep	for
	IOI	-	WEST STATES				17/2/200		80			150	2112			132	14 2	-	376		17	18	19	20				23		1 '			27		29	30	23I	32	33	3 ?	25		7			39	9	241	42	43	44	45	246	47	48		200	Diff	
Dep	41.6	41.0	42.2	7 2 7	1 1	7.74	43.0	43.3	43.5	42.8		44.1	44.4	7 7 7	44	44-9	45.2	45.5		43.	40.0	46.3	46.6	46.0	1	47.1	47.4	47.7	48.0	0	40.7	48.5	48.8	49.I	49.3	49.6	49.0	40.2	50.4		Shaff		51.3	51.5	54.0	2.4.1					35	383		54.3	54.		55.1	Lat	
Lat	145.I	46.1	1.4.	100	40.0	149.0	149.9	150.9	¢1.0	162.8	0	53.8	154.7	4	1334	150.7	157.6	158.6	13	139.3	160.5	161.5	162.4	T62.4		104.4	165.3	166.3	167.2	2007	100.2	169.2	170.1	1,1,1	172.0	173.0	174.0	174.0	175.0	2 947	177 8		176.0	179.7	160.7	101.7	182.0	183.6	184.5	185.5	186.5	187.4	188.4	189.3	190.3		192.2	Dep	
	ISI	M M P	53	2 2 2		7	-		GMN40			8	191				64]				02	89	69				72	73	7.4			176		78		80	181	82	83	3	2	g.a		87				H	700	93		95	No.	100		100	200	Diff	
Dep	27.8 1	28.1	28.4	28.7	92.43	TSON TO	250000	29.5	29.8	20.0		30.3	30.6	30.0	200	31.1	31.4	31.7	200	34.0	32.2	32.5	32.8	22.I	100	33-3	33.6	33.0	24.2		34.4	34.7	35.0	35-3	35.6	35.8	16.1	26.4	26.7	26.0	30.7	*!	37.5	37.8	38.0	30.3	38.0	38.9	39.1	39.4	39-7	40.0	40.2			41.1	41.3	Lat	
Lat	97.1	080	000	000	3 6	7	101.9	102.8	103.8	TO4.8		105.7	106.7	9 40	200	0.801	100.601	110.4	1:	2	112.5	113.4	114.4	II K. 2		110.3	117.3	118.2	TTO.2	****	120.1	IZI.I	122.1	123.0	124.0	124.9	124.0	10.6.0	120.8	0000	0.071	179.0	130.7	131.7	132.0	133.0	134.0	135.5	136.5	137.4	138.4	139.4	140.3	141.3	142.2	143.2	144.2	Dep	
	IOI	02	02	ENCOUNT.	6.000A	HETS: DA	90	NIEK ZEU	08	STANSON SO	March C			WHO IS	1	13	14	IC	14	TO SEC	17	18	19	20	NATED IN	Displace)		23	mental title	7 0	श	126	27	78	29	30	III	22	33	3,5	4 .	न	130	37	30	39	81	141	42	43	44	45	146	47	48	49	150	Dig	
Depl	4.I	4.3	9		4.7	3	15.4	15.7	16.0	16.2		10.5	16.8	1	1./-	7.4	17.6	17.0	180		18.5	18.7	0.61	IO. 2	3	19.0	19.8	20.I	20.4	1 0	7.07	20.9	21,2	21.5	21.8	22.0	22.3	22.6	22.0	1 00	40.0	*3.4	23.7	24.0	24-3	44.5	24.0	25.I	25.4	25.6	25.9	26.2	26.5	26.7	27.0	27.3	27.0	Lat	
Lat	40.01	0.0	0	,	1.7	510	20.	4.8	5.7	6.7	3	7.7	8.6	2	5	52255	61.5	-	1	*	4	SEEDING.	66.3	67.2	7	. 2	2-69	70.2	1:1	1 0 0		Name of Street	74.0	75.0	75.9	6.94	77.0	00	70.8	80.3	× 1.0		02.7	83.0	04-0	05.2	00.5	87.5	88.4	89.4	90.3	91.3	92.3	93.2	94.2	95.3	196	Dep	allagaran
Diff	13	MARKET !	200	333	545	555	565	575	283	200	37	90	61 6		677	63 6	64 6	6516			67.0		969				72	73	744			70	77	78.	79	80	81	82	-	3		ी	000	62	000	Section 1		16	92	93	94	95	96	97	86	66	8	Diff	, St
Dep	00.3	00.00	00		1.10	19	01.7	0.10	02.2	2.00	200	02.8	02.0	2	03.3	03.0	03.0	O.T.	1	04.4	04.7	05.0	05.2	OF. F	25.0	05.9	1.90	06.3	9-90	9	6.9	07.2	07.4	07.7	08.0	08.3	8.6	000	1.00	3	4.00	3	6-60	100.000	OR AND	10.7		11.3	11.6	11.9	12.1	12.4	12.7	13.0	13.2	No. of Lot	CONTROL OF	Lat	
Lat	01.0	O.T.O	100	6.70			05.8	06.7	07.7	180	100	9-60	TO.6	3	11.5	12.5	I 2.K	TALA		15.4	16.3	17.3	18.3	10.0	1	20-2	2I.I	22.I	7.7.T	1.00	24.0	25.0	26.0	26.9	27.9	28.00	20.8	20.8	21.7	7 0	34.1		34.0	35.0	30.5	37.5	38.4	39.4	40.4	41.3	42.3	43.3	44.2	45.2	46.I	47.I	48.1	Dep	1 · · · ·
Dift	F	100		3.	4	5	9	7	00			IO	-	1	17	13	IA	15	1	01	17	18	IO	1000		21	22	22	3 6	44	25	36	>27	28	20	30	27	200	20	99	34	35	36	37	38	39	9	41	42	43	44	45	46	47	48	49	50	Diff	1

Difference of Latitude and Departure for 17 Degrees. 17

			1	September 1	edin se				W.		200	Birtis.		500	60	1900			1200	Section 1					Strate.		300	100	致规		Sec. 6	1000	12.25		100		民生		Sept.		(9.98			1000			S S				1	2000	
Dep	42.2	73.6	73.0	74.1	74.4	74.7	75.0	75.3	75.6	75.9	16.0	1000	70.5	70.8	77.1	77.4	77.7	77.9	78.2	78.	78.8	10.7	- 6	79.4	79.7	80.0	80.3	80.6	80.9	81.2	81.5	81.7	82.0	82.3	82.6	82.9	8342	83.5	83.8	84.1	84.4	84.7	85.0	85.3	85.5	8.50	86.1	86.4	86.7	67.0	87.3	2/6	3
Lat	240.0	241.0	24 I.O	242.0	243.8	244.8	245.8	246.7	247.7	248.6	4 080	249.0	250.5	251.5	252.4	253.4	254.4	255.3	256.3	257.2	258.2	3.00.T	239.1	200.I	26I.I	262.0	263.0	263.9	264.9	265.8	266.8	267.7	268.7	269.7	270.6	271.6	272.5	273.5	274.4	275.4	276.4	277.3	278.3	279.2	280.2	281.I	282.1	283.0	284.0	285.0	285.9	Konsk	dea
Diff	1:00	42	2	2 4 3	35	256	57	85	59	9	140	707	07	63	40	65	266	67	89	Q	10	100		72	73	74	7.5	276	77	78	79	80	281	82	83	-84	85	286	87	88	.89	90	291	92	93	94	95	296	97	98	66	3	
Dap 1	28.8	69.0	50.3	60.6	59.9	60.2	60.5	8.09	61.1	61.4	67.4	1000	07.0	62.3	05.0	62.8	63.1	63.4	61.7	64.0	64.3	64.6	1	04.0	65.2	05.5	65.8	1.99	66.4	9.99	6.99	67.2	67.5	67.8	. 68.I	68 4	68.7	0.69	69.3	69.6	6669	70.2	70.4	70-7	71.0	71.3	71.6	71.9	72.1	72.4	72.7	3	Trut
Lat	102.2	T02.2	1.70J	100	0.961	197.0	197.9	6.861	199.9	300.8	1000	401.0	202.7	203-7	204-6	205.6	206.5	207.5	208.5	200.4	210.4	1:10	411.3	212.3	213.2	214.2	215.2	216.1	217.1	218.0	219.0	219.9	220.9	221.8	222.8	223.8	224.7	225.7	226.6	227.6	228.5	229.5	230.5	231.4	232.4	233.3	234-3	235.2	236.2	237.I	238.1	234.1	Dep
Diff	10%	PERSONAL PROPERTY.	Charles	04	050	902	00	80	8	IOI	15		77	13	14	15	216	17	18	10	20		1 1	22	23	24	25	326	27	30	29	30	23I	32	33	34	35	236	37	38	39	40	241	42	43	44	45	246	47	48		250	
Dep 1			44.7	45.0	45-3	45.6	45.9	46.2	46.5	46.8	44.4		47.4	47.0	47.9	48.2	48.5	48.8	49.I	40.4	40.7	20.0	2	50.3	20.0	50.9	\$1.2	51.4	51.7	52.0	52.3	52.6	52.9	53.2	\$3.5	\$3.8	54.1	54.4	54.7	\$5.0	55.2	55.5	55.8	56.1	56.4	56.7	57.0	57.3	57-6	57.9	58.2	30.5	Lat
Lat	139	46.2	146.3	147.3	148.2	149.2	ISO.I	ISI.I	1,52.0	153.0		1340	154.0	155.9	156.8	157.8	158.7	159.7	160.6	161.6	162.6	160 .	203.5	104.5	165.4	100.4	167.3	168.3	169.3	170.2	171.2	172.1	173.1	174.0	175.0	175.9	176.9	177.9	178.8	179.8	180.7	181.7	182.6	183.6	184.6	185.5	186.5	187.4	188.4	189.3	190.3	141.º	Dep
Oi R	15	52	6.3	44	55	156	57	Name of	65	9	distract	ESTRACE	MARKET STATE	GREAT SHAPE	no collisco	9	CONNUC	67	Industrial Res	Name and Address	70	L/MANUAL	-/-	72	73	74	75	176	77	28	79	80	181	82	.83	84	85	186	87	80	89	90	IOI	92	93	94	95	1961	97	98	66	200	Diff
Dep 1	20.5	20.02	10.1	10.4	30-7	31.0	31.3	31.6	31.0	33.2	200	9 4.4	32.7	33.0	33-3	33.6	33.0	34.2	34.5	24.0	3.8.I	1	55.4	35-7	36.0	36.2	36.5	36.8	37.I	37.4	37.7	38.0	18.3	38.6	38.9	39.2	39-5	30.8	40.0	40.2	40.6	40.9	41.2	41.5	41.8	42.1	42.4	42.7	43.0	43.3	43.6	43.0	Lat
Lat	9.90	07.6	08.4	4.00	100.4	IOI.4	102.3	I03.3	104.2	105.2	Too T	100	107.1	108.1	0.601	110.0	110.0	III.0	12.8	K	114.7		1.0.	110.7	117.6	118.6	119.5	120.5	121.4	122.4	123.4	124.3	125.3	126.2	127.2	128.1	129.1	130.0	131.0	132.0	132.9	133.9	134.8	135.8	136.7	137-7	138.7	139.6	140.0	141.5	142.5	143.4	Dep
Dift	13	020	03	0.0	-	190		80	-	ROBERT 44		1	77	13	14	15	911	17	81	- C	20	or Walk State	-	and the same		and the last	2.5	126		38	20	30	131	32	33	34	35	136	37	38	39	40	141	42	43	44	45	146	47	48	49	150	
Depi]	19	16.3	16.6	00	16.1	16.4	16.7	17.0	17.2	17.5	۱	17.0	18.1	18.4	18.7	19.0	F9.3	10.6	10.0	000	20.5	000	0 1	2I.0	21.3	21.0	21.9	22.2	22.5	22.8	23.1	23.4	23.7	24.0	24.3	24.6	24.8	25.I	25.4	25.7	26.0	26.3	26.6	26.9	27.2	27.5	27.8	28.1	28.4	28.6	28.9	7.62	Tat
Lat	8	10.7	40.7	61.6	52.6	53.5	54.5	\$ 5.5	\$6.4	47.4	10	50.3	59.3	600.2	61.2	62.2	61.I	64.I	66.0	7 99	999	1:	6.60	98.8	69.8	70.8	71.7	72.7	73.6	74.6	75.5	70.5	77.5	78.4	79.4	80.1	81.3	82.2	83.2	84.1	8 5. I	86.1	87.0	88.0	88.9	89.9	8.06	91.8	92.8	93.7	94.7	95.0	a a
Diff	1	6.0	62	6.4	55	56	5.7	200	65	99	1:3	100	07	63	64	65	99	67	89	y	100	1:	16	72	73	74	7.5	36	77	78	79	80	81	82	00	-84	85	86	82	00	80	06	10	92	93	94	95	96	97	98	66	8	Dig
Depl	3	9 9		31.2	2.IC	8.10	07.0	52.3	22.6	0.00	0	03.2	03.5	03.8	04.1	4-40	94.7	0.00	36.2	200	0	7	1.00	06.4	06.7	0,10	07.3	07.6	07.0	08.2	08.5	08.80	1.00	00.4	9.60	0000	10.2	10.5	10.8	II.I	11.4	11.7	12.0	12.3	12.6	12.9	13.2	13.4	13.7	14.0	14.2	14.0	Lat
Lati			7 6	200	04.8	15.50	06.7	07.6	08.6	9.00	1	10.5	11.5	12.4	13-4	14.3	15	16.3	9.2	8	10.1	13	200	2I.0	22.0	22.9	23.9	24.9	25.8	26.8	27.7	28.7	20.6	30.6	31.6	32.5	33.5	34.4	35.4	36.3	37.3	38.2	39.2	40.2	4I.I	42.I	43.0	44.0	44.9	45.0	46.9	47.0	Dep
Diff	ľ			2 4	2	100	7	00	0	_			IZ		ササ	IS	91	17	18	1	20	1	18	22	23	24	2.5	36	27	28	29	30	31	32	33	34	35	36	37	90	39		41	42	43	44	45	46	47	400	49	2	
Marian	-contra		-	_	-	-	_	-	10000	-	the same of	and the last	STATE OF THE PARTY.	All Property lies	1	9000000	125/08/2020	THE REAL PROPERTY.	and the state	0.00000	TO SHARE WAS	DESCRIPTION OF THE PARTY NAMED IN	Section 2	DOM:N	CHESTAGE	CONTRACTOR OF THE PARTY OF	100000	CHICAGO CONTRACTOR	STATE OF THE PERSON	5/67/753/973	356517 P	E-1000	CONTRACTOR OF	STREET, STREET,	1000 CC	100000	1200000000	2850V25	P. 259-553	ASSESSED FOR	T-10153	PC 099055	CHILD PROPERTY.	SECTION SECTION	THE RESERVE	NAME OF TAXABLE PARTY.	ASSESSED AS	STHE CO.	290000000000000000000000000000000000000	10/00/00	ALC: UNDER	CONTRACT	PERSONAL PROPERTY.

18 Difference of Latitude and Departure for 18 Degrees.

	77.6	77.9	78.2	78.5	78.8	79.1	79.4	79.7	80.0	80.3	80.6	81.0	0.0	8 T &	2	61.9	02.7	82.5	0.70	03.1	63.4	83.7	84.0	84.4	84.7	050	65.3	05.0	6.50	86.5	86.8	87.1	87.4	87.8	88.1	88.4	88.7	0.60	80.00	800	00.2	90.0	90.8	91.2	91.5	8.16	92.1	92.4	100
Tat	238.7	239.7	240.6	241.6	242.5	243.5	244.4	245.4	246.3	247-3	248.2	2.40.2	7.64.	1000	101200	欧洲 雅	253.0	253.0	254.9	0 0	250.8	257.7	258.7	250.0	20000	201.5	202.5	203.4	404-4	266.2	31 6	268.2	1.69z	270.1	271.0	272.0	272.9	273.9	274.0	2,40	1.014	278.6	270.6	280.5	281.5	282.4		284.3	
šl	251	52	53	54	5.5	256	57	58	6.5	900	190		COMPANIES.	3,4	COURS.	arcents.	2000	02	00		report the	271	72	73	74	5	270	77	10/	80	281	82	83	84	85	286	82	000	60	भेड	100	25	94	95	296	97		66	31
120	62.1	62.4	62.7	63.0	63.3	63.7	64.0	64.3	64.6	64.0	66.0	7.59	00	0.50	1.00	00.4	00.7	07.I	07.4	07.7	0000	08.3	08.0	68.9	09.3	200	8.60	70.1	70.5	71.1	71.4	71.7	72.0	72.3	22.6	72.9	73.2	73.5	73.9	11:	24.	75.1	75.4	75-7	76.0	76.3	76.6	70.0	
	191.2	192.I	193.I	194.0	195.0	195.9	196.9	8.26	8.861	199.7	200.7	20T-6	9 000		200	204.5	205-4	200.4	207-3	*00.3	2005	210.2	211.I	212.1	213.0	214.0	14.9	215-9	217.00	218.7	\$10.7	220.6	221.6	222.5	223.5	224-4	225.4	220-3	2000	220.2	220.1	231.1	232.0	233.0	233.9	234.9	235.8	230.0	
	NAME OF STREET	07	03	8	8	90%	07	80	60	IOI	117	10		? :	# ;	3	210	17						23	4		220	2007	0 0	30		32	33	34	35	236	37	30	39	1	144	4	44	45	246	47	4	49	
	46.7	47.0	47.3	47.6	47.9	48.2	48.5	48.8	49.I	40.4	40.7	100		200	100	21.0	51-3	51.0	51.9	54.4	52.5	52.0	53.I	53.5	53-0	54.1	54.4	54-7	2000	9000	55.0	56.2	56.5	56.9	57.2	57.5	57.8	50.1	000		50.0	20.0	20.0	60.3	9.09	6000	61.2	61.8	
	143.6	144.6	145.5	146.5	147.4	148.4	149.3	150.3	151.2	152.2	152.7	T.64.T		2000	4502		157-9	No. 244	0 1	7.001	10107	102.0	0	104-5	3	41	107-4	100-3	2000	171.2	172.1	173.1	174.0	175.0	175.9	176.9	177.8	178.8	180.7	181 6	182.6	183.5	184.5	185.4	186.4	187-3	188.3	189.2	
	ISI	52	53	54	55	156	57	58	59		147	#1400MG/I	VIII CONTRACTOR	?;	+		0		-			171	7	73	74	-	170			× %		82	83	200	2	186	82	-	60	45	100	03	94	95	196	97	86	99	
	31.2	31.5.	31.8	32.I	32.4	32.8	33.I	33.4	33-7	34.0	24.2	24.6	0 00	25.2	300	33.5	35.0	30.4	30.00	30.0	37.1	37.4	37.7	30.0	30.3	30.0	30.9	39.2	20.00	40.2	T NACH	NAME OF TAXABLE PARTY.	maiotomos	NAME OF TAXABLE		43.0	42.3	42.0	43.0	42.4	43.0	44.2	44-5	44.8	45.1	45.4	45-7	40.0	
	1.96	97.0	0.86	6.86	6.66	8.001	8.101	102.7	103.7	104.6	100.6	100.	200	200	4	109:4	110.3	111.3	11202	113.2	14.1	13.1	0.01	112.0	17.9	18.9	2.61	20.0	7.17	22.6	24.6	125.5	126.5	127.4	128.4	129.3	130.3	131.2	132.2		134.1	136.0	136.0	137.9	138.8	139.8	140.1	141.7	1 4 4 4 5
1	IOI	07	03	40	3	1001	04	080	60	IOI	13	NORS. 7	1	2.5			011	17	101		20	121	22	23	24	25	120	27	0 0	30	131	32	33	34	35	136	37		3 0	1	127	- 4	44	45	146	47	48	150	
1	5.00	1.01	4.93	16.7	17.0	17.3	9.43	17.9	18.3	18.5	00	10.2		200	, ,	3	4.0	0.7	3 0	5-1	21:0	6.1.	77.7	77.0	12.0	13:2	3.5	0.63		4.7	13	5.3	15.6	0.97	26.3	9.93	50.0	27.2	200	2	8	28.7	29.0	29.4	29.7	30.0	30.3	30.0	
1	8.5	9.5	0.4	1.4	52.3	3.3	4.2	5.3	6.1	7.1	8.0	50.0	0	60.0	COMP II		0.00	3.7	1	5.6	0	7.5	0.5	9-4	4.0	1.3	£.3	3.00	1	6.1	7.0	8.0	8.9	6.6	800	81.8	2.7	3.7	2.6	2 2	37.5	88.4	89.4	0.3	1.3	2.2	3.2	4.1	
	514	524	53 5	543	55 5	365	573	585	595	605	9119	RUBURY	600	25	,			020	900	60	701	716	72	73	74/	75	70/	77	100	807	811	827	837	847	85	98	87	000	600	7	02	03	94	95	96	97	86	100	
1	00.3	9.00	6.00	DI.2	01.5	6.10	02.2	02.5	02.8	03.I	22.4	02.7	20.00	24.0	24.0	24.0	04-0	5-3	25.0	6-50	200	2000	200	07.1	07.4	07.7	0.00	00.3	1000	200.2	90.00	6.60	10.2	10.5	10.8	II.I	II.4	11.7	10.1	10.7	T2.0	13.3	13.6	13.9	14.2	14.5	14.8	15.1	
	010	6.10	02.9	03-8	8.40	05.7	06.7	07.6	08.6	5.60	101	2 5	-	600	20.0	41	15.2	10.2	1.6	100		0.00	50.0	21.9	27.0	23.8	24-7	25.7	0 9 6	200	100	30.4	31.4	32-3	33-3	34.2	35.2	30.1	37.1		20.00	40.0	41.8	42.8	43.7	44-7	45.0	40.0	5 1
	1	4	3	4	5	9	7	00	6					? ?	1:	3	0 1	17	01	61	70	21	23	23	24	25	20	70	0 0	and the second	311	33	33	34		36	37	38	39	2 :	100	4	44	45	46	47	40	46	

for 72 Degrees.

Difference of Latitude and Departure for 19 Degrees. 19

	1000		300	6		200	2014		e (e)							250		500		100						-			3000					-						0.00			100										-	
Dep	81.7	82.1	82.4	82.7	83.0	83.4	83.7	84.0	84.2	2 4		65.0	85.3	85.6	86.0	86.3	86.6	8,4	2 2 2	2.70	0./0	67.0	88.7	88.6	88.9	89.2	89.5	89.9	90.1	90.5	800	91.2	91.5	91.8	92.1	92.5	92.8	93.1	93.4	93.8	94.1	94.4	94.7	95.1	95.4	95.7	96.1	96.4	96.7	97.0	97.4		Lat	,
Lat	237.2	38.3	139.2	40.1	14I.I	143.0	43.0	43.0	44.0	000	100	140.0	147.7	148.7	149.6	150.5	13:13	20.0	200	100	54.3	25:3	220-2	257.2	258.I	1.652	260.0	5000	6.197	262.8	163.8	264-7	265.7	9.997	9.697	268.5	5-69-5	270.4	271.3	272.3	273.2	274.2	175.I	176.1	177.0	178.0	178.9	6.661	80.8	181.7	282.7	2	Dep	100
Diff	251 2		532	542	55 2	2562	572	000	60	609	1	201	62 2	63/2	647	65	266	64	689		3 8	श	271	72	73	74	75	276	77	78	79	8	281	82	83	84	8	286	87	88	89	8	291 2	92	93 2	94	95 2	2962	97 2	00	66	Title-ordered	Dift	
Dep	gor.	65.8	1.99	66.4	66.7	67.I	67.4	67.7	68.1	68.4	107	1000	0.69	69.4	69.7	70.0	70.3	70.7	71.0	11.0	2.1	1	72.0	72.3	72.6	72.9	73-3	73.6	73.9	74.2	74.6	74.9	75.2	75.5	0	7	n-months	76.8	77.2	3	77.8	78.1	78.5	78.8	79.I	79.4	798	80.1	80.4	80.7	8T.A	*	Lat	
Lat	0.06	191.0	6.161	192.9	193.8	194.8	195.7	196.7	107.6	108.5		199.5	200.4	201.4	202-3	203-3	204.2	206.2	1.902	1 100	1000	2000	508.9	209.9	210.8	211.8	212.7	213.7	214.6	315.6	\$16.5	217.5	218.4	219.3	220.3	221.2	222.2	\$23.I	124-1	125.0	126.0	126.9	127.9	128.8	229.7	230.7	231.6	232.6	233-5	234.5	235.4	1000	Dep 1	
Ditt	20I	-	03	acceptable a	05	PROPERTY	07.1					311	12	13	14	15	216		181				_		23	24	25	226	27	28	3	3	-	32	33	34	35	236	37	38	39	8	241	42	43	44	45	2462	47			-	Diff	
Dep	49.2		49.8	50.I	50.5	50.8	51.1	51.4	% I.S	£2.1		52.4	52.7	53.I	53.4	53-7	64.0	2.4.7	5.4.2	1	35.	55.4	55.7	26.0	56.3	56.7	57.0	57.3	57.6	58.0	58.3	58.6	58.9	59.3	59.6	59-9	60.2	9.09	6009	61.2	61.5	61.9	62.2	62.5	62.8	63.2	63.5	63.8	64.I	64.5	64.8	05.1	Lat	I
Lat	42.8	143.7	144-7	145.6	146.5	147.5	148.4	149.4	150.3	151.2	7	154.4	153.2	154.1	15551	156.0	1,56.0	1 57.0	1,50	0	1500	7	101.7	162.6	163.6	164.5	165.5	166.4	167.3	168.3	169.2	170.2	171.1	172.1	173.0	174.0	174.9	175.9	176.8	177.7	178.7	179.6	180.6	181.5	182.5	183.4	184.4	185.3	186.3	187.2	188.1		Dep	
Dift	ISI	52	53	54	55	156	57	8	02	60	1	101		7	40	65	991	63	down or				171		73	74	75			_			181	87	83	84	8	186	87	88	68	8	191	92	93	4	9.5	961	97	86	8		Diff	ı
Dep 1	32.0	33-2	33.5	33-9	34.2	34.5	34.8	35.2	25.5	200	5	30.1	36.5	36.8	37.1	37-4	27.8	200	286	000	30.7	39.1	39.4	39.7	40.0	404	40.7	41.0	41.4	41.7	43.0	42.3	42.7	43.0	43.3	43-6	44.0	44.3	44.6	45.0	45.3	45.6	45.9	46.2	46.6	46.9	47.2	47.5	47.9	48.2	48.5	40.0	Lat	
Lat	3.56	96.4	97-4	98.3	99.3	100.2	IOI.2	102.1	103.1	104.0		104.9	105.9	8.90I	107.8	108.7	100.7	9.011	9.111		C-711	113.5	114.4	115.3	116.3	117.2	118.2	11611	120.I	121.0	122.0	122.9	123.9	124.8	125.7	126.7	127.6	128.6	129.5	130.5	131.4	132.4	I33.3	134.3	135.2	136.1	137.1	138.0	£39.0	13949	140.9	0	Dep	
	IOI	03	03	940	05	SWEETERS	CONTRACTOR OF	80	erion and	IO	MINE SE	000000000	12	13	14	15	1911	1.7	2				Marie Series	4	23	24	25	126	27	780		30	131	32	33	100000	35	1///	37	ALC: N	un discussion and	9	141	42	43	44	45	NO CONTRACTOR	47	CONTRACTOR OF THE PERSON OF TH	49	and the second	Dift	ı
Dep	9.91		17.3	17.7	17.9	18.2	18.6	18.0	10.2	10.6		6-61	20.2	20.5	20.8	21.2	21.6	0 T	7.2.T		200	7.4.0	23.I	23.4	23.8	24.1	24.4	24.7	25.I	25.4	25.7	26.0	26.4	26.7	27.0	27.4	27.7	28.0	28.3	28.7	29,00	29.3	29.6	300	30.3	30.6	30.9	31.3	31.6	31.9	32.2	24.5	Lat	
Lat	48.2	7	-	Sici	52.0	52.9	53.9	84.8	8.53	46.7		57.7	58.0	29.6	60.5	61.5	62.4	62.2	64.2	2 2	7.7	31	07.1	1.80	0.69	70.0	70.9	71.9	72.8	73.7	74.7	25.6	76.6	77.5	78.5	79.4	80.4	81.3	82.3	83.4	84.1	85.1	86.0	87.0	87.9	88.9	89.8	8006	91.7	92.7	93.6	3	Dep	ı
	115	19		4	55	56	57	00	20	9	-	-	10000			65	ALC: NO		700	200000	3	1	71	72	73	74	75	76	11	78	79	8	81	87	83	84	83	98	87	00	89	8	16	92	93	94	95	96	97	86	662	THE REAL PROPERTY.	Did	ı
Dep	00.3	00.7	0.10	OI.3	0I.6	05.0	02.3	02.6	03.0	02.3	7	03.0	03.9	04.2	04.6	04.0	04.2	96.6	0.00	200	2 4	500	00.8	07.3	07.5	07.8	08.I	08.5	∞. ∞ ∞	1.60	4.60	8.6	IO.I	10.4	10.7	11.1	11:4	11.7	1230	12.4	12.7	13.0	13.3	13.7	I4.0	14.3	14.7	15.0	15.3	15.6	10.0	?	Lat	
Lat	0000	0.IC	02.8	03.8	04.7	05.7	9.90	07.6	08.5	00.0		10.4	3	12.3	13.2	14.2	133	1.91	17.0	0 0	000	3	19.9	20.8	21.7	22.7	23.6	24.6	25-5	26.5	27.4	28.4	29.3	30.3	31.2	32.I	33.I	34.0	35.0	35.9	36.9	37.8	38.8	39.7	40.7	41.6	42.5	43.5	44.4	45.4	40.3	13	Dep	-
Diff	I	d			5	9	COMPANY OF THE PARK OF THE PAR	.00	100000000		-	1	13	13	14	15	192	12	100	1 5	4	3	71	7.7	23	24	25	50	27	300	29	30	31	32	33	34	35	36	37	300	39	9	41	42	43	44	45	46	47	20 4	49	200,000	Diff	

for 71 Degrees.

20 Difference of Latitude and Departure for 20 Degrees.

			1														a His	220					1053	5505	200.5									100	1			020					di mana		-	-	-		
Dep	85.00	6.2	6.5	6.0		2 1	88.0	7 0		60	9.3	9.6	6.6	0.3	90.06	0.16	01.3	11.7	0.2	32.3	92.7	93.0	93.3	93.7	94.1	94.4	94.7	95.1	95.4	95.8	1.96	96.4	96.0	07.6	07.8	98.2	98.5	98.8	2.66	99.5	6.66	1001	0.001	IOI.	ior.6	ioi.9	102.3	102.6	Lat
(MESISPINA)	900	Section 1	000	0 0	0 0	00	0 00	0 00	0 0	01	00	00	8	6	6	10	-		No. of Street,	7		STATE OF THE PARTY.	-		4	4	3	7	64	H	н	0	6	700	100	7	9	9	2	3	4 ,	000	2 6	2	H	0	0	श	1
at	235.9	9.0	237.7	7		•	5	4 6	2	4:	45.3	46.2	47.1	48.1	49.0	0.0	000	\$1.8	32.	53.	\$4.	55.	256.5	257.	\$8.	.59.	.60	.19	.62.	63.	.64	.05	205	.67	897	269.	170.	271.	272	273	4/4	2.76	277	378	279	280	181	281	å
	23	23	3 23	9 (0 3	2 0	3 0	* 0	31	IS	8	63 2	4	25	6 2	67 2	4	2	0 2	1 3	12 2	13 2	4 2	7.5 2	762	772	28	79 2	8	817	020	600	2000	198	87	800	68	8	01	92	30	9 6	90	97	86	66	0 1	則
	251	5	5,	3,	1	3,	٥,	٥,	2	Ų	63					19	9	9 1		7	5 27	1	3	9	0	3 27	9	0	89	7	4		4 14	4	1 6	E	4	7		40	0 F	4	00	1 2	.5	20	7	5	
Dep	68.7	1.69	69.4	09.00		200			0	7:0	72.2	72.5	72.8	73.2	73.5	73.9	74.2	74.6	74.9	75.2	75.	75.	76.	76.	77.0	77.3	77.	78.	780	78	79.	79.	79.7	000	80.	81.	.i.	i o	020	022	000	300	000	84	90	8	200	8	Fa
		20 0			5 1 V		2	0,	+ 6		10.00			-	0	10	6	_	00	2	.7	9.	9	3	न	4	33	•3	4	7	T	Q.	0 0	× 00	100	1.0	3.6	0	3	6.5	4.0	2 0	0.2	1.2	2.I	3.0	4.0	4.9	ep
Lat	188.9	189	190.8	91.	3	73.	4	2 4	2	197.	198.3	199.2	2007	toI.	202	203	203.0	204	205	206.	207	208	209.	210.	211	212	213.	214	2 I.S	216	2.57	21	219	220	18	33	22	33	2	33	227	220	230	2	23	233	23	023	
BECKE STORY	CHANGE OF THE PARTY OF THE PART	TO SHEET	MANUFACTURE OF THE PARTY OF THE	04	313	3	200	3 8	7	A STATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF T	211	10000	13	14	15	10	17	18	19	8	ZI	22	23	24	25	977	27	38	30	38	23 E	32	33	35	12	37	38	39	8	24 E	4 2	4 4		246	4	46	46	256	
			33	2		-			F		State Section	and the	7	H	4	00	4	.5	00	H	.5.2	00	4	59.5	59-9	60.2	60.5	6.09	61.2	91.19	6.19		62.0	62.3	63.6	0	64.3	64.6	65.0	5.3	66.7	6.99	66.7	7.0	7.4	7.7	68.I	68.4	Lat
Dep	51.6	\$2.0	52.	52.			33.4			54.	55	55.4	55	56	56.	56	57.3	57	57	58.1	58.5	58	59	59	58	9	હ	8	<u>5</u> ,	9	9	<u> </u>			9			10,00		9	0 4	9 9		1	9				- 1
-1	0,0	000	00		7	? '	?	2	* 6	#	·3	1.3	3.3	1:1	Į.	0.6	6.9	57.9	80	59.7	60.7	1.6	162.6	63.5	4.4	5.4	6.3	7.3	168.2	밁	70.1	0.1	0 0	172.8	4.8	15.7	176.7	177.0	78.5	179.5	180.4	00	183.2	84.	185.1	186.1	187.0	187.9	a le
3	141	143	143	144	143	4	147		4 4	110	151.	152.	153	157	15	156		The same	Z.	Storage Storage	H	116	3 16	911	5 164	2 126) IE	8 I 6	916		14	7 1	3 1	+ 2	10	7	8	16	01	H 1	1 2	0 4	. 5	19	1/1	8 I	A CONTRACTOR OF THE PERSON NAMED IN	EX PROPERTY.	
	ISI	53	53	54	3	130	57	9	24	8).	191	62	63	64	65	166	67	89	69	70	171	72	7	7	1	17	7	7	1	20	181	0 0	0 0	000	l ia	00	00 0	0	9	6	200	70	0	T O		2		91	-1
리	g soughter	34.9	4	5.0	7	6.0	0.0		2	9	0.0	38.3	8.6	30.0	30.3	9.7	0.0	0.4	0.7	1.0	1.4	1.7	42.I	3.4	2.8	3.I	13.4	3.8	14.1	4.5	4.8	15.1	5.5	6.2	9.9	16.9	17.2	47.5	47.5	20.0	46.0	40.7	40	49.0	30	50.6	51.0	51.3	Lat
مّا	34.5	34	35	35			, c	,	2	ल	3	3	6.	7		100				4	4	4		4	4	4	4	4	4	4	H	0	0 0	0 0	100	7	7	<u>,</u>	01	3	4 .	4 6	2 6	2 6	H	H	0	91	اـ
at	4.9	5.00	8.9	7.7	6.7	99.0	00.5	101-5	4.50	93.4	04.3	05.8	106.2	107.1	08.1	1000	100.0	0.01	8.11	112.8	113.7	114.6	15.6	16.5	17.	18.	613	120.3	21.2	23.2	23.	24.0	25.	26	27.	28	139.7	30.0	31:0	132.5	133	134.4	146	137	130	139.1	140.0	141	De
	6 1	6	6	6	3		2	0 0		읽	DI I	Z IC	3 10	4 IC	Z	9	7 1	8	16	O	SEP STATE	2 1	3 1	4 1	5 1	19	7 1	18	1 61	3	311	77	33	35	16	No.	38	39 1	잌	41	45	2 3	45	97	4	8		31	割
	IOI	8	0	0	3	5	0 0	ŠČ		1	11	H	1	H	H	12	H	H	1	4	121	7	7	2	7	12	2	2	0	440	7	0	4 1	\ H	14	00	H	4.0	×01	H	× 00) H	1	100	4	3	6	7	3
)ep	7.4	7.8	8.1	500	000	7.6	9.5	0.6	5	0.0	6.00	L. 1.	7.I.	0.17	12.2	22.6	22.9	7.3	23.6	23.5	24.	24.0	25.0	25.	25.	36.0	26.	26.	27.	37:	27.	200	900	20.	20.	39	30	30	30	31.	31	22	32	32	33	33	33	34	اد
It I	16.	16.	00	.7	<u>-</u>	0	9 1	3.	1	表	-3	•3	2.	I,		10	0	6	00	00	5.7	1.7	8.6	9.5	0.5	1.4	2-4	3.3	4.2	5.2	1.9	7.1	0 0	0.0	0.8	1.8	2.7	3.6	4:0	5.5	0.5	- 00	0	0.2	1.3	3.1	3.0	3	de
7	47	48	3 49	150	2	57	5.5	5 54	55	20	157	2 58	3 59	4 60	6 61	662	7 6	9	9 6	0 6	19	2 6	3 6	4 6	5 7	6 7	77	8 7	16	07	1 7	7	2	35.4	98	878	00	69	81	916	929	2 4	36	196	97	986	66	8	
Diff	5.1	53	53	5	5	5	5	5	5	ŏ	9	9	9	9	9	9	9	9	9	1	1	7	_		7	7		2	1	80	9	6	60 4	5 0	7	7.	0	3	7	0	4 1	- c	4	10	-	4	00	#	흵
Jep	0.3	100	0.10	1.4	1.7	72.I	22.4	22.7	33.1	3.4	3.8	1.70	24.4	24.8	1.30	26.6	25.00	26.2	26.5	9.90	27.2	37.6	2.70	98.3	08.6	08.0	60	00	60	10.	Io.	IO.	II.	F.Z.	12.	12.	13.	13.	13.	14.	1	1 1	IC	IS.	16.	91	16	17	L
at 1	06.	06.	8.	8.	3	0.	0.0	.5	2.5	3	0.30	63	22	.2	H	0	0	0.0	2.9	00	13	22	9.1	9.2	3.5	4:4	5-4	6.3	7.3	8.2	1.6	0.1	0.1	2.0	3.8	4.6	5.7	0.0	7.0	0.5	9.5	2	2.3	3.2	4.2	15.1	0.91	17.0	Dep
1	8	TO T	300	4 03	0	0	0 0	0		8	LIC	2 II	3 I 2	E.	H	1 9	7 1	8 I	9 I	OIL	H	7	3	4	5 2	19	7 2	100	2 6	0	1 2	23	33	9 4 4	19	7	38	39 3	9	11	27	5 4	7 7	199	47	00	49	2	
6	1000 1000 1000 1000						No.	SH II			H	H	H		F	JF			H	4	19	"	4	d	4	14	4	d	4	3	60	42	.,						1			100			700	100			21

for 70 Degrees.

Difference of Latitude and Departure for 21 Degrees. 21

		Sec.	988			986							Silve					Sec.		(Dresta)	ACCOM.			/	1									odi si		1000												533			
Dep	0.06	90.3	90.7	91.0	91.4	8.16	92.1	92.5	92.8	93,2	03.60	73.5	93.9	94.3	94.0	95.0	95.3	95.7	1.96	96.4	8.96	97.1	97.5	97.8	98.2	98.6	6.86	99-3	9.66	100.0	100.4	1001	IOI.I	101.4	101.0	102.6	102.9	103.2	103.6	103.9	104-3	104.7	105.0	105.4	105.7	1001	106.8	107.2	107.5	Lat	
Lat	234.3	235.3	236.2	237.I	238.I	239.0	239.9	240.9	241.8	242.7	2427	443-1	444.0	245.5	240.2	247.4	248.3	246-3	250.2	25 I.I	252.I	253.0	253.9	254.9	\$55.8	256.7	257.7	258.6	3	260.5	201.4	262.3	263-3	204-2	266.1	267.0	267.9	268.9	8.697	170.7	171.7	272.6	173.5	174.5	275.4	176.3	277.3	1.072	1.80.1	Dep	2000000
Die	251	52	53	54	55	256	57	58	59	9	190	107	70	03	40,	न	9	0	diam'r.	69	70	27I	72	73	74	13	276	77	78	79	8	78I	0 0	003	0 %	286	87	88	89	90	291	92	93	94	25	362	97	66	-	Dia	No. of London
Dep	72.0	72.4	72.8	73.I	73.5	73.8	74.2	74.5	74.9	75.3	10.6	13.0	70.07	70.3	70.7	77.5	77.4	77.8	78.1	78.5	78.8	79.2	79.6	79.9	80.3	80.6	81.0	81.4	81.7	82.1	82.4	82.8	83.I	83.5	84.2	84.6	84.9	85.3	85.7	86.0	86.4	86.7	87.1	87.4	87.8	88.2	88.0	89.2	89.6	Lat	Mark Sand
Lat	187.6	188.6	189.5	190.4	191.4	192.3	193.2	I94.2	195.1	196.0	107.0	2	197.9	190.0	199.8	200.7	201.6	202.0	203.5	204.4	205.4	206.3	207.2	208.2	209.I	210.0	211.0	61112	212.8	213.8	214-7	215.6	216.6	217.5	210.4	220.2	221.2	222.2	123.I	224.I	\$25.0	225.9	226.9	227.8	228.7	229.7	230.6	232.5	233.4	Dep	THE REAL PROPERTY.
割	201	03	03	04	9	300	CONTRACTOR OF THE PERSON NAMED IN	80	60	IO	11.6	1	77	13	14	न	216	17	18	19	20	221	22	23	24	25	226	27			S	231	32	33	34	226	37	300	39	40	241	42	43	44	45	246	47	49	250	Dig	
Dep	54.1	54.5	54.8	55.2	55.6	55.9	56.3	56.6	57.0	57.3	67.5	100	50.1	50.4	50.0	59.1	59.5	59.9	2.09	9.09	60.0	61.3	61.6	62.0	62.4	62.7	63.1	63.4	63.8	64.2	04.5	64.9	65.2	05.0	66.3	66.7	67.0	67.4	67.7	68.I	68.5	88.8	69.2	69-5	6.69	70.2	70.6	71.3	71.7	Lat	
Lat	141.0	141.9	142.9	143.8	144.7	145.7	146.6	147.5	148.5	149.4	100	5000	151.3	152.2	153.1	154 1	1550	155.9	156.9	157.8	158.7	1.651	9.091	161.5	162.5	163.4	164.3	165.3	166.2	1.67.1	1001	0.691	6-691	170.9	172.7	172.7	174.6	175.5	176.5	177.4	178.3	179.3	180.2	181.1	182.1	183.0	183.9	18,8	186.7	Dep	
	151	~	53	54	5.5	156	57	28	59	TO MAKE SHAPE	147	Name of Street		- Mary and	MANAGE	lol.	991			69	70	171	72	73	74	75	176	77	_				7		8 0 4	186	87	88	89	90	161	92	93	94	न्न	961	97	000	MILE STORY	Did	
Dep	36.2	36.6	36.9	37.3	37.6	38.0	38.3	38.7	39.1	39.4	800	39.0	40.1	40.5	40.9	41.2	41.6	41.9	42.3	42.6	43.0	43.4	43.7	44.I	44.4	44.8	45.2	45.5	45.9	46.2	40.0	47.0	47-3	47.7	40.0	187	40.1	49.5	49.8	50.2	50.5	50.9	51.3	\$1.6	52,00	52.3	52.7	53.4	53.8	Lat	
Lat	94.3	95.3	96.2	97.1	98.1	0.66	6.66	10001	8.IOI	102.7	1007	7.00	04.0	105.5	1000.5	107:4	ro8.3	109.3	IIO.2	III.I	112.1	113.0	113.9	114.9	115.8	116.7	117.7	118.6	119.5	120.5	121.4	122.3	123.3	124.2	125.1	12.7	127.0	128.9	129.8	130.7	131.7	132.6	133.5	134.5	135.4	136.3	137-3	139.1	140.1	Dep	
	IOI	02	03	04	05	901	08707210990	80	60	IO		(September)		ensumille	14	Non-con-	niekalem	17	201	161	20	121	22	23		25	9				2012	н	32	33	34	136	37	38	39	40	141	42	*43	44	45	146	47	49	STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET,		
Depl	18.3	18.6	19.0	19.4	19.7	20.I	20.4	20.8	2.I.I	21.5	10	41.9	7.7.7	22.0	22.9	23.3	23.7	24.0	24.4	24.7	2,5.I	25.4	25.8	26.2	26.5	26.9	27.2	27.6	2000	28.3	28.7	29.0	29.4	29.7	30.1	200	4 E-2	31.5	31.9	32.3	32.6	33.0	33.3	33.7	34.0	34.4	34.8	25.5	35.8	Lat	I
RESIDE	9	48.5	49.5	50.4	51.3	52.3	53.2	54.I	55.1	56.0	10	7	70	0	29.7	00.7	9.19	62.5	63.5	64.4	65.3	66.3	67.2	68.I	1.69	70.0	10.0	71.9	00	7	74.7	9	76.5	77.5	70.4	80.2	81.2		83.1	84.9	84.9	85.9	86.8	87.7	88.7	9.68	80	92.4	93.4	Dep	
	.51		53	54	5.5	56	57	58	59	9	14	1 7	707	03	0,4	श	99	67	89	69	70	71	72	73	74	75	16	77	78	79	8	81	27	83	4 %	86	87	88	89	90	16	92	93	94	95	96	97	000	TOO	記	l
Dep	00.4	00.7	OI.I	OI.4	8.10	02.2	02.5	03.0	03.2	03.6	0000	7.00	04.3	04.7	05.0	5:4	05.7	06.1	06.5	8.90	07.2	07.5	6.40	08.3	08.6	0000	09.3	2.60	10.0	10.4	10.8	II.I	11.5	11.8	12.5	T2.0	13.1	13.6	14.0	14.3	14:7	15.1	15.4	15.8	16.1	16.5	17.2	17.6	17.9	Lat	
Lat	6.00			03.7	04.7	05.6		07.5	-	00.3	- Carrier		7.11	12.1	13.1	31	14.9	13.9	16.8	17.7	18.7	19.61	20.5	21.5	22.4	23.3	24-3	25.2	26.I	27.I	28.0	28.9	29.0	30.9	32.7	22.6	34.5	35.5	36.4	37.3	38.3	39.2	40.I	41.1	43.0	42.0	43.9	45.7	46-7	Dep	
	1	લ			5	9	7	00	6.	IO	1:	1 0	7.7	13	14	15	91	I7	200	61	20	2.1	22	23	24	2.5	26	27	700	29	श्र	31	32	33	35	26	37	38	39	40	41	42	43	44	45	46	47	49	50	סים	1

to 68 Degrees

22 Difference of Latitude and Departure for 22 Degrees!

7	0	4	00	e	*	0		, 6	7	,	11	00	199	No.	77		.از.	9	o	4	00	-	T	7 4	50		0	01	4	00	H	35	6	43	9	0	4	00	7	*5	6	43	9,	0	4	00	r.		6	erj.	9	o ·	11	T T
De	94	4	94	95	95	0	90	90		6	16	97	00	080	00	6	99.	-66	100.	100.	IOO.	IOI.	į	1	101	102.	102.	103	103	103	104	104	104	Ios.	105.	106.	106.	106.	107.	107.	107.	108.	108	109.	100	100.	IIO:	JIO.	IIO.	III	III.	112.	112	La
Lat	232.7	233.7	234.6	235.5	236.4	237.4	218.4	2.20.2	4 (0)	1000	444:1	242.0	242.0	242.0	0	444.0	245.7	246.6	247.6	248.5	240.4	250.2		40.00	252.2	253-I	254.I	255.0	255-9	256.8	257.8	258.7	259.6	260.5	261.5	262-4	263.8	264-3	265.2	266.I	267.0	268.0	268.9	269.8	270-7	271.7	272.6	273.5	274.5	275-4	276.3	277-2	278.2	Dep
Dift	25 I	7.5	53	5.4	5.5	256	67	200		25	8	261	62	6.2	3.7	\$,	श	266	67	89	9	70		7/7	72	73	74	7.5	276	77	78	79	8	281	82	83	84	85	286	87	88	89	06	201	92	93	94	95	296	.97	86		300	Dia
Dep	75.3	75.7	76.0	76.4	76.8	77.2	77.0	77.0	101	000	7:07	79.0	70.4	70.8	000	000	80.5	80.9	81.3	81.7	82.0	82.4	0 00	0 %0	63.2	63.5	83.9	84.3	84.7	85.0	85.4	85.8	86.2	86.5	86.9	87.3	87-7	88.0	88.4	88.8	89.2	89.5	89.9	90.3	90.7	91.0	91.4	91.8	92.2	92.5	92.9	93-3	93-7	Lat
Trat	186.4	187.3	188.2	1.681	190.I	0.191	IQI.0	102.0	0	19.50	174.7	195.7	106.6	107.6	1001	2006	177.4	200.3	201.2	202.I	203.I	204.0	0.00	0	2000	2000	207.7	208.0	200-5	210.5	\$11.4	212.3	13.3	114.2	115.1	0.913	217.0	217.9	8.812	2.612	220.7	221.6	222.5	223.5	224.4	225-3	226.2	227.2	228.1	229.0	229.9	230.0	231.0	Dep
	20I	02	03	40	05	300	7	-			श	2II	12			4 :	15	316	17	18	OI				7 7	2,3	24	25	326	27	100	29	30	231	32	33	34	35	236	37	38	39	40	24I	42	43	44	45	246	47	400	49	250	Diff
Dep	9.95	6.95	57.3	57.7	58.1	58.4	8.8	50.2	200	0.60	59.3	60.3	60.7	61.1	1 19	70.77	01.0	62.2	62.6	62.0	63.2	63.7	1	,	04.4	04.0	05.5	02.0	62.0	66.3	000.7	67.I	67.4	67.8	68.2	9.89	68.0	69.3	69.7	70.1	70.4	70.8	71,3	71.5	71.9	72.3	72.7	73.0	73.4	73.8	74.2	74.5	74.9	Lat
Lat	140.0	6.04	£41.9	142.8	143-7	144.6	145.6	46.5	144.	0	140:4	149.3	150.2	I G D. I	1.001	1000	0.00	153.9	154.8	155.8	156.7	157.6	168.6	2	6.66-	400.4	101.3	102.3	163.2	1.40	105.0	10000	106.9	167.8	8.891	1.691	170.6	171.5	174.5	173.4	174.3	175.2	176.2	177.1	178.0	178.9	8.641	180.8	181.7	182.7	183.6	184.5	185.4	Dep
E I	ISI	52	53	54	55	156	63	, 00		200	-commu	ILOI	62	2000000			S	100	67	89	69	NAME OF STREET	17-4000M		7	7.3	74	75	176	77	781	00029-0		181		epopolis	DATE OF SECURITY	and the same of	MINE COMM		88	68	90	161	92	93	94	9.5	961	16	ALC: NAME OF			Diff
Dep	37.8	38.2	38.6	39.0	39-3	39.7	40.1	40.6	40.00	1	1	41.6	42.0	42.3	42.7	7.0%	4301	43.5	43.8	44.2	44.6	45.0	16.34	2.0	45.	40.1	40.5	40.8	47.2	47.0	47.9	48.3	7200000	100		49.8	50.2	50.6	50.9	51.3	51.7	52.I	\$2.4	52.8	53.2	53.6	53.9	54-3	54-7	55.1	55.4	55.8	50-2	Lat
rat	93.6	94.6	95.5	96.4	97.4	98.3	99.2	1001	TOT			102.0	103.8	104.8	105.7	3,40		107.0	108.5	109.4	LIO.3	LII.3	112.2	TTUL	1.0.1	0	113.0	115.9	110.8	117.8	118.7	119.0	120.5	121.5	122.4	123.3	124.2	125.1	176.I	127.0	128.0	128.9	129.8	130.7	131.7	132.6	13333	134.4	135-4	136.3	137.2	138.1	139.1	Dep
	IOI	07	03	40	05	901	07	COUNTY N	and the same	and the last of	40.0	III	12	13	-		7	OII	17	18	19	20	PERSONAL PROPERTY		7 7	63	24	man of the	126	27			38	131		33	34	35	136	37	00	39	40	141	43	43	44	4.5	146	47	48	49	3	Did
ne b	19.1	19.5	19.9	20.2	20.6	21.0	21.4	21.7	20.1	20.00	200	22.9	23.2	23.6	24.0		1	24.7	25.I	25.5	25.8	26.2	9.92			0./,	1.67	100	20.5	20.0	20.5	0.62	000	30.3	30.7	31.1	31.5	31.8	32.2	32.6	33.0	33.3	33-7	34.1	34.5	34.8	35.2	35-5	36.0	36.3	36.7	37.1	37.5	Lat
rat	17.3	18.2	1.64	50.1	51.0	\$I.9	52.0	300	4.80	,	2	9.95	57.5	8.4	50.2	2	3	2.10	62.I	53.0	0.40	6-40	100	6 4 9	2		0.00	5.6	20.2	7.I.4	72.3	13.2	74.2	75.E	0.9	17.0	17.9	8.8	79.7	30.7	81.6	82.5	83.4	844	85.3	86.2	87.2	88.1	89.0	6.68	6.06	8.16	92.7	Dep
	SIL	52	53	34	55	56	57	85	80	60	3	199	62	63	64	,	3	- 100	62	89	69	70	1;			13	74	75	70	77	78	79%	8	81	82	83	84	85	98	87	88	68	90	16	92	93	94	9.5	96	97	98	99		Diff
Dep	4.00	7.00	OI.I	01.5	6.10	02.2	02:6	03.0	02.0	200	12:5	04.1	04.5	04.0	06.2	3		0000	06.4	2.90	07.I	07.5	01.0	100	7.00	0.00	0.60	99.4	09.7	IO.I	ro.5	10.9	11.2	9.11	12.0	12.4	12.7	13.I	13-5	13.9	14.2	14.6	15.0	15.4	15.7	101	16.5	16.9	17.2	17.6	18.0	18.4	10.7	Lat
Lat	6.00	6.10	02.0	03-7	04.6	05.6	96.5	07.4	08.3	3	2	10.2	ir.	12.I	12.0	100	73.7	14.8	15.8	16.7	17.6	18.5	1 3	27.0	40.4	41.3	22.3	23.2	24.1	25.0	20.0	26.9	27.8	28.7	29.7	30.6	31.5	32.5	33-4	34.3	35.2	36.2	37.1	38.0	38-9	39.9	40.8	41.7	42.7	43.6	44.5	45.4	40.4	Dep
Ditt	1	a	8	4	3	9	63	-00	0	7.0		11	12	13	LA		12	10	17	18	19	20	12	: 6	*	57	74	25	20	27	20	29	잃	31	32	33	34	35	36	37	38	39	9	41	42	43	44	45	46	47	48	49	20	Diff

for 68 Degrees.

-																			N.				1.																				ı										
Dep	08.1	80	88	00	9.00	100.0	100.4	100.8	ToI.	101.6		102.0	102.4	102.8	103.1	103.5	103.0	104.1	104.7	TOT.	1001		105.9	100.3	1001	107.1	107.4	107.8	108.2	108.6	100.0	100-4	109.8	110.2	110.6	0.111	1113	111.7	112.1	112.5	112.9	13:3	13.7		14.5	116.9	1	200	116.4	16.8	117.2	Lat	
Lat	21.0	22.0	33.0	00	34-7	235.6	36.6	37.5	28.4		26	40.5	41.2	42-1	43.0	43.9	44.9	45.8	46.7	47.6	0		3	50.4	51.3	53.2	53.I	54.I	55.0	55.0	20.8	7	258-7	9.6	600.5	4	3	.3	12	H	12,455	650	02.0	0.00	1.0	7.1	1	3.5	74.2	75.2	16.2	Dep	Degrees
Did	2.6.1.2	6.2.2	5.3.2	5.4.2	55.2	2562	57 2	582	50 2	6002	00,000	707	02 2	03/2	64 2	65 2	266 2	67 2	68 2	600	2000		100	72 2	73 2	74 2	25 2	276 2	77.3	787				200	4		85.2			88			4	3	95 40			4000	082	99 2	300 2	Dift)egi
Dep	78.€	78.0	79.3	70.7	80.I	80.5	80.0	81.3	81.7	82.0	0	4.4	62.6	83.2	83.6	84.0	84.4	84.8	85.2	85.6	200	96	000	200.7	87.1	87.5	87.9	88.3	88.7	89.1	5.6%	60.60	90.3	9006	91.0	4.16	91.8	92.2	97.6	93.0	93.4	33.0	4.5	24.5	94.9	0.5.7	7,50	200	0.90	97.3	97-7	Lat	7
Lat	185.0	8.0	186.9	87.8	88.7	9.681	190.5	20161	192.4	102.2	200	194.4	195.1	1061	197.0	197.9	8.861	199.7	200.7	20I.6	202.		***	704-4	205.3	20002	207.1	000000	2000	209-9	210.8	7777	OF SHEET	213.0	214-5	15.4	10.3	217.2	18.2	219.1	20.0	5.0	2000	0.77	24.6	25.5	190	27.4	28.3	29.2	230.I	Jep	for 6
Did	201	NUMBER OF	NAME OF STREET	MAGGINE N	WYCKIN	P. Anne	07	10000	CONC.	Andrews .		1	12 1	13 1	14 1	15 1	216 1		. 18 2					3		4	201	9	1			018		32 2		G.	COL	9	1		39 2	9	241 2	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	43	4: 2	1	440	48 2	49 2	250 2	Dift-1	J
Dep	60.0	50.4	59.8	60.2	9.09	6009	61.3	61.7	62.1	62.5	200	6-70	03.3	63.7	64-1	64.5	64.0	65.2	65.6	66.0	7.99	o yy	0 0	07-2	02.0	0.00	68.4	8.89	2-69	69.5	6-69	70-3		71.1		71.9	3	74.7	73.I	73.5	73.8	74.2	74-0	75.0	4.00	26.2	10,7	2007	17.4	77.7	78.1	Lat	
Lat	30.0	130.0	140.8	41.8	42.7	43.6	44.5	45.4	46.4	47.3	3	4000	49.1	150.0	151.0	151.9	152.8	153.7	154.6	9.331	93000		1000	50.3	159.2	100.2	IOI.	E10.74	C 000		164.8	105-7	9.991	67.5	108.5	169.4	70-3	71.2	72.1	73-I	74.0	74-9	73.0	70-7	100	70.6	200	181	182.2	83.2	184.1	Dep	
DICE	Ter	62	53	A COL	55	156	57	000	40	9	1	70		STORES COMMO	4	65]	1991	NAME OF TAXABLE PARTY.				-	-	72	73	74 1	73	176 1					1000000		-		8	1861	87 H	88	89	3	161		93	740	3	2 6	180	1 00	-	I I	
Dep 1	20.€	20.0	40.2	40.6	4 I.O	41.4	41.8	42.2	42.6	42.0	2	43.4	43.8	44.1	44.5	44.9	45.3	45.7	16.1	46.0	16.0		4/.3	47.7	48.I	48.4	48.8	49.2	49.6	20.0	50.4	50,8	51.2	51.6	52.0	52.4	52.7	\$3.I	53.5	53-9	54.3	54-7	55.1	55.5	55.9	50.5	7.00	57.0	400	500	58.6	Lat	
Lat	01.0	03.0	948	06.7	66.7	97.6	98.5	4-66	100.3	IOI.2		102.2	103.I	104-0	104-9	105.9	8.901	107.7	108.6	TOO.	110.5		4.74	112.3	113.2	114.1	115.1	0.911	6.911	117.8	118.7	179.7	20.6	21.5	22.4	23.3	24-3	25.5	26.1	27.0	27.9	28.9	129.8	30.7	31.0	32.60	7.25	34.4	T26.2	37.2	138.1	Dep	
Diff	IOI	020	03	9	90	901	07	80	da sedicion	STATE OF THE	-	111		_	14		116		18	0					23					281		MHG-RI	131 1	32 1	33 1	34 1	35 1	1361	37 1	38 1	39.1	9	September 1	42	43	4 4 4	1	40	100	40	of Marie Williams	Diff	
Dep	10.0	20.3	20.7	21.1	21.5	21.9	22.3	22.7	23.I	23.4	000	43.0	24.3	24.0	25.0	25-4	25.8	26.3	26.6	27.0	27.2	3	1.00	7.0.7	20.5	28.9	29-3	29.7	30.I	30.5	30.9	31:3	31.6	32.0	32.4	32.8	33.2	33.6	34.0	34-4	34.8	35.2	35.0	35-9	20.3	27.4		37.5	30.0	200.7	39.I	Lat	
E	46.0	47.0	00	49.7	50.6	31.5	52.5	53.4	54.3	56.2	- 7:	200	57.1	500	58.9	59.8	8.09	61.7	62.6	62.5	7	F1 -	4,5	00.3	07.5	1.90	00.60	10.0	20.9	71.8	72.7	23.0	74.6	75.5	70.4	77.3	78.2	79.5	80.1	81.0	6.10	02.0	03.00	04.7	05.0	200	4.00	000.4	200		92.0	Dep	10
Trial	13	23	53	54	5.5	95	57	00	65	90	1	7 .	03	63	64	65	99	69	89	9	-	-	9 (12	73	74	25	94	17	18	20	श	N 0	000	83	*	-	9	7		68	थ	16	2 6	22	* č	श्र	2 5	× 0	0	18	TE S	land
Dep	00.4	00	OI.2	31.6	07.0	02.3	02.7	03.1	03.5	03.0		24.5	04.7	Oj.1	05.5	6.50	06.3	9.90	07.0	07.4	07.0	2	700	000	0.60	00.4	8.60	10.2	10.5	10.9	11.3	11:2	12.I	12.5	12.9	13-3	13.7	14.1	14.5	14.8	15.2	25.0	10.0	407	17.0	17.6	200	200	00	1.61	19-5	Lat	60
Lai	0000	01.8	02.8	03.7	04.0	05.5	06.4	07.4	08.3	00.2	1	3	11.0		12.9	13.8	14.7	15.6	9.91	17.6	18		200	20.3	21.2	22.I	23.0	23.9	24.9	23.8	20.7	27.0	28.2	29.5	30.4	31.3	32.2	33.I	34-1	35.0	35.0	30.0	37.7	30.7	200	AT.A		44.0	44.2	45.1	46.0	Dep	
SIR.		0	er.	9 4	1	100	7	00	0	IO		1	L2	13	14	15	91	I7	1.8	TO	200	113	4 6	n de	23	24	3	36	2	77	_	01	31	32	3	34	35	36	37	300	39	9	41	4 .	45	7	भे	4 5	1 4	49	So	193	

24 Difference of Latitude and Departure for 24 Degrees.

													Sec.				100		(April				e Pros													-	-			-	of Street	100.00	ethral.	and the last	-	reproje-	W ^a tes	PERM	074	~		44	× .	2	01	ALC: N
Dep	T02.1	102.5	102.9	103.3	103.7	104.1	104.5	104.9	TOK. 2	106.7	1	1001	9.901	107.0	TO7.4	200		108.2	108.6	E09.0	100.4	100.8		110.2	110.6	O'III	III.4	111.8	12.					113.9	114.3	114.7	III	IIC	TTEO	1						118.3	2.811	119.2	119.6	120.0	120.4	120.8	121.2	The same of	122.	Lat
Lat	220.3		MINISTER N			100 2500	4.0	5.7	9.9		2	230.4	239.3	240.3	241.2	-		243.0	243-9	244.8	245.7	246.6		247.0	248.5	249.4	250.3	251.2	202.1	1000		454.0	254	255.0	256.7	257.6	258.5	-	-	10	4 4	4 6	-	7	26		200-7		_	269.5	270.4	7271.3	\$ 272.2	27	274.1	H Dep
Dift	ÇI 2			54	55	56	57	58	02	9	ŀ	707	62	63	64	39.	गः	200	67	89	69	70	1	271	72	73	74	75	18		77	70	79	8	281	82	83	84			1	8		5 6	1,	7			94	6	296			66	300	
Dep 1D	31.72	32.2	32.6	83.0	33.4	83.8	84.2	84.6	85.0	8.7		0.50	86.2	86.6	87.0	87.	*	87.8	88.3	88.7	89.1	80.5	7	6-69	90.3	90.7	1.10	91.5	oT.o	200	92.3	7.76	93.1	93.5	93.9	94.4	94.8	95.2	9.50	0.00	7 90	200	200	416	200	90.0	90.4	98.8	99.2	99.0	1000	100.5	100.9	IOI.	ioi	Lat
850390.	181.6		03000	6.4	1000	77						192.7	193.7				=	3	198.2	1		0 TO C		201.9	202.8	103.7	04.6	2000	3 90	5	4.07.4	200.3	2000	210.I	211.0	211.9	212.8	213.8	214.7	13	213.0	0.010	1010	410.3	77.67	220.2	221.1	222.0	222.9	223.8	224.7	225.6	226.5	4	228.4	Dep
Dift 1		900004348	COLUMN	04 118	PARCONAL S	CHARMS	SCHOOL SECTION	08 I	00	-	m Carr	ZIII	12 I	ITI	14	1 1	<u>:</u>	101		181	192					23	242	25.	36	2 4 4	70	CONTACTOR		30	231	32	3		v	140		200			4		43	43	44	45	246	47	48		250	Dift
Dep D	PERMIT				1000	14			100				6.59	6.3	6.7			67.5 2	6.49	68.3	58.7	1 09		69.5 2	20.07	70.4	70.8	71.2	4.6	0 1	72.0	72.4	72.8	73.2	73.6	74.0	74.4	74.8	75.2	20.0	10.07	1 4 4	26.07	No. 1	11.3	77.7	78.1	78.5	78.9	79-3	79-7	80.1	80.5	80.0	81.3	Lat
it D	37.0						1.4 6	1.3 6	4.2 6		1	0 1./	Elec-	48.0 6					152.6	(III)			1	7	н	0	0	. 4.4			20		163.5	164.4	165.3	166.3	167.2	168.1	0.091	1000	6660	2 4 4 4	/::/	/4./	73.0	74.5	75.4	70.3	77.2	18.1	0.64	80.0	180.9	181.8	182.7	Dep
E	2		130.8		-		7 14	3 144	LAN	1		14	H	-		334				68 IS	69 15			1 15	2 157.	3158			11/2		7 10	VO IC	79 It					84 1			_	1 1	1000	1 60	31,	1 16	1 76	93 I	94 I	95 1	196	97 1	×	CONTRACTOR OF THE PARTY OF		Diff
Dia	171	SCHOOL STATE	b-135a		55	H		1		200		H		5 63				2 I 166					g u	2 17	9	0	4	.00	16	7	7				H				1 250	10				30.5			57.0	2 >	50.0	30.0	+	000	00.2		0.1	Lat II
Dep	41.1	41.5	41.0	42.3	42.7	43.1	43.5	43.9	44.2		-	45.I	45.6	46.0	46.4	2 4	4	47.2	47.	48.	48.	8 8		49.2	49.6	50.0	50.4	800	1	•	51.7				53.3	53	54.I	54.5	\$4.0	1	23	25.			200	57			50	55	1 59-	3 3	2	0 1		1
Lat	02.0	02.2	1.70	0.50	95.0	8.96	97.7	98.7	9.00	7.00	3	IOI.4	102.3	102.2	1001	1	1001	0.901	6.901	107.8	108.7	7 001	2	IIO.5	III.4	112.4	II 2.2	II4.2		113.1	I 10.0	110.9	117.8	118.8	119.7	120.6	121.5	122.4	122.	100	1	700		0./41	14/19	120.0	129.	130.0	I3I.	132.	133.	134.	135		137.	Dep
ig	10	Total Control	0	04	05	190	100	80	80	4000	SCOOLS AND ADDRESS OF THE PARTY	I	12 1	131	1	-		913	17	18	IO					23		2.5	or Total Care	1		70		30	131	32	33	34	35	1 26	100	200	, ,	3,0	1:	141	47	43	44	4.5	146	47	4 .	4 ;	श्री	
Jepi	D.7 I	Joseph Committee of the	9.1	2.0	2.4	2.8 I	3.2	3.6	0		410	4.8	25.2	35.6	26.0	,	10.4	8.93	27.3	27.7	28.I	200	0	28.9	29.3	29.7	30.I	30.5	100	20.00	31.3	31.7	32.I	32.5	32.9	33.3	33.8	34.2	34.6	25.0	25.4	25.8	26.0	3,46		3/0	37.4	37.0	30.2	3000	39.0	39.4	39-9	40.2	10.	Lat
Lat	6.62	4	00.0	0.3 2	0.2	I.2 2	2.1 2	53.0 2	62.01	000		55-7 2	56.6 2	19.43	000	rigge.		60-3	61.2	62.1	63.0		NO.	00	65.8	66.7	67.6	4	y oy	100	70.3	71.3	1	73.1	74.0	74-9	75.8	76.7	77.6	18.6	30.0	80.4	81,	8,5	8	0.50	04.0	050	05.0	000	87.7	288.0	-	THE REAL PROPERTY.	7/1	t'Dep
Oift 1	15	52	S	54	555	\$66	57	58	, 0	CAPACIDA	1	OI	62	63	7.9	7	3	-	67	89	9			71	72	73	74	7.5	196	2 1	707	0/	79	8	81	82	83	84	85	98	87	000	8	6		3 6	,	3	7 6	2	26	6	5, 6	7 79	116	
Depi	18	000	OT12	9.10	07.0	02.4	8.20	03.3	200	1.50	04.1	04.5	6.40	05.2	200	1.50	1100	06.5	6.90	07.3	07.7	000		08.5	08.0	09.4	8.00	10.2	10.6		11.0	11.4	II.8	12.2	12.6	13.0	13.4	13.8	14.2	14.6	STE	TEST	STE	176	7. 7.	2 4 5	-/-	317	17.	100	018	9 19.	610	7 20	Mark Street	pl Lat
Lat	0000	200	02.7	3.7	4.6		06.4	07.3	08.0	1 00	11/3	10.0	LILO	11.0	000	1	?	14.6	15.5	16.4	17.4	18.3	2	19.2	20.1	2I.0	21.0	22.8	22.8		44-1	25-0	20.2	MANAGE N	1 28.3	29.2	30.I	1 31.1	\$ 32.0	6 22.0	7 22	34	25.0	26.1	200	1 3/	200	3.0%	4 .	5	0 42.	7 42-	0 43	0 44.0	-	III Dep
Dift	1	1		7		9	,	.00	•	1	श	11	12	TI	? :	1 :	न	91	117	18	IO	200	1	21	22	23	2.4	25	100	1	7	77	22	위	3	3	33	3		1					1	4 .	4 .		4	41	N	S. C.	1		200	7,

for 66 Degrees.

Difference of Latitude and Departure for 25 Degrees. 25

-		ter y	-	-	00.1	2	2	0	25	0	100	7		7	-	1 -	- 00		7		1	-		~~	-	75		-	7	33	100	2	2	0	-	~	~				_	-		-			=	3		
Dep	106.1	106.	106.0	107	107.	108.2	108.	100	100	1000.	IIO.	IIO.	III.	111.	112.0	112.	112.8	II 2.	113.	114.	114.	114.0	115.4	115.8	116.2	116.	117.	117	117.0	118.	118.8	119.2	119.6	120.0	120.4	120.9	121.3	121.7	12201		143	122.8	124.2	124-7	125.	125.	125.9	126.4	126.2	Tat
Lat	227.5			230.2		0	232.9	233.8	234.7	235.6	236.5	237.5			240.2	41.	242.0	42	43.8	44.7	245.6	0	SECTION AND ADDRESS OF	248.3	40		7 8	5.2	52.	253.8	254.7	55.	256.3	57.	3	201	0	01.	6-102		7.502	66.5	2 2	67.4	68.3	260.2	270.1	271.0	271.9	Dep
Diff	241	chapped.		54		256	57		- Charles	9					-		67	Marie Property		ALC: NO.	271	7	73	74	75	276	1	700	79		281	CALIFOCAL STREET		% 4 0	50	200110	CONTRACTOR	No. of Concession,	articular tares	011	1 0	0 2	2 4	+ 5	19		-00		300	Diff
Dep	84.0	85.4	85.8	86.2	86.6	87.1	87.5	87.9	88.3	88.7	89.2	89.6	0.06	90.4	000	91.3	OI.7	02.I	92.5	93.0	03.4	03.8	04.2	04.7	0 5.I	95.5	0.50	4.90	96.8	97.2	97.6	98.0	98.5	6.86	99-3	2.66	100.2	100.0	0.101	0 10	0.101	102.7	102.1	103.5	104.2	104.4	104.8	105.2	105.7	Lat
Lat	182.2	183.1	184.0	184.9	185.8	186.7	187.6	188.5	189.4	190:3	191.2	192.1	193.0	193.0	194.0	195.8	106.7	107.6	198.5	199.4	200.3	201.2		203.0	203.0	204.8	205.7	206.6	207.5	208.4	2002	210.3	21112	12.1	13.0	213.9	0	15.7	0.017	300	4 (220-2	2.2.T. T	222.0	22.	225.0	44	225.7	226.6	Uep
Dift	20I	300000	03	-			00		_	2	211	12	13	4			1		6		221	4	33	4		9	1		29	-	H	32	3	4	Market Committee					11	_	44	2 <	4	246	47	4 4	4	250	
Dep	63.8	64.2	64.7	65.1	65.5	62.9	66.3	2.99	.67.2	67.6	68.0	68.5	68.0	69.3	69.7	70.2	70.6	71.0	71.4	71.8	72.3	72.7	73.I	73.5	74.0	74.4	74.8	75.2	75.6	76.1	16.5	76-9	77.3	77-8	78.2	78.6	79-0	79.4	79.9	5.00	000.7	81.6	0	82.4	82.8	822.2	83.7		84.5	Tar
Lat	136.0	137.8	138.7	139.6	140.5	141.4	142.3	143.2	I44.I	145.0	145.9	146.8	147.7	. 4	200	I 50.4	I CT.A	I 52.2	153.2	I54 I	166.0	155.0	156.8	157.7	158.6	150.5	160.4	161.3	162.2	163.1	164.0	164.9	165.9	166.8	167.7	168.6	169.5	170.4	171.3	7 / 110.2	173.1	174.0	0	176.7	177.6	178.5	179.4	180.4	181.3	Dep
Diff	ILI	52	53	54	DESIGNATION OF	156	57	20	59	8	_	62	-	4	-	-	_		6				73	74	_	or distribution		78/	6	100000000000000000000000000000000000000	181	73		\$	05	981		800	60	भ	161	3 6	2 2	20	106		98		200	
Dep	42.7	43.I	43.5	44.0	44.4	44.8	45.2	45.0	46.I	46.5	46.9	47.3	47.8	48.2	48.6	40.0	40.4	40.0	50.3	50.7	SI.I	\$1.6	52.0	52.4	\$2.8	53.2	52.7	54.I	54.5	54.9	55.4	55.8	56.2	56.6	.57.I	57.5	57.9	58.3	50.7	59.4	59.0		3 9	61.3	61.7	62.1	62.5	630	63.4	Lat
Lat	91.5	92.4	93.3	94.2	95.2	1.96	97.0	97.9	98.8	99.7	100.6	IOI.5	102.4	IO3.3	104.2	1.501	106.0	106.0	107.8	108.8	100.7	110.6	III.	112.4	113.3	114.2	1	0.911	0.911	117.8	118.7	9.611	120.5	121.4	122.4	123.3	124.2	125.1	120.0	6 071	127.0	1007	100.5	131.4	122.2	122.2	134.1	135.0	135.9	Dep
Dift	IOI	03	03	04	05	901	07	80	60	Io	III	0.007.0		D-1378A	S2811203	911	1	10000000	and the last		H	~	64	7		19	1.1	78%	0			73	.33	4			10	Contract of the Contract of th		21;	NINGGE	7 4	Distance.	45	146	47	48	THE RESERVE	150	
Dep	9.13	22.0	22.4	27:8	23.2	23.7	24.I	24.5	54.0	25.4	25.8	26.2	26.6	27.0	27.5	27.0	28.3	28.7	20.5	29.6	30.0	30.4	30.8	31.3	31.7	32.I	22.5	33.0	33-4	33.8	34.2	34.7	35.I	35.5	35.9	36.3			37.0	2000	30.0	30.0	20.7	40.I	40.6	4I.O	41.4	41.8	42.3	Lat
Lat	46.2	47.1	48.0	48.9	49.8	30.8		52.0	53.5	54.4	55.3	56.2	57.I	58.0	58.9	20.8	60.7	1.6	~		64.3	65.3			68.0	689	60.8	70.7		72.5	73.4	74.3	75.2	1.92	77.0	77.9	78.8	79.0	00.7	01.0	02.5	24.7	8	86.1	87.0	87.0	000	89.7	90.0	nebi
Did	5.1	5.2	53	4	5	9	57	50	59	8	19	62	63	64	65	99	62	89	69	70	71	72	7.3	74	75	76	77	7%	79	80	81	82	83	84		98	82	8 6	60	3	1,6	7,0	0.4	95	90	07	98	6	100	
Dep	00.4	0000	01.3	01.7	02.I	02.5	03.0	03-4	03.8	04.2	04.6	0.50	05.5	6.50	06.3	8.90	07.2	07.6	080	08.5	080	00.3	00.7	10.1	10.6	II.0	11.4	11.8	12.3	12.7	13.1	13.5	13.9	14.4	14.8	15.2	15.0	1.01	10.5	10.7	5./-	18.2	18.6	19.0	TO.A	10.01	20.3	20.7	21.1	Lat
Lat	00.00				04.5								00	12.7		1000	I C. A	16.3	4		10.01	19.0	20.00	21.8	22.7	23.6	24.5	25.4	26.3	27.2	28.I	28.0	29.9	30.8	31.7	32.6	33.5	34.4	35.3	5000	3/04	30.0	20.0	40.8	41.7	42.6	43-5	44.4	45.3	Dep
Dift	H			4			7		ő	IO	II	IZ		-	1.5	_	-	18	61		21	22	23		25	26	27	78	29	30	31	32	33	34	35	30	37	30	3,9	41;	4 5	7 7	4.4	45	46	47	48	49	သို့	

for 65 Degrees.

		op.																																	4.5					4			1. 12		10014	Service.	614					
Dep	IIO.O	JIO.	IIO.0	rii.4	8.111	112.2	112.7	113.1	II 2.5	ILAO		114.4	114.9	115.3	115.7	116.2	9.911	II 7.I	117.6	117.0	118.4	8.811			1.67	1,00	120.0	121.0	121.4	121.9	122.3	122.8	123.2	123.6	124.1	124-5	124.9	125.4	125.8	126.3	126.7	127.1	127.0	128.0	120.5	120.0	56	129.8	130.4	131.1	131.5	Lat
Lat	225.6			228.3	229.2	230.I	231.0	231.9	222.8	222.7	7.00	234.0	10			238.2	239.I	240.0	240.0	2.4 T. S	242.7	242.6	240	244	445.4	440.3	247.2	248.I	246.0	249.0	250.8	251.7	252.6	253.5	254.4	255.3	250.2	257.I	258.0	258.9	259.8	260.7	201-6	202.4	203.3	204.2	1	2000-0	267 8	268.7	269.6	Dep
Diff	2 C.I				55	256		Market Co.	202	200	or item	2000 A	ESCOPIS	63	64	65			000	9	70,	1:	1/1	7	?:	74	75	276	77	78	79	8	281	87	003	84	85	286	87	80	89	위	291	92	93	\$ 2	3	290	97	8	300	Diff
PARTY.		W.	80.0	89.4	89.9	90.3	90.7	9I.2	0.T.6	02.1		92.5	6.26	93.4	93.8	94.3	94.7	04.1	9.20	0.90	006.4	90	200	2/6	0.00	90.5	98.0	1.66	99.5	10001	100.4	100.8	IOI.3	101.7	IO2.I	102.6	103.0	103.5	103.9	104.3	104.8	105.2	105.1	1.901	100.5	107.0	4./01	107.8	100.3	100.2	109.6	Lat
Lat	180.7	181.6	182.5	183.4	184.3	185.2	186.1	187.0	187.8	188.7	100	109.0	190.5	191.4	192.3	193.2	194.1	10.0	105.0	106.8	107.7	108.6		277.0	4 5	201.3	207:5	203.1					UDPAYER	ar Spring	4	3	211.2	212.1	213.0	213.9	214.8	215.7	210.0	217-5	410.4	220.0	***	221.I	922.0	223.8	224.7	Dep.
Dift	201	ASSESSED						80				711	12	13	14	IS	216		00	-	STATE OF THE STATE OF	-		3 6	and the same	77	-	226	27		29	30				34	35	236	3.7	38	39	위	24I	42	43	44	4	240	47	40	250	Diff
Dep	TERM!		67.1	67.5	68.0	68.4	8.89	69.3	60.7	70.1	-	200	71.0	71.5	71.9	72.3	72.8	72.2	72.7	7.4.1	74.5		2.7	200	13.0	70-3	70.7	77.2	77.6	78.0	78.5	78.9	79.4	79.8	80.2	80.7	SI:I	81.5	82.0	82.4	82-9	83.3	83.7	84.2	04.0	05.0	05:5	85.9	1 2		87.7	Lat
Lat	134.7	136.6	137.5	138.4	139.3	140.2	AI.I	142.0	T42.0	142.8	70	44-7	145.6	146.5	47.4	48.3	49.2	I KO.I	Ter.o	Ter.D	152.8	167.7	7.00	2010	1930	150.4	157.3	158.2	1.651	10000	160.9	161.8	162.7	163.6	164.5	165.4	166.3	167.2	168.1	0.691	6.691	170.8	171.7	172.6	173.5	174.4	1/5:3	170.2	177.1	178.0	179.8	Dep
Diff				Marian St. Sec.	551	1951	571		-		Mary Street	NAME OF TAXABLE PARTY.	ACCUPATION NAMED IN	63 1	STATISTICS.	65 1	(Gard	風和	ng akwiburn					7	3	74	Fig.	1761	a constant	78					83				87			8	161			-	त्र	190	600		4	THE REAL PROPERTY.
Dep	44.3	44.7	45.2	45.6	46.0	46.5	46.9	47.3	47.8	48.2	186,022	SHIGHN	49.1	49.5	30.0	50.4	50.0	CI.21	KI.7	52.2	52.6	63.0	200	0000	33.7	54.4	54.0	55.2	55-7	50.I	26.6	57.0	57.4	57.9	58.3	58.7	59.2	59.6	1.09	60.5	6.09	61.4	61.8	62.3	02.7	63-1	13:0	04.0	64.4	65.3	65.8	Lat
Lat	800	01.7	02.6	93.5	94.4	95.3	96.2	97.1	08.0	080	1000	0.66	1001	9.101	102.5	103.4	104.3	105.2	1001	107.0	107.0	200	1	700		5.11.	112.4	13.2	141	115.0	115.9	8.91	12.7	0.811	119.5	120.4	121.3	122.2	123.I	124.0	124.9	125.8	120.7	127.0	120.5	120.7	2000	131.2	122.0	133.9	134.8	Dep
Diff	101	03	03	0.4	03	1901	40	80	00	IO	Ì		121	13 1	14 1	151	911		181	and the last	Marie Local		and the same of	2000	(MAKE)		moved to	1455ballete	27	000000	Villanda		200		33		35	136	37	38		9	All broads	42	43	4 4	3	140	4 ×	49	150	Diff
Dep	24.4	00	23.2	23.7	24.1	24.6	25.0	25.4	25.0	26.2	7	1200	27.3	27.6	28.5	28.5	28.9	F-02	20.8	20.2	20.7		3.10	0	3 %	34.4	32.9	33.3	33.8	34.2	34.6	35.1	35.5	35.9	36.4	36.8	37:3	37-7	38.1	38.6	30.0	39.5	39.9	40.3	40.0	41.2	41	42.1	44.5	43.4	43.8	Lat
Lat	8.5	16.7	17.6	8.5	19.4	50.3	I.2	1.7.	2.0	62.0	70	4.0	55.7	26.6	3	58.4	59.3	50.2	61.1			52.8	, ,	Y	2	200.5	41/2	200.3	2.69	10.I	0.17	6.17	72.8	73.7	74.6	75.5	70.5	77.3	78.2	1-61	80.0	6000	%I.%	82.7	03.0	04-5	500	80.3	07.2	80.0	89.9	Dep
Diff	12	22	5.2	5.4	55	26	57	00	03	209	all dispus	10	62	63	64	65	99	63	689	66	10	1	100	7 7	13	14	75	16	77	78	79	8	81	82	03	84	85	98	87	00		श		92	93	4 0		06	200		HI	THE PERSON NAMED IN COLUMN 1
Dep	00.4	30.0	51.2		02.2	02.6	01.I	01.5	02.0	200	0	04.0	05.3	05.7	1.90	9.90	02.0	57.6	04.0	200	000	200	4	0.60	100	10.5	0.11	11.4	8.11	12.3	12.7	13.2	13.6	14.0	14.5	14.9	15.3	15.8	16.2	16.7	17.1	17.5	18.0	18.4	10.0	19.3	3	20.2	0.00	21.5	21.9	Lat
Lat	0.00	0	32.7	93.6	04.5	05.4	6.3	07.5	L	Charles of		6-60	10.8	II.7	12.6	13.5	14.4	16.2	16.2	1.6.1	18.0	180	0	2	5	71.0	22.5	23.4	24.3	25.2	76.I	27.0	27.9	00 00 00 00	29.7	30.6	31.5	32.4	33.3	34.2	35.I	30.0	30.0	37-7	30.0	39-5	1	41.3	44.4	44.0	44.9	Dep
Diff	1	2	7	4	5	10	7	00	0	To			12	13	14	15	91	17	00 H	10	20	10	100	X .	57	24	25	26	27	28	50	39	31	32	33	34	35	36	37	38	39	9	41	42	43	4 4	1	40	4 4	49	50,	EIG

for 64 Degrees.

-	20000	0200	MINE CO	2000	2000	175400	1000	dolate	A100.00	DENN	200		SALE	55,546	pots	33506	200	(0)/(0)	andre	1	BULL ST				MILES.	1		NAME OF						150.27		10000	31.6	100	600	AND DE		111/6	4520	See all			3030				35573	
Dep	114.0	114.4	114.9	115.8	115.8	116.2	116.7	117.1	117.6	118.0	0	110.5	118.9	119.4	119.9	120.3	120.8	121.2	121.7	122.1	7000	7.7.7.	123.3	123.5	123.9	124-4	124.9	125.3	125.8	126.2	126.7	127.1	127.6	128.0	126.5	120.9	100 8	1 2 2	130.00	131.2	131.7	132.1	132.6	133.0	133.5	133.9	134.4	134.8	135.3	135.7	Lat	
Lat	223.6	224.5	225.4	226.3	227.2	228.1	229.0	229.9	210.8	22I.7	7 000	732.0	233.4	234.3	235.2	236.I	237.0		.00	酆	7000	201	241.5	242-4	243.4	244-1	245.0	245.9	246.8	0,000	248.6	249.5	250.4	251.3	252.2	253.0	? ? ?	25.4	9.9			59.3	100	261.1	0	262.8	3.7	4.0	05.5	267.2) da	Degrees
Did	251		53		55	256			60	99	CONTRACT	and large					266	continue				1	7/7	7	73	74	75	276	2	78			281	62	69	8 0	386		88		90	291	92	93	46	95	296	97	96	2002		Deg C
Dep	91.3	91.7	92.2	92.6	93.1	93.5	94.0	94.4	04.0	04.2	0		96.2	96.7	97.2	97.6	.08.1	08.5	0.00	40000	000	477.7	100.3	100	101.2	101.7	102.2	102.6	103.1	103-5	104.0	104-4	104.9	105.3	105.6	100	102	107.6	108.1	108.5	109.0	109.4	6.601	IIO.3	rio.8	111.2	1111.7	IIZ.I	112.0	113.0	Lat	63]
Lat	1.661	180.0	180.9	81.81	182.7	183.5	184.4	185.3	186.2	187.1	188	0.001	166.9	8.691	190.7	9.161	192.5	193.3	194.2	104.1	Tobo.		190.9	0.761	1,061	199.0	200.5	40I.4	200	-	204.0				207.0	5.00	2007.	2110	212.1		I3.8	15	215.6	216.5	17.4	218.3	4	Victoria de la constante de la	0	222.8		September 1
Dist	101	DOMESTAN	MANAGE STATE	8	NAME OF	-		80					12	13	14	13	216		18						-	INCOME.	SPENCE OF	SECTION S.	27	STATE OF THE PARTY.					33	-	NIN	3 6	700	20		d-Crosbane	42	43	and the same of	45	246	47	\$ 4	-	語	+
Dep	68.6	69.0	69.5	6.69	70.4	70.8	71.3	71.7	72.2	72.6	100	1.3.1	73.5	74.0	74.5	74.9	75.4	75.8	76.2	76.7	77.7	11:0	77.0	70.	70.5	79.0	79-4	79.9	80.4	80.00	81.3	81.7	82.2	82.0	63.E	03.5	0410	04.4	0 00	000	86.3	86.7	87.2	87.6	88.1	88.5	89.0	89.4	89.9	90.3	Lat	
Lat	134.5	135.4	F36.3	137.2	138.1	139.0	139.9	140.8	141.9	142.6	100	143.5	144-3	145.2	146.1	147.0	147.9	148.8	149.7	150.6	ICLE	200	100.0	0.00	10401	1550	2552	150.8	157.7	150.0	159.5	1000	161.3	102.2	1.501	6.507	104.0	7.03.	167.5	168.4	169.3	170.2	171.1	172.0	172.9	173.7	174.6	175.5	170.4	178.2	Dep	
Dit	151	407007000	53	SOCIAL PROPERTY.	EXPLORES	156	URBAT 25	00	60	The State of the S		200			-	65							1,2			erentan in	5	176	77						60	400							-		_	52		97	98	99	訓	
Dep	45.9	46.3	46.8	47.2	47.7	48.I	48.6	49.0	49.5	40.0		30	50.0	51.2	51.8	52.2	52.7	53-I	53.6	54.0	54.6	2 2 2	2 2 3 3	2	25.0	200	5000	572	57.7	50.1	58.0				400		5 5	6.09	62.7	62.1	63.6	64.0	64.5	64.9	65.4	65.8	66.3	66.7	67.2	68.4	Fall	
Lat	006	6.06	8.16	92.7	93.6	94.4	95.3	96.2	97.I	98.0	080	200	0.66	10001	9.101	102.5	103.4	104.2	IOS.I	106.0	0.901	107 8	200	9	2007	5.011	41:4	112.3	113.2	14.0	114.9		110.7	117.0	110.4	1001	121.0	T 22. T	123.0	123.8	124-7	125.6	126.5	127.4	128.3	129.2	130.1	131.0	131.9	131.7	Dep	
	IOI	03	03	40	05	901	07	80	8	IO	I	1	12	13	14	15	911		18	10		_		_		2 PONESS	00000000	NAME OF TAXABLE PARTY.	27	20			-		20	SCOMMON!		The second	A Decision of		ACCRECATION OF	141	42	43	4		146	47	ASSESSMENT OF THE PARTY OF THE		DIE	
Dep	23.2	23.6	24.I	24.5	25.0	25.4	25.9	26.3	26.8	27.2	100	10	7007	28.0	29.I	29.5	30.0	30.4	30.0	31.3	31.8	200		1 00	350-	33.0	1	34.5	35.0	35.4		30.3	0 1	3/0	28.1			30.6	40.0	40.4	40.0	41.3	41.0	42.2	42.7	43.I	43.0	44-0	44-5	- market	Lat	
Lat	15.4	16.3	47.2	18.I	49.0	49.9	30.8	51.7	52.6	53.5	7	24.4	55.3		57.0	(2)	-	59.7	S	61.5	62.4		000	7	2 0	200	0	0	2	5	70.4	77:3	72.2	73.1	0 00		9.92		4	79-3	900 W	81.1	82.0	82.9	3	84.0	85.5	00.4	80%	89.1	Dep	
Ditt	51		53		55	56	57	58	50				-				99					-	1 2	1 6	ر د :	4		10	200				0		200	· ~	198	87	88		96	16	92	93	\$	-	100	92		ALCOHOLD TO		
Depl	00.5		DI.4	S.IC	02.3	02.7	03.2	03.6	04.I	04.5	13	0.00	05-4	6.50	06.4	8.90	07.3	07.7	08.3	08.6	00°I	18	2 2		40.4	10.9	41	11.8	12.3	12.7	13.2	13:0	14.1	14.5	2 5	16.0	16.2	16.00	17.3	17.7	18.2	18.6	F-61	19.5	20.0	20.4	20.9	24.3	0017	22.7	Lat	100
Lat		0.10	02.7		04.5	05.3	06.2	07.1	080	08.0	0	0.60	10.7	0.11	14.5	13.4	14.3		16.0	16.91	17.8	18.	7		3	41.4	27.3	23.5	24-1	24.9	25.0	20.7	27.0	40.5	40.0	27.2	12.1	2 2 0	33.9	34-7	35.6	36.5	37-4	38.3	39.2	40° I	41.0	41.9	7 7 7	44.6	Dep	276 276 277
Dial.	F	2	3			9		00	Service Co.	TO		1	12	13	14	1.5	91		18	IO	20	100/255	200	7.7	23	24	25	26	27	200	29	R	31	32	33	200	3/8	22	000	39	40	41	42	43	44	4	40	40	4 6	100	信	

28 Difference of Latitude and Departure for 28 Degrees.

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 | GE S | | | 200 | THE SALE | 3,100,000
 | 2507100 | de de la constante de | 16500 | | | | | | | |
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 | Anna Raigh | | and the same | - | ARRESTS IN |
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7.8	8.3	80	9.2	9.7	0.2
 | 25.4 | 2. | 26.3 | 26.8 | 27.2 | 27.7
 | 28.2 | 28.6 | 29.I | 29.6 | 30.1 | 30.5
 | 31.0 | 31.5 | 31.9 | 32.4 | 32.9
 | 33.00 | 34.3 | 34.7 | 35.2 | 35.7 | 36.2 | 36.6 | 37.I | 37.0 | 2000 | 20.0
 | 130.4 | 139.9 | 140.4 | 140.9 | Lat |
| MICROPOWEN | CHICAGO | 4 11 | 3 | and I | SALIDIA SO | | H | Section Co. | - | 1 | | | | | 100000000000000000000000000000000000000
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 | 1.7 | 2.5 | 4 | .3 | 4 | ": | 0 | 2.0 | 6.7 | |
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\$23.2 101 \$0.00 \$0.00 \$0.5 14 \$5.0 \$2.4 10.0 \$0.01 \$0.00 \$0.0 | 00.00 00.5 14 k | 00.00 00.00 5.1 44.0 24.0 10.1 89.2 47.4 15.1 13.3 10.9 20.1 177.5 9444 95.2 32.3 4.0 10.00 00.00 00.00 178.4 94.8 14.0 12.3 14.0 17.8 14.9 94.8 15.4 15.0 17.9 10.0 17.8 4.9 94.8 15.0 17.0 17.0 17.0 17.0 17.0 17.0 17.0 17 | COLOR OND 5 14450 6349 101 89-8 47-4 151 133-1 70-9 101 87-9 94-8 53 233-81 COLOR OND 5 4450 634-9 101 89-8 47-4 151 133-1 71-8 101 179-8 95-3 53 33-34 in out of the state o |

for 62 Degrees.

Difference of Latitude and Departure for 29 Degrees. 29

100	1000				1865	100		-				265			Halic	200							-	-		-	-	_	-		-	7	3		1	-	-	T. Part	75	70.00	7	0	5	31	5	7 1	0	-	1	-
Dep	121.7	122.2	122.7	123.1	123.0	124.1	144.0	125.1	126.0	1	120.5	127.0	127.5	128.0	128.5	129.0	129.4	6-621	130.4	130.0	131.4	131.9	132.4	132.8	133.3	133.8	134.3	134.8	135-3	135.7	130.2	130.7	137.	138.7	138.	139.1	139.6	140.1	140.0	141-1	141.	142-	142	143	143	144	145	145.		
Lat	19.5	20.4	21.3	-	123.0	23.9	44.0	25.0	22.7.4	0	220-3	229.I	30.0	30.0	2,31.8	232-6	233.5	234.4	3	230.1	37.	237-9	238.8	239.0	240.5	241.4	242-3	243.I	244.0	244.9	245.0	240-0	248.4	249.3	250.1	251.0	25 1.9	252.8	253.0	254.5	255-4	250-3	257-1	250.0	250.0	260.6	261.5	262.4	Dep	
Diff	5112	52 2	53	296.200	55	250	57	50	59	1	201	2	6,	4,	5	0	20	00	-	श	271	200	73	74	25	276	77	700	200	000	201	0 0	200	.00	286	87	88	68	의	29I	92	93	4,6	95	290	90	1 99	300	Die.	
Dep	97.4	97.9	98.4	6.96	99.4	6.66	400	000	200	9 88	102.3	102.8	103.3	103.7	104.2	104.7	105.5	105.7	100.2	100.7	107.1	107.6	IOS.I	108.6	1001	109.6	IIO.D	1000000	111.0	111.5	112.0	112.5	113.0	II 3.0	114.4	114.9	115.4	6-511	116.4	116.8	117.3	117.8	0011	110.0	119.3	120.2	120.7	121.2	Lat	
Lat	7.5.8	1.92	177.5	+	-1	-	3 (20	182.7	1	4.5	5.4	0.3	64	01	0	×	.7	I.5	192.4	193.3	-	2.0	5.0	201	7	5.861	9.4	3	CO 88	202.0	300	20.50	205.5	206.4	207.3	208.2	2000	5-602	210.8	211.7	212.5	213.4	214.3	215.2	3.4.0.0	217.8	218.7	Dep	
) TE	1 10	02 I	03 I	-	101	0 1	700		101		111	State S	13	14	all the last		17.	CONTRACTOR OF		201	221 I	22 1	23	24	25	226	27	28	29	2	231	3.5	3.0	35	236		300	39	श	141	Total Service	43		_	246	47	40	250		
Dep L	73.2 2	73.7	74.2	74.7	75.1	75.0	1.0/	70.07	1.4.6	10	70.1	78.5	20.6	79.5	0.00	80.5	ØI.o	ØI.4	6.18	82.4	82.9	83.4	83.9	84.4	84.8	85.3	85.8	86.3	900	67.3	67.7	000	80.7	80.7	90.2	90.7	91.1	91.6	92.1	92.6	93.1	93.6	94.1	+	95.0	95.5	9000	ideal	判当	
Teq.	32.1	6	00	4.7	91	130.4	37.3	130.2	139.1	0	140.8	(41.7	143.0	143.4	44.3	145.2	1.0t	140.9	147.8	148.7	149.6	150.4	151.3	152.2	153.1	153.9	154.8		156.6	157.4	158.3	159.2	1.001	8.191	N BUTC	162.6	164.4	165.3	166.2	167.0	6.791	168.8	1.00.7	170.5	171.4	172.3	174.0	174.0	Dep	
Jit J	151	53 1	5.3		and the second			50			CONTRACTOR OF THE PARTY OF THE	07	63	4.	5	1991	67	89	69	2	171	72		74	7.5	176	77	78	79		100	0 00	000	200	186		88		9	161	92	93	94	95	961	97	00	200		
Dep	49.0	40.4	49.9	50.4	50.9	S1.4	51.9	52.4	52.0	33.0	53.0	54.3		55.3	55.8	56.2	56.7	57.2	57.7	58.2	58.7	59.I	59.6	1.09	60.6	61.1	61.6	62.I	62.5	03:0	63.5	64.0	04.5	65.4	65.0	66.4	66.9	67.4	67.9	68.4	8.89	69.3	69.8	70.3	70.8	71.3	71.0	72.7	Lat	
Lat	88.3	89.2	Section 1999	0.16	3.49	92.7			95.3	3559	97.1	0.86	98.8	2.66	100.0	roi.5	102.3	103.2	104.1	105.0	105.8	10001	107.6	108.5	100.3	110.2	III.I	6.111	112.8	113.7	114.0	115.4	IIO.3	1.811	118.0	110.8		121.6	122.4	123.3	124.2		125.9	120.8	127.7	128.0	129.4	121.2	Dep	
7.17	Tol	03	03	04	50	001	00	90	60	1	TIT	12	13	14	STATE OF THE PERSON NAMED IN	and the second	17	Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, whic	COLUMN TO SERVICE	20	H			-	-	126	27		_	39	131	32	33	3.4 2.e	126	27	38	39	40	141	42	43	4	45	146	47	4 4	1		
Dep	4.7	5.3	15.7	2.97	26.7	27.1	27-0		20.0		29.0	30.1	30.5	31.0	31.5	33.0	32.5	33.0	33.5	33.9	34.4	34.9	35.4	35-9	36.4	36.8	37.3	37.8	38.3	38.8	39.3		40.2	40.4		12.2	42.7	43.1	43.6	44.1	44.6	45.E	45.6	46.1	46.5	47.0	47.5	00	1 3	
Lat	14.6	15.5	46.4	47.2	4 % I	40.0	49.0	30.7	51.0	24.5	53.4	54.2	55.I	50.0	26.8	57.7	58.0	59.5	60.3	61.2	62.I	63.0	63.8	64.7	65.6	66.5	67.3	68.3	1.69	200	70.8	71.7	72.0	73.3	100	76.1	77.0	77.8	78.7	79.6	80.5	81.3	82.2	83.1	84.0	04.0	86.	800		
Did	12	52	53	54	55	50	70	50	50		19	62	63	64	65	99	67	99	69	70	71	72	73	74	7.5	196	77	78	19		20.0	0.00	0 0	000	98	00	00	8	06	16	1 92	93	9	9.5	96	0	803	10		1
Dep	00.5	0.10	01.5	6.10	02.4	03.0	03.4	03.0	4.4	150	05.3	05.8	06.3	06.8	07:3	07.8	08.2	08.7	09.2	09.7	10.2	10.7	11.2	11.6	12.1	12.6	13.1	13.6	14.1	14.5	15.0	15.5	10.0	10.0	1:	17.0	188	18.9	19.4	19.9	20.4	20.	2I.	21.	22.	à ·	23.	0 4	#	
Lat	0.0	01.7	02.6	03.5	41	05.5	1	02.0	0	7	9.60	10.5	11.4	12.2	13.1	14.0	14.9	15.7	16.6	17.5	18.4	19.2	20.I	21.0	21.9	22.7	23.6	24.5	25.4	26.2	27.E		38.0	500	3,10	22.4	33.2	-	35.0	35.9	36.7	37.6	38.5	39.4	40.2	41.1	42.	42.	4.1.	
Dift	1	V9000411	67	scale/yea	HERMAN	9	conferences	10000000		श				14	15	91	17	1.8	61	20	21	22	23	24	25	26	27	200	29	30	31	32	33	45	36	2 6	000	39	40	41	42	43	44	45	46	47	40	4 5	作	1

for 61 Degrees.

30 Difference of Latitude and Departure for 30 Degrees.

00.0) 00.1; 51 44.2 25.5 101 87.5 50.5 151 1908 75:5 101 174.1 100.5 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 4, 3, 2, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3, 3,	1	200						Tar			Lac	9		Lac			1001	
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05.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RESPONSE	-	5.00	51	44.2	25.5	101	07.5	50.5		130.8	75.5		174.1	100.5	51	217.4	125.5
03.5 03.6 03.6 03.6 03.6 03.6 03.6 03.6 03.6	SCHOOL	_	0.10	52	45.0	20.0	5.5	000.3	51.0		131.0	70.0	03	174-9	101.0		210.7	120.0
04.3 02.0. 5 4 4 4 6 2 7 0 4 9 0 1 5 2 0 5 4 13 2 4 7 10 2 0 5 1 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NATIONAL PROPERTY.		21.5	53	45.9	20.5	03	2002	51.5		132.5	70.5	03	175.8	101.5	3	219.1	120.5
04-2 0-4-2 0	40		0.70	54	46.8	27.0	04	1.06	52.0		I33.4	77.0	04	176-7	102.0	54	220.0	127.0
05.4 05.0 05.4 05.4 08.0 106 91.8 53.0 156 135.1 180 206 175.2 103.0 5.2 22.0 056 103.0 179.2 103.0 5.2 22.0 056 103.0 179.2 103.0 5.2 22.0 056 103.0 179.2 103.0 5.2 22.0 056 103.0 179.2 103.0 5.2 22.0 056 103.0 179.2 103.0 5.2 22.0 057 103.0 179.2 103.0 5.2 22.0 057 103.0 179.2 103.0 5.2 22.0 057 103.0 179.2 179.2 1	5	4-3	2.5	55	47.0	27.5	050	6.06	52.5	55	134.2	77.5	Marie Co.	7.5	102.5	55	220.8	127.5
0651 03:5 5 / 4944 48.5 9 / 7 53.5 5 / 136.6 78.5 9 / 136.6 78.5 9 / 139.6 78.5 78.5 78.5 9 / 139.6 78.5 78.5 9 / 139.6 78.5 9 / 139.6 79.5 9 / 138.6	nation out out	5.2	03.0	56	48.5	28.0	901	91.8	53.0	9	135.1	78.0	206	178.4	103.0		221.7	128.0
0.64 0.64 <th< td=""><td>70</td><td></td><td>33.5</td><td>57</td><td>49.4</td><td>28.5</td><td>04</td><td>92.7</td><td>53.5</td><td>-</td><td>136.0</td><td>78.5</td><td></td><td></td><td>103.5</td><td></td><td>222.6</td><td>128.5</td></th<>	70		33.5	57	49.4	28.5	04	92.7	53.5	-	136.0	78.5			103.5		222.6	128.5
09. 04. 04. 09. 04. 0 94. 54. 59 1377 794 09 1810 104. 0 94. 25. 0 0 138. 0 10	0		0.40	200	50.2	29.0	80	93.5	54.0	000	136.8	70.0			104.0		223.4	120.0
8,			34.5		CI.I	20.5	00	04.4	54.5	20	127.7	70.5		181.0	TO4.6		224.2	120.5
99, 95, 5, 5, 5, 15, 28, 31, 11, 19, 11, 19, 19, 19, 19, 19, 19, 1			0.20			20.0	10	05.2	0	200	128.61	80.0			TOP		20.5.0	1000
094 65.5 01 52.6 30.5 III 90.4 55.5 101 139.4 80.5 211 182.7 1105.4 201 2020.0 094 65.5 01 52.6 30.5 III 90.4 55.6 1040.3 81.5 11 182.7 1105.4 201 2020.0 11.3 65.5 65 134.2 81.5 13 184.5 106.6 65 13.2 5.6 13.2 5.6 144.2 81.5 13 184.5 106.6 65 13.2 5.6 13.2 5.6 144.2 81.5 13 184.5 106.6 65 13.2 5.6 13.2 5.6 14.2 81.5 13 184.5 106.6 65 13.2 5.6 13.2 5.6 14.2 81.5 12 185.2 10.7 6 62 13.2 5.6 13.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0						200	3	2	33.6	3	13000				3		11:	
13.0 0.0		-	25.5	Serious.	52.8	30.5	III	1.96	55.5		139.4	80.5			105.5			130.5
11.3 06.5 69 54.6		4	0.90	62	53.7	31.0	12	97.0	26.0		140.3	81.0			106.0			131.0
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14. 08.5 67 58.0 33.5 17 101.3 58.5 67 144.6 83.5 17 187.9 108.5 68 232.1 16.5 09.5 69 59.8 34.5 19 103.2 59.0 68 145.5 84.5 19 198.8 109.0 68 233.1 16.5 09.5 69 59.8 34.5 19 103.4 16.5 09.5 69 59.8 34.5 19 103.4 16.5 09.5 69 59.8 34.5 19 103.4 16.5 09.5 69 59.8 34.5 19 103.4 16.5 09.5 69 59.8 34.5 19 103.4 16.5 09.5 09 103.9 16.5 09.5 09.5 09.5 09.5 09.5 09.5 109.5 16.5 10.5 10.5 10.5 10.5 16.5 10.5 10.5 10.5 16.5 10.5 10.5 10.5 16.5 10.5 10.5 10.5 16.5 10.5 1	-		0.80	99	57.2	23,0	19	100.6	58.0		142.8	82.0		187.1	1080	266	30.4	132.0
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17.3 10.0 70 50.0 35.0 20 103.9 60.0 70 147.2 85.0 20 190.3 111.0 71 234.7 18.2 10.5 71 51.5 34.5 121 104.8 60.5 171 148.1 85.5 221 191.4 110.5 271 234.7 19.9 11.5 72 62.4 35.0 22 105.5 61.5 71 149.8 86.5 22 193.3 111.5 71 234.3 20.8 12.5 74 64.1 37.0 24 107.4 63.0 74 159.4 88.0 22 194.9 111.5 71 234.3 22.5 12.5 75 65.8 38.0 126 109.1 65.0 176 153.4 88.0 22 196.6 113.5 77 239.9 23.5 13.5 77 665.8 38.0 126 109.1 65.0 176 153.4 88.0 22 196.6 113.5 77 239.9 23.5 13.5 77 665.8 38.0 22 106.6 113.5 77 239.9 23.5 13.5 77 665.8 38.0 28 110.5 65.0 176 153.4 88.0 28 197.4 114.0 77 239.9 23.5 13.5 77 665.8 38.0 28 110.5 65.0 176 139.0 116.0 80 244.5 24.5 14.5 77 665.8 38.0 126 109.4 113.5 77 241.0 25.0 15.0 82 77 665.8 38.0 113.5 77 241.0 25.0 15.0 82 77.0 74.1 73 77 77 77 77 77 77 7			39.5		2	34.5		103.1	59.5		146.4	84.5		189.7	109.5		233.0	134-5
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19.9 IL. 73 63-2 36.5 23 106.5 61.5 73 149.8 86.5 23 193:1 III.5 73 236.4 220.8 120.7 74 150.7 8 70.0 24 194.0 III.5 73 236.4 220.8 120.7 74 150.7 8 70.0 24 194.0 III.5 75 236.4 237.3 220.8 120.7 766.7 38.5 10.8 24 107.4 62.0 74 150.7 8 87.0 24 194.0 III.5 75 236.4 237.3 222.5 13.0 766.7 38.5 27 196.6 III.3.6 76 67.3 8.7 196.6 III.3.6 76 67.5 39.0 28 III.0.8 64.0 79 153.0 89.5 24 194.0 III.3.6 78 67.5 39.0 28 III.0.8 64.0 79 153.0 89.5 29 198.3 III.4.5 79 23.9 24.2 II.4.5 79 68.4 39.5 29 III.7 64.5 79 153.0 89.5 29 198.3 III.4.5 79 24.0 7.2 25.1 II.4.5 79 68.4 39.5 29 III.7 64.5 79 155.0 89.5 29 198.3 III.4.5 79 24.0 7.2 25.1 II.4.5 79 68.2 13.1 II.3.4 65.5 181 156.7 80.0 155.7 23.2 20.0 116.0 82 24.2 5.7 16.0 82 17.0 14.0 5 131 III.3.4 65.5 181 156.7 91.0 32 20.0 116.0 82 24.2 5.7 16.0 82 17.0 14.0 5 131 III.3.4 65.5 181 156.7 91.0 33 20.0 III.6 82 24.2 5.7 16.0 84 17.2 14.2 66.5 83 158.5 91.0 33 20.0 III.6 82 24.2 5.7 16.0 84 17.2 14.2 66.5 83 158.5 91.0 33 20.0 III.6 82 24.2 5.7 16.0 84 17.2 14.2 66.5 83 158.5 91.0 33 20.0 III.6 82 24.2 5.7 16.0 84 17.2 16.0 88 16.2 16.0 10.0 10.0 88 16.2 16.0 10.0 10.0 88 16.2 16.0 10.0 10.0 10.0 10.0 88 16.2 16.0 10.0 10.0 10.0 10.0 10.0 88 16.2 16.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0			0		4	30.0	7	105.1	010	-72	148.0	0000		192.3	0111	72	235.0	130.0
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21.7 12.5 75 65.0 37.5 15 15.0 87.5 25 194.9 112.5 75 65.0 38.0 226 195.7 113.0 76 65.8 38.0 126 195.7 113.0 76 65.8 38.0 226 195.7 113.0 77 65.7 38.0 226 195.7 113.0 77 65.7 38.0 28 197.4 113.0 77 65.7 38.0 28 197.4 114.0 78 154.1 89.0 28 197.4 114.0 78 154.1 89.0 28 197.4 114.0 78 154.1 89.0 28 197.4 114.0 78 25.0 115.0 89.0 28 197.4 114.0 78 154.1 89.0 28 197.4 114.0 78 14.0 78 14.0 78 14.0 78 24.0 <t< td=""><td></td><td></td><td>12.0</td><td></td><td>64.1</td><td>37.0</td><td></td><td>107.4</td><td>62.0</td><td>74</td><td>150.7</td><td>87.0</td><td>24</td><td>194.0</td><td>112.0</td><td>74</td><td>23</td><td>I 37.0</td></t<>			12.0		64.1	37.0		107.4	62.0	74	150.7	87.0	24	194.0	112.0	74	23	I 37.0
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23.4 [3.5] 77 [0.67] 36.5 27 [110.0] 63.5 477 [153.3] 88.5 27 [190.6] 113.5 77 [23.9] 77 [23.9] 24.2 [14.0] 78 [154.1] 89.0 28 [197.4] 114.0 78 [24.1] 78 [24.1] 78 [24.1] 79 [25.0] 29.0 28 [17.0] 114.0 78 [24.1] 79 [25.0] 29.0 28 [17.0] 114.0 78 [24.1] 79 [25.0] 29.0 29 [19.2] 114.0 78 [24.1] 79 [25.0] 29.0 29 [15.0] 29.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 80 [24.2] 20.0 115.0 20.0 115.0 20.0 115.0 20.0	0	4.5	13.0		02.0	30.0	0	1.601	234000	0	152.4				113.0	270	434.0	130.0
24.2 14.0 78 67.5 39.0 28 110.8 64.0 78 154.1 89.0 28 197.4 1114.0 78 67.5 39.0 28 111.7 64.5 79 155.0 89.5 29 198.3 114.5 79 241.6 26.0 15.0 80 69.3 40.0 30 112.6 65.0 15.0 90.0 30 199.2 115.0 80 242.5 26.8 15.0 87.1 14.5 79 15.0 80.1 15.0 80 242.5 26.0 15.0 82 71.0 41.0 32 114.3 66.0 82 157.6 91.0 32 20.0 116.0 82 244.2 28.6 16.5 83 71.9 41.5 33 115.2 66.5 83 158.5 91.5 33 201.8 116.5 82 244.3 28.6 16.5 83 71.9 41.5 33 115.2 66.5 83 158.5 91.5 33 201.8 116.5 82 244.3 28.6 16.5 83 71.9 41.5 33 115.2 66.5 83 158.5 91.5 33 201.8 116.5 82 244.3 28.6 16.5 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 84 72.7 7.2 18.0 88 76.2 44.0 38 110.5 69.0 88 162.8 94.0 38 206.1 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 94.0 38 206.1 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 94.0 38 206.1 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 94.0 38 206.1 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 97.0 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 97.0 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 97.0 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 97.0 119.0 88 76.2 44.0 38 110.5 69.0 88 162.8 97.0 119.0 88 76.2 44.0 38 120.0 90 27.1 120.0 90 12	27 2	3-4 1	13.5		200	38.5	7	0.01	63.5	7	153.3	800.5	1000		113.5	77	S	138.5
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35.5 20.5 91 78.8 45.5 141 122.1 70.5 191 165.4 95.5 241 208.7 120.0 90 2511.1 35.5 20.5 91 78.8 45.5 141 122.1 70.5 191 165.4 95.5 241 208.7 120.5 291 252.0 30.4 21.0 92 79.7 46.0 42 123.0 71.0 92 166.3 96.0 42 209.6 121.0 92 252.9 37.2 21.5 93 80.5 46.5 43 123.8 71.5 93 167.1 96.5 43 210.4 121.5 93 253.7 38.1 22.0 94 81.4 77.0 44 124.7 72.0 94 168.0 97.0 44 211.3 122.0 94 254.6 39.0 22.5 95 82.3 47.5 45 125.6 72.5 95 168.9 97.5 45 212.2 122.5 95 255.5 39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 123.0 296 256.3 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 85.7 49.5 49 129.0 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 92.8 124.5 124.0 120 120 120 120 120 120 120 120 120 12	3 6	7	2.6	6	1.//	44.2		40.4	2.60		103.	94.5	-	-MORNEY	119.5		4300	144.5
35.5 20.5 91 78.8 45.5 141 122.1 70.5 191 165.4 95.5 241 208.7 120.5 291 252.0 36.4 21.0 92 79.7 46.0 42 123.0 71.0 92 166.3 96.0 42 209.6 121.0 92 352.9 37.2 21.5 93 80.5 46.5 43 123.8 71.5 93 167.1 96.5 43 210.4 121.5 93 252.9 35.2 22.5 94 81.4 47.0 44 124.7 72.0 94 168.0 97.0 44 211.3 122.0 94 254.6 39.0 22.5 95 82.3 47.5 45 125.6 72.5 95 168.9 97.5 45 212.2 122.2 122.2 25.5 39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 129.6 256.3 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 85.7 49.5 49 129.0 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 92.8 92.8 124.5 99 85.7 49.5 129.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 92.8 124.5 124.5 125.0 120 125.6 124.5 125.0 120 125.6 124.5 125.0 120 125.6 124.5 125.0 120 125.6 124.5 125.0 1	2	31		श	77.9	45.0	-	121.2	70.0		104.5	95.0		207.0	120.0		72711	145.0
36.4 21.0 92 79.7 46.0 42 123.0 71.0 92 166.3 96.0 42 209.6 121.0 92 252.9 37.2 21.5 93 80.5 46.5 43 123.8 71.5 93 167.1 96.5 43 210.4 121.5 93 253.7 38.1 22.0 94 81.4 47.0 44 124.7 72.0 94 168.0 97.0 44 211.3 122.0 94 254.6 39.0 22.5 95 82.3 47.5 45 125.6 72.5 95 168.0 97.0 44 211.3 122.0 94 254.6 39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 123.0 296 256.3 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 258.1 42.4 24.5 99 85.7 49.5 49 129.0 75.0 200 173.2 100.0 25.0 216.5 125.0 300 259.8 92.8 92.8 92.8 92.8 92.8 92.8 92.8 9	11 3.	5.3 2	10.5	16	78.00	45.5	141	122.I	70.5		165.4	95.5	241	208.7	120.5		forest his	145.5
37.2 21.5 93 80.5 46.5 43 123.8 71.5 93 167.1 96.5 43 210.4 121.5 93 253.7 38.1 22.0 94 81.4 47.0 44 124.7 72.0 94 168.0 97.0 44 211.3 122.0 94 254.6 39.0 22.5 95 82.3 47.5 45 125.6 72.5 95 168.9 97.5 45 212.2 122.5 95 255.5 39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 123.0 296 255.3 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 258.1 42.4 24.5 99 85.7 49.5 49 129.0 75.0 200 173.2 100.0 25.0 216.5 123.0 300 259.8 Dep Lat Diff Dep Lat	12 3		0.I.	92	79.7	46.0	42	123.0	71.0	92	166.3	0.96	1000	209.6	121.0		252.9	146.0
38.1 22.0 94 81.4 47.0 44 124.7 72.0 94 168.0 97.0 44 211.3 122.0 94 254.6 39.0 22.5 95 82.3 47.5 45 125.6 72.5 95 168.9 97.5 45 212.2 122.5 95 255.5 39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 123.0 296 256.5 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.3 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 258.9 42.4 24.5 99 85.7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.5 99 25.8 90 173.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 25.0 216.5 123.0 300 259.8 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	3 3		7.I.		80.5	46.5	43	123.8	71.5		167.1	90	-	त्र	121.5		253.7	146.5
39.0 22.5 95 82.3 47.5 45 125.6 72.5 95 168.9 97.5 45 212.2 122.5 95 255.5 39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 123.0 296 256.3 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 3.5 7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.5 99 3.5 8.9 43.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 Diff Dep Lat Dep Lat D	4 3		2.0		8I.4	47.0	44	124.7	72.0		168.0	0.20		. ~	122.0	0.0	254.6	147.0
39.8 23.0 96 83.1 48.0 146 126.4 73.0 196 169.7 98.0 246 213.0 123.0 296 256.3 40.7 23.5 97 84.9 49.0 48.1 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 85.7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.0 98 85.7 49.5 49 129.0 77.0 200 173.2 100.0 250 216.5 123.0 300 259.8 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	5 20		2.5		82.2	47.5	74	12.6.6	72.6		168.0	21.0		0.10.0	100	1 2	25.50	147.6
39.0 23.0 90 83.1 40.0 140 120.4 73.0 190 109.7 98.0 246 213.0 123.0 296 250.3 40.7 23.5 97 84.0 48.5 47 127.3 73.5 97 170.6 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 25.7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.5 99 85.7 74.5 99 172.3 99.5 49 215.6 124.5 99 258.9 43.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep				N	?	2/3			(1)			3	21		: "":		0	10
40.7 23.5 9784.0 48.5 47 127.3 73.5 97 170.0 98.5 47 213.9 123.5 97 257.2 41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 84.9 49.5 74.5 99 172.3 99.5 48 214.8 124.0 98 25.7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.5 99 258.9 43.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	ALC: N	0	20.0	5 .	03.1	40.0	-	170.4	73.0	0	100.1	98.0	0	0	123.0		250.3	140.0
41.6 24.0 98 84.9 49.0 48 128.2 74.0 98 171.5 99.0 48 214.8 124.0 98 258.1 42.4 24.5 99 85.7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.5 99 258.9 43.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	Name of Street		43.5	-	84.0	40.5	-	127.3	73.5	7	170.0	98.5		0	123.5	97	257.2	140.5
42.4 24.5 99 85.7 49.5 49 129.0 74.5 99 172.3 99.5 49 215.6 124.5 99 258.9 14 43.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 15 Dep Lat Diff		1.0	4.0	96	84.9	49.0	-	178.3	74.0	86	171.5	0.66		214.8	124.0	86	258.1	149.0
43.3 25.0 100 86.6 50.0 150 129.9 75.0 200 173.2 100.0 250 216.5 125.0 300 259.8 15 Dep Lat Diff		2.4	4.5	66	85.7	49.5		129.0	74.5	66		99.5		215.6	124.5		258.9	149.5
P Lat Did Dep Lat	-	33	200	8	86.6	50.0		129.9	75.0	200	SIMPLE	100.0		216.5	125.0		259.8	150.0
	R D	ep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat	Diff	Dep	Lat	Diff	Dep	Lat

for 60 Degrees.

-Gerba		1000	and the same							1										200					others -											100												2
Dep	129-3	129.8	130.3	130.0	131.3	131.0	134.4	132-9	133.4	133.9	134.4	134.0	126.4	1000	106.	3000	137.0	137.5	130.0	130.1	130.6	140.1	140.6	141.1	141.6	142.1	142.7	143.2	143.7	144.7	144.7	45.4	146.3	146.8	147.3	147.8	48.3	148.8	149.4	49.9	150.0	51.4	51.9	52.4	53.0	153.5	154.0	54.5
Lat			× .	217.7	410.5	4	PRINT	NATIONAL PROPERTY.	0	222.8	223.7	224.5		† ,	NAME OF		20	APRIL CONTRACTOR		430.5	220.0	22.1		2000	35.7	36.5	4	238.2	39.1	0.0	40.8	41.7	43.4	44.2	45.1	46.01	46.81	47.7	48.5	49.4	SU.Z	252.0 I	252.8 1	53.7 1	54.5 I	55.4 1	254000	257-1
		52	53	54	न	250	57	-		8	261	62 2	DOM: N	-	PRIMA	ROMEN		OFF CORNES		20	No. of Lot	727	727	742	75 2	2762	77 2	00	79 2	810	2812	7 00	84.2	85 2	2862	87 2	88	89 2	80	1 2	9 20	0 4		296 25	97 2.	98	1000	010
מפת	103.5	104.0	104.5	105.1	105.0	1001	1000	10/01	107.0	108.2	108.7	100.2	100.7	110.0	110.1		411.4	0.111	117.9		21.0	TI4.2	2 7 1	115.4	115.9	116.4	116.9	117.4	117.9	110.5	119.0	120.0	120.5	121.0	121.5	122.1	122.6	123.1	123.0	24.1	124.0	25.6	26.2	26.7	27.2	127.7	128.2	128.8
100	2.3		74.0			170.5	4.//1	20000	1.6		180.8		WAN		1			0.001				+ 0	2 H	10	00		. 10	+	3		198.0		12			4	0	·	1	200.5	208.2	2 -	-	10.81	211.7 1	12.5	13.4 I	14.3 1
1	201	07	03	0 0	ीं	200	5 %	ŝ	6	S	21I	12	12	27	17	31,0	410	17	0 0	400	22.1	1 6	23	Market Street	25 1			28 I		श्ल		32		35 2	2362	7		STATE OF THE PARTY OF	404	enderen de la constitución de la	424	Complete of Section	-	246 21	47 2	48	49 2	250 2
	77.8	70.3	78.8	7.50	0.67	000	× 2.0	0.10	6-1-9	62.4	82.9	83.4	82.0	200	84.0	× ×	0000	7 7 7 8	24.0	87.6	88.1	88.6	89.1	89.6	90.1	90.6	91.2	61.7	92.2	74.1	93.2	93.7	94.8	95.3	95.8	96.3	8.96	97.3	97.9	4000	00.4	0000	100.4	6.00	01.5	102.0	102.5	103.0
	129.4	130-3	131.I	122.00	3.4.0	1,000	25.0	- 22.4	130.3	17.75	138.0	138.8	130.7	140.6	141.4	TA2.2	2	143.1	0 0 0	145.7	146.5	147.4	48.3	149.1	150.0	150.8	151.7	54.5	153.4	12403	155.1	1.66.8	57.7	58.5	59.4	160.3	191	162.0	102.8	103.7	165.4	166.3	167.1	68.0	∞.	7	170.5	71.4
	151	52	53	4,	SIX	-HAGES	2	PRODUCT	DESCRIPTION OF THE PERSON NAMED IN	8	191	62	63	64	9	166	2 4	38	3 9	702	17.1	1 2	. 65	74	30			184	79		101	8 6	841	851	9			6	211	174	93 1	4	95 1	1961	10	96	_	007
	52.0	5 2.5	53.0	2000	7	24.0	65.6	25.	50.1	50.7	57.2	57.7	58.2	58.7	50.5	50.7	600	200	6I-2	61.8	62.3	62.8	63.3	63.9	64-4	64.9	65.4	62.0	62.4		68.5	68.5	69.0	69.5	70.0	20.6	71.1	71.0	72.1	72.4	73.6	74.2	74.7	75.2	75.7	70.2	10.1	3
1	86.6	4./0	800.3	000	000	01.7	02.6	200	4.5%	74.3	95.1	0.96	8.96	97.7	98.6	4.00	100.2	101	102.0	102.8	103.7	104.6	105.4	106.3	107.1	108.0	08.00	2.601	110.0	100	112.1	114.0	114.8	115.7	9.911	117.4	116.3	1.90.1	000	121.7	122.6	123.4	124.3	125.1	126.0	120.0	128.6	0.07
1	ioi	7 0	5 6	7 6	3 3	200	000	3 8	3 5	शे	III	12	1.3	14) I	911	1	200	IOI	207		73	23	4	25	9	27		29		131	1 93		35.1	9	70	-		<u>}</u>	7 2 7	STATE OF THE PARTY.	CONTRACTOR OF	45 I	WHEN DOWN			2000	3
1	26.3	40.0	1 × × ×	200		20.4	20.0	200	4 0	200	31.4	31.9	32.4	, "	33.5	24.0	24.6	25.0	25.5	36.I	36.6	37.I		38.1	38.6	39.I	39.7	40.2	40.7		44.7	42.7	43.3	43.8	44.3	44.8	45.3	45.0	404	47.4	47.9	48.4	48.9	46.4	20.0	50.5	21.0	5.1.5
	43.7	1	45.4	47.1	000	84	40.7	200	7 4	-	52.3	53.I	54.0					58.3	59.1		60.8	61.7	62.6	63.4	64.3	65.1	0000	0 00	9.89	100	70.3	71.1	72.0	72.8	73.7	74.0	15.4	77.1	78.0	200	79-7	80.6	81.4	82.3	03.r	84.8	85.7	
1			55	7 7	1	2 2	200		24	U	19 /		63	9		_					71	72	73	74	75	76	77	70	80	٥			84	8	98	800	000	6	No	02	93	94	95	96	92	000	10	
1			02.1		-						05.7		06.7			08.2			00	-	000000000000000000000000000000000000000			12.4	12.9	13.4	13.9	4.4	14.9	16.0	16.5	17.0	17,5	18.0	18.5	1.61	19.0	20.6	21.1	21.6	22.I	22.6	23.2	23.7	24.2	25.2	25.8	?
1	000	3	0.50	04.2	06.1	0.90	0.90	07.7	200		4.60	10.3	II.I	12.0	12.9	13.7	14.6	15.4	16.3	17.1	18.0	18.9	19.7	20.6	21.4	22.3	23.I	44.0	25.7	26.6	27.4	28.3	29.I	30.0	30.9	31.7	34.0	24.2	35.I	36.0	36.9	37.7	38.6	39.4	46.3	42.0	42.0	
1	H (* 0	3	- 4	الم	,,	-00	0		3	II	12	13	14	15	91	17	18	19	20	2.1	22	23	24	2.5	26	270		307		3 6	33	34	35	36	37	30	30	4	42	43	44	45	40	4.	40	20	-

for 59 Degrees.

32 Difference of Latitude and Departure for 32 Degrees.

Dep	122.0	· ·	133.0	34.1	34.0	35.2	35.7	29.5	106 4	100	137.3	137.8	0	1,50.3	130.0	139.4	139.0	140.5		2 1	41.5	42.0	43.6	43.I	42.6		:	44.7	45.2	45.0	40.3	46.8	47.3	47.9	48.4	48.9	149.5	150.0	50.5	I.I	51.6	52.1	52.6	53.2	53.7	54.2	54.8	55.3	55.8	\$6.4	\$6.9	157.4	6.25	58.5	60.0
136	12.8		20	5	5.4 I 34	2 I	17.1	17.0 It	0	0 N	0	220.5 I	100	0 0	3	0	223.9 I		14	Common of	4.0.4	ZZ7-3 I	228.I I	229.0 I	220.8			1 00	1 4.464	31000	454.0 I	234.9 I	235.7 I	30.0 I	437.4 I				40.8 I	41.7 I	43.5 I	43.4 I	44.2 1	45.I I	45.9 I	46.8 I	47.6 I	48.5 I	49.3 I	50.2 I	51.0I	1 6-15	53.7 I	53.6 I	54.4 I
7 110	14 I 21	6	7	53 214	54 21	55 216	256 21	57 217				00 22	261133				64 2	65 224						70 2	271 2				7 4 4			77 2			S L	281 2	64	4	9	85	286 2	87.4	88	89.2	90	291 2	92 2	93 2	942	952	2962	97.2	98.2	99.2	3002
don	106.5	107.1	7 7 7 0	107.0	1001	108.7	109.2	109.7	TT0.2	0	0.0	111.3	III.8	110 4	1.7	113.0	113.4	114.0	114.5	TTE	2000	6.6	IIO.I	116.6	117.1	117.7	118.2	118	110.2	2 0 1 1	0.64	120.3	120.0	4.1.4	617	122.4	123.0	123.5	124.0	124.0	125.1	125.0	I20.I	120.7	127.2	127-7	128.3	128.8	129.3	129.9	I30.4	130.9	131.4	132.0	132.5
	10.4	- 6	ED200E 0	-	2000	73.8	74.7	175.5 1	7.9		4		10					182.3	182.2	Markey (IV)			85.7	9	187.4		-	1	200	N	5	-	20.			0	_		~	199-3	200.I	201.0	201.8	202.7	203.5	204.4	205.2	206.1	206.9	207.8	208.6	200.5	1000	ZII.I	212.0
II.	201	02 1		60	041	5	206 1		80	-	4880	9	2II	1.0		13	141	15	116	17	18			2	22I	MIN.	23	2.0	No. No.	226	9.7	¥ 0	9 6	2 6	ने	407	3 6	33	34	4	230	37	30	39	4	24I	4	43	44	4	24				250
-	80.0	80.6	21.1	0.10	0.10	82.2	82.7	83.2	83.7	0	0	04.0	85.3	84.0	70	900.4	80.9	87.5	88.0	88.4	80.0	200	9.60	90.1	90.6	91.2	01.7	02.2	02.8	03.2	0.00	93.0		74.7		95.9	5.00	27.0	97.5	700	98.0	1.66						102.3	102.8	103.4	103.9	104.4		105	106.0
	128.0	128.0	1007	1-69	130.0	31.4	132.3	33.I	I 34.0	2 4 8		135.	126.5	127.4	100	130.4	139.I	139.9	140.8	141.6	142.6		43.3	144.2	145.0	145.9	146.7	147.6	148.4	140.2	T.CO.T	100	25.7	757.6	1		204.0	133.4	150.0	200		158.0	159.4	100.3		102.0	162.8	163.7	104.5	105.4	166.2	167.1	-	0.001	100.6
÷	ISI		6.2	-	2	55	0	57			29		191		44	5	04	65	H		89	oy	5	2	ILI	72	73			1961	77	786	70	80	N.		i oc	90	0 0		100	000	-	8 8	3	161		93	4		961	97	9, 8		2000
	53.5	54.1	64.6	-	23.	55.7	50.2	56.7	57.2	67.8	. 0	30.3	50.00	50.4	200	37.7	4.00	01.0	61.5	62.0	62.5	1 69	40,4	03.0	64.I	64-7	65.2	65.7	66.3	8.99	67.2	67.8	68.	68.0	709		1000	31.0	71.0		-		1.5.4			14.	75-3	75.	26.07		77.	77-9	70.4		. 1
- September 1	85.6	86.5	87.2	288	000	0000	6-68	90.7	91.6	02.4	000	25.52	94.I	0.50	8	2 40	40.7	97.5	98.4	99.2	1001	TOO.	0 101	01.0	102.6	103-5	104.3	105.2	106.0	106.8	107.7	108.5	100.4	110.2	1111	III.0	112.8	7.611	114.6		2.6.0	1140.6		1187			120.4	121.3	1.44.1	123.0	123.0	124.7	1.96.	1000	44/14
TO DESCRIPTION OF	TOI	0.2	0.2	3 2	5 6	3	100	07	80	00	2 0	श	III	12	62	2:	14	15	911	17	18	2	-		IZI	22	23	24	2.5	126	27	200	20	9			addition for	2.4	25	126	200	386	900	40	1	-4-	47	43	4	₹];	140	47	4 4	TEO	71.
	27.0	27.6	28.I	28.6		31	29.7	30.2	30.7	1I.3	31.8	2	32.3	32.9	22.4	100	33.9	34.5	35.0	35.5	36.0	36.6	2 4 6	3/:	37.0	38.2	38.7	39.2	39.8	40.3	40.8	41.2	41.0	42.4	42.0	43.5	44.0	77.		46.6	9	9	49.0	7.7	~	0	4	4			2 :	2 2 2 2	62.0	62.0	3.0
	43.2	44.1	44.0	00	7 7	40.0	47.5	40.3	49.2	50.0			51.7	52.6	E-2.4				56.0	56.8				<u> </u>	00.2	61.1	6.19	62.8	63.6	64.4	65.3	66.1	67.0	67.8	68.7	69	70.4		72.1	72.0	7.2.5	3 74.6	75.0	76		100	200		0	10	83	200	84	(Citation)	-
1	SI	52			10	3	20	57	500	60	9	31.	19	62	62	?	2	5	99	67	89	9	70	4	71	72	73	74	3 7.5	3 76	3 77	100	1 79	80	81	82	00	80	8 9	1 8 E	9	- SC	2	2	10	2	200	, r	0	7	10	4	0	5 100	1
	00.5	01.1	01.6	1		3	03.2	03:7	04.2	8.40	200	3	05.5	06.4	0-90		200	00.0	08.5	000	00	TO.	100		1	111.7	17.7	12.7	13.	13.	14.	14.	15.	15-6	16.	17.0	17.	318	18	10.	IO	20.	1 20.	0 2I.	2 I.	5 22.	22	2 22	2 2 3	200	0 24	7 25.	6 26.	4 26.	1
1	00.8	01.7	02.5	0.2.4	3	3	95.1	5.50	00.8	07.6			09.3	10.2	11.0				13.6	14.4	15.3	16.1	17.0		17.6	18.7	19.5	20-4	21.2	22.C	122.9	23.7	24.0	25.4	26.2	27-1	28.0	28.8	29.	30	31.	32.	33	333	1 45	25.	26.	27.	30	20,	7 30.	8	941.	0 42.	1
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for 58 Degrees.

Difference of Latitude and Departure for 33 Degrees. 33

128.3 83.3 139.8 83.9 139.9 133.9 88.8 144.8 99.9 144.8
56.6 54 129.1 83.9 04 171.1 III.1 54 57.2 75 130.0 84.4 05 171.2 III.6 55 58.3 57 131.2 85.5 06 175.4 113.3 58 59.4 59 131.3 86.6 09 175.4 113.4 56 60.5 161 135.9 87.1 176.9 114.4 60 60.5 161 135.9 88.2 12 177.6 115.5 64 61.0 62.1 137.5 88.2 12 177.6 115.5 62 61.0 62.1 137.5 88.2 12 177.6 115.5 64 61.0 62.1 137.5 88.2 12 177.6 115.5 64 61.0 62.1 137.5 118.6 117.6 117.6 117.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 147.6 </td
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for 57 Degrees.

34 Difference of Latitude and Departure for 34 Degrees.

T LOOK	8		42.7	28.5		81.7	山間				15	+ KK K	1:		NO.	
2 01.7		524	43.1	20.I	02	84.6	2000	131	126.0	200	0 0	167.8		451	2080	140.0
POLICIA/SETSION.			3.0	20.6	3	85.4					3 6	168.2		6	200.7	
4 03.3	02.2		44.8	30.2	04	86.2		54			9	1.691		5.45	210.6	
5 04.1	02.8	554	45.6	30.8	05	87.0		55	128.5		6	169.9	114.6	55	211.4	142.6
6 05.0	03.4	564	6.4	31.3	901	87.9	59.3	156	129.3	87.2	206	170.8		256	212.2	143.
Programme in	03.9		17.3	31.9	00	88.7		57	130.2		07	171.6	and Plants	anilla.	213.1	143.
				32.4	8	89.5		58	131.0	CYBS	80	172.4	116.3		213.9	144.
			and the same	33.0	6	90.4	01.0	59	131.8		60	173.3	A Contract		214.7	144.
	Contractors.		17.7	33.0	श	91:2		8	132.0	-	입	174.1	SECOND .	L	215.5	145.
		_	20.0	34.I	III	92.0		191		aleste.	2II	174.9	-	7	216.4	146.
	-	63	I.4	34-7	12	92.8		62	134.3		12	175-7			217.2	14
13 10.8	-		necessarily	35.2	13	93-7	63.2	63	135.I		13	176.6		63	218.0	147.
11.6			53.I	35.8	14	94.5	63.7	64	136.0	1992	14	177.4	119.7	64	218.9	-
12:4	08.4	655	3.9	36.3	15	95-3	64.3	65	136.8	92.3	15	178.2	120.2	65	219.7	148.
16 13.3		66 5	4.7	36.9	911	2.96	64.9	991	137.6		216	1.671	120.8	266	220.5	148.
I4.1	09.5	67 5	5.5	37.5	17	97.0	65.4	67	138.4	93.4	17	6.6LI	121.3	-	221.3	149
14.9	IO.I	5	6.4	38.0	18	97.8	0.99	89	139.3		18	180.7	121.9	89	222.2	149.9
15.8	10.6	69 5	7.2	38.6	19	98.7	66.5	69	140.1	94.5	19	181.6	122.5	69	223.0	150.4
20 16.6	II.2	705	8.0	39.I	20	99.5	67.1	70	140.9	er ger		182.4	123.0	70.	223.8	
17.4	11.7	715	58.0	10.7	IZI	100.3	67.7	171	141.8		22.1	182.2		271	224.7	I ; I.
18.2	12.3	72 5	9.7	0.3	22	IOI.I	68.2	72	142.6		22	184.0		-	225.5	152.1
1.61	12.9	736	0.5	0.00	-	102.0	8.89	73	143.4	96.7	23	184.0		73	226.3	152.7
19.9	13.4	746	I.3	1.4		102.8	69.3	THE REAL PROPERTY.	144.2	97.3	24	184.7	125.3	74	227.I	153.2
20.7	14.0	9	2.2	0.1		103.6	6.69	-	145.1	97.9		186.5	125.8	7.5	228.0	153.8
21.6	14.5	766	63.04	2.5		104.5	70.5	-	145.0	98.4	10	187.4	126.4	276	228.8	154.
22.4	15.1		63.8	7 H		105.3	71.0	-	146.7	0000		188.2	126.0	77	220.6	154.0
23.2	15.7	786	4.7.4	3.6	-00	1.901	71.6	700	147.6		-00	(A.) (E.)	127.5	78	230.5	155.5
29 24.0	16.2	9	5.5	4.2		106.0	72.1	Name and Post	148.4	200	0	180.8			221.2	1,60
4	16.8	80/6	66.3 4	4.7		107.8	72.7		140.2	100.7		1007		200	222.1	156.6
31 25.7	17.2	816	67.1	100		9.801	72.2		150.0	-		101	100	38	222.0	1.7.1
6	17.0	826	68.0	200		IOO.4	72.00		I CO.O	-	10,	1000		2	2.2.2.8	167.7
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34 28.2	TO.O.	846	9.6	100		I.I.I	74.0	300	152.6	-	3.4	10401		300	200	200
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40 33.2	22.4	00	- Department	50.3	Name and Address of the	116.1	18.3		167.6	1001		10001	+ +		240.4	162.2
	3000		COLUMN TO SERVICE		- STATES	116.0	286		27.5		21	2000	41)	-		
24.0	7 0 0	76	5.5	5	-	7 2 2	0.0/		13000	100.0	Mariament	199.0	134.0	291	441.4	1.77
25.6	24.00		77.1	4.4	4 4	1001	79.4	7 0	2.661	107.4	43	20000	135.3	92	242-1	103.3
26.5	24.6	200	námostka	2.5	43	110.0	200		2001		43	201.4	135.9	93	442.9	103.0
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 | 164. | 164. | 105. | 105. | .00 | .000 | 107
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 14.8 14.8 |

for 55 Degrees.

36 Difference of Latitude and Departure for 36 Degrees.

								e Kini	gero	MARKE.	ak-ce	en la	Diedos.	1000			-	4	-	-	-	=			-		-	-	-				La	~	3	0	10	IH	7	33°	6	8	0	9	7	00	4	0	9	19	2	50	
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1	147	148	148.	14	14	150.	IS	IS	1	1 2				H	TEE		190° 1000	N*4910					H	015	= (COMPARE	100	- H	10		I b	1 2	H	0	00	9	4 1		0		91	4	7	0	00	7	5	3	H (-
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4	203.1	203.	204.7	205	206.	207	20	208.7	200	2.10		7 I	21	212.	2.1	7.1		2200	-					22	22	2		12	1				12			7	a	6 2	7 2	88	9 2	90 2	1 2	7		4	5	9	10	00			100
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dsa	rr8.1	118.7	119.3	119.9	120.	IZI.	121.	122.	122.	9.3	143	24.	124.6	125.	19.6	200	7	127	127	126.1	128.	129	129.9	130	131.	131.7	132.	122.8	0 5	133	1216	124	126	136.4	137	137	138.1	I 38.	139.		14	14	14	20000000						ar-countries			
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5	62.6	53.4	164.2	165.0	165.8	166.7	167.5	168.	T.Vy	7600	3	70.	171.5	172.2	1.77.	113	13	174.	175	170.	177	178	178.8	179.6	I80.4	181.2	182.0	182	OX I	187	×	18	186.	00 1	188	189.	19				193	194	13						-	· Constant			29
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5	TOI	0	0	0	0	101	0	0				H		-			310	H	+	0 \	0	HI	7 1	3	6		O SEE	M.	Mess	200	4	- 0	9	.2	00	4	0.0	0.6	۲.	.7	2.3	12.9	3.5	4.1		600	2.0	6.4	0 4	0.0	00 00	100	2 4 55
Dep	0.0	0.6	1.2	1.7	2.3	2.9	1.5	4.1		-	-	5.5	6.4	27.0	-	200	000	300	39.	0	40.	41.	41.	42.	42.0	42.5	44.1	44.	16.2	45.00	46.4	47.0	4.7	4	48.8	49.4	20	1 10	31.1	51.7	5	Sec.	53	54	54	30	v.I	56	57	57	2 5	G de la	i
real.	63	13	9	7.3	33	100	I	0	2 6	5.	7	3	6	C	00	· ×	श	4	2	0 0	o ·	3	4	7	F:	-	1	61.5		2 14			1	66.3	67.I	0,0	68.8	9-69	0.4	1.2	2.0	2.8	3-6	4-4	5.5	0.0	6.0	1.1	8.5	,	0.0		1
Lat	4I.	42.I	42.	43.	4	45.	46	46		100	4		50		2	7			and the last		n	2	57	58.2	59.		-			9			9	32 6			9 5		87 7	8	7	00	17	27	37	47	5/1	67	977	000	STATE OF THE PARTY.	ALC: UNKNOWN	Section 1
Diff	SI			54	55	26	57	80		50	3	19	62	29	3	13	5)	00	00	00	60	120	71	72	73	74	75	16		786	, ,		000	00	00	00	00	98	000	00	00	0	6.	6	6	6	9	6	6	ه, د	H		
669,203	9	2	00	4	6.	1 45	H	1	, ,	2 0	7	.5	H	97		1 0	01	4	0	0	67 6	0	.3	6.	3.5	H	.7	1 %	0.0		17.0	9.	18.2	18.8	4.	0.0	20.6	1.2	21.7	22.3	22.9	23.5	4.1	4.7	5.3	5.9	0.5	7.0	200	200	29.4	2	Section
Dep	9.00	01.2	8.10	0.7.	02.	10	04.	20		5 6	3	90	07.I	0.7	0						-	11.8	12.	12.9		14.	SAME OF THE	1:	M.		0.0000		12			4		12			90	41	2 2	0	Electron.	4	4 2	7	0 0	2 10	20		
Lat	8.00	9.10	02.4	03.2		04.0	05.7	06.5	0 40	5-70	100	08.0	00.7	TOPE	TT	7	17.1	12.9	13.0	14.0	15.4	10.2	17.0	17.8	18.6	19.4	20.2	I.o.	21.8	22.7	22.5	24.3	1	25.9	26.7	27.5	28.3	29.	29.9	30	31.6	32.	33.	34-	34.	35.0	ان	37.	3000	20.	40.5	Den	
1	0	0	0	0	O	10	0	3				0	-			1	-	and the same of the same of					eterotendo	- contractor	-	make the	THE RESIDENCE	14				30 2			33		15	36	37	300	39	्रा	41	42	43	4:	3	40	44		-	-	1
5		4				L					3	I	12	1.2			1	10	-	01	10	18	7.1	22	23	2.4	13	12	2	7,7	7	3	15			63		13		1	4.0	1		200								13	-

for 54 Degrees.

Difference of Latitude and Departure for 37 Degrees. 37

2000	N A	10		7	W	7	7	3	6	W	7	K	3	0	5	H	7	3	6	15	T	F	67	6	-	174	7	3	6	2	7	7	3	6	V)	H		20	7	14	1	3	6	2	H	~	0	ומיו	1500
Dep	ISI.	151.	152.	1,52.	153.	154.	154.	155.	155.	156.	157.	157.	158.	158.	159.	160.	160.	161.	161.	162.	163.	163.	164.	164.	165.	166.	166.	167.	169.	168.	169.	169.	170.	170	11:	172.	172.	173.	174.	175.	175.	176.	176.	177.	178.	170.	179.	180.	اذ
Cat	80.4	2.1	2.0	3.8	3.6	4.4	5.2	000	8-90	07.0	08.4	2.60	10.0	210.8	6.I.	147	13.2	0.1	4.8	12.6	6.4	人	8.0	8.8	219.6	4.0	2.I.2	22.0	22.8	2346	4.42	25.5	26.0	20.8	27.0	4.0	2000	30.0	31.6	32.4	33.2	34.0	34.8	35.0	36.4	37.4	38.8	39.6	Dep
	18	30	20	9	2	8	20	8	4	8	8	3	2	7	7	5	7	2	2	2	2	2	2	7	7	200	7	8	0	2	1 2	7	3	7	21	20	2 6	0	6	7	7		4	2	9	7 00	0 2	0	\exists
D'O	251	22	53	54	2	256	57	58	59	နှု	261	2	63	9	65	266	9	30	59	70	273		7	7	7	276	7	7	7	8	28	82	00	84	0	700	82	, ∞	9	29	6	6	94	9	39	90	6	30	Ē
l dec	0.17	9.I	12.2	12.8	13.4	14.0	24.6	25.3	\$5.00	\$ 97	27.0	27.6	28.2	128.8	29.4	130.0	130.6	31.2	31.8	132.4	33.0	33.6	34.2	34.8	35.4	36.0	36.6	37.2	137.8	38.4	39.0	39.6	40.2	40.8	41:4	42.0	42.0	43.8	44.4	45.0	45.6	46.2	46.8	47.4	48.0	40.0	49.8	50.4	Lat.
F	H	3	1	20		S	3 1	H	0	7	SI	3 1	I	ROV.	71	2 1	3 I	HI	1 6	7 4	5 13	3 I	H	9 13	71	5 1	3 I	H	16	7 1	SI	3 I	I	16	7	5 I	3 1	16	71	SI	3 I	1	16	7.	5.	3	16	21	_
Lat	160	161.3	162.	162.9	163.7	164.	165.	100	100	167.	168.	169	170.	170.9	171.	172.	173.	174.	174.	175.	176.	x77.	178.	178.	179.	180.	181.	182.	182.	183.	184.	185	186	186	107	× ×	100	190	191.	192.	193	194	194	25	196	197	198	199	De
Dift	TOE	03	03	40	6	300	5	8	60	위	211	12	13	14	15	316	17	18	19	20	122	22	23	3.4	25	226	27	28	29	30	23I		33	34	शे	230	37	39	40	241	42	43	44	4	246	47	49	250	
Dep	6.06	91.5	92.1	92.7	93.3	93.9	94.5	95.1	95.7	96.3	6.96	97.5	98.1	98.7	99.3	6.66	IOO.5	IOI.I	roi-7	102.3	102.0	F03.5	104.1	104.7	105.3	105.9	106.5	1.701	107.7	108.3	108.9	109.5	I.O.I	110.7	11:3	6.111	112.5	113.7	14.3	14.9	115.5	116.1	116.7	117.3	6.713	170.0	119.8	120.4	Lat
	9	and the same	7	Michigan Park	district to	9	4	67	0	99.	Sec.	*	7	254		9	4 I	.2 I				4	4	10000000	-	19	4	7.	NO.	7	.5.	.3		6.0	7	.5		10000	TSENSO, S	5.	3.3	7.	6.	7	٠.	5 1	6.	1.7	<u>a</u>
La	120.	[2.I.	122.	123.0	123.8	124	125	126	127	127	128.6	129.	130	131.0	131.8	132.	133	134	135.0	135.8	136	137	138	139.0	139.8	140	I4I	142	142.9	143.	144	145	146	146	14	148	149.3	150.9	ISI.	I52.	153	154	154	155	150	157	158	159	ے
Diff	ISI	52	53	54	3	156	57	28	53	- Contract	THAT I WAS		63	-	6.5	9	7		69	70	171	72	73	74	antibated in	176	77	78	79	80	181	87	83	***	ीं	981	× ×	80	90	191	92	93	94	95	196	97	99	200	Diff
Dep	100	SA COLUMN	62.0	62.6	63.2	63.8	64-4	02.0	92.0	2.99	8.99	67.4	0.89	9.89	69.2	8.69	70.4	71.0	21.6	72.2	72.8	73.4	74.0	74.6	75.2	75.8	76.4	77.0	77.6	78.2	78.8	79.4	80.0	80.6	81.2	81.8	82.4	83.6	84.2	84.9	85.5	86.1	86.7	87.3	87.9	80.1	89.7	90.3	Lat
t I	7	5	1. 180	H	6	98633C	1000	300 551		MESCES	PLEASE.		\$150.00A		75F02F		Skiro	67	0	00	9.	4	64	0	00	9	4.	.2	0	00	9.	4.	.2	00	0	•	4 0	0	00	9.	¥.	.2	00	٥١:	0	4 6	0	8	<u>a</u>
La	8	81	8	83	83.	84.	85.5	800	200	87.8	88	89.4	90.2	91.0	16	92.	93.4	94	95.0	95.8	96	97.4	98	0.66	66	100	IOI.	102	103.0	103.	104	105	106	107.0	[0]	108	100	III.0	III.	II	II3	114	115		II	311	IIC	II	ĬĚ
Dif	IOI	0.2	03	9	50	90I	04	80	60	의	III	12	13	14	15	911	17	18	19	20	171	22	23	24	25	126	27	28	29	30	131	32	33	34	35	136	37	30	40	141	42	43	44	45	140	48	49	150	劃
Dep	30.7	31.3	31.9	32.5	33.1	33.7	34-3	34.9	35-5	36.1	36.7	37.3	37.9	38.5	39.I	39.7	40.3	40.0	41.5	42.I	42.7	43.3	43.9	44.5	45.I	45.7	46.3	46.9	47.5	48.I	48.7	49.3	49:0	50.6	51.2	51.8	52.4	53.6	54.2	54.8	55.4	56.0	56.6	57:2	57.8	50.4	59.6	60.2	Lat
Lat	40.7	1.5	2-3	13-E	43.9	14-7	5.5	10.3	17.1	5	8.7	19-5	20.3	51.I	51.9	52.7	53.5	54-3	55.I	55.9	56.7	57.5	58.3	59.I	6-65	2.09	61.5	62.3	63.1	63.9	64.7	65.5	66.3	67.1	61.6	68.7	200.2	71.1	71.9	72.7	73.5	74.3	75.1	75.9	10.1	78.3	79.1	29.9	Dep
Did	51	524	53	54	55	-56	57	500	50	8	19	62	63	64	65	99	-		69	70	71	72	73	74	75	16	77	78	79	80	81	82	000	84	ी	900	804	89	06	16	92	93	46	3	9 6	80	66	100	
Dep	9.00	21.2	8.IC	02.4	03.0	23.6	04.2	94.8	95.4	0.90	9,96	2.40	07.8	08.4	0000	9.60	10.2	10.8	II.4	12.0	12.6	13.2	13.8	14.4	15.0	15.6	16.2	6.91	17.5	18.1	18.7	I9-3	6-61	20.5	21.1	21.7	22.3	23.5	24.1	24.7	25.3	25.9	26-5	77.1	27.7	28.9	29-5	30.1	Trat
Lat	800	9:10	02-4	03.2	04.0	04.8	05.0	4-90	07.2	08.0	8.80	9.60	10.4	11.2	12.0	12.8	13.6	4.4	15.2	0.91	8.91	9.41	18.4	19.2	20.0	20.8	21.6	22.4	23.2	24.0	24.8	25.6	79.7	27.7	20.0	78.8	29.0	31.2	31.9	32.7	33.5	34-3	35.I	35.7	30.7	38.3	39.1	39.9	Dep
Did	١	7	3	4	5	9	7		-	IO	II	12	F3 1	14	15	91	17	18	19	20	21	.22	23	24	25	2.6	27	28	29	30	31	32	33	34	35	30	37	39	40	41	ed to the said	43	4 4	45	40	48	49	20	

for 53 Degrees.

38 Difference of Latitude and Departure for 38 Degrees.

					63.00																															0.00	3.4						1.110	41.62	-			-
Dep	154-5	155.4	¥.6.4	157.0	157.6	158.2	158.9	159.5	1001	160.7	161.3	161.9	162.5	163.2	163.8	164.4	165.0	165,6	166.2	166.9	167.5	168.I	168.7	169.3	6.691	170.5	171.2	171.8	172.4	173.0	173.0	174.2	175.5	176.1	176.7	177-3	177.9	178.6	179.2	8.621	180.4	181		182.0	183.5	183.1	184.7	Lat
Lat	2001		200.I	200.9	201.7	.5	.3	204-1	204.9	205.6	206.4	207.2	208.0	208.8	3000	210.4	211.2	211.9	212.7	213.5	214.3	215.1	215.9	216.7	217.5	218.2	219.0	219.8	220.0		222.2	223.0	224.5	225.3	226.1	226.9	227.7	228.5	229.3	230.I	30	222.4		233-2	134.8	235.6	GI	Dep
	251	5.5	2 4 2	5.5	256	57	58	59	८	197	62	63	64	. 65	366	67	89	69	70	371	72	73	74	7.5	276	11	78	29		281	025	603	8 %	286	87	8	89	श	162	92	93	44	3	290	788	. 3	300	
Black Y	123.8	26.0	25.6	126.2	126.8	127.4	178.1	138.7	129.3	129.9	130.5	131.1	131.8	132.4	133.0	133-6	134.2	134.8	135.5	136.1	136.7	137.3	137.9	138.5	139.I	139.8	140.4	141.0	141.6	142.2	142.8	143.5	144.1	146.3	145.0	146.5	147.2	147.8	148.4	149.0	149.0	150.4		151.5	152.7	153.3	153-9	Lat
DOI: DO		20.03	160.7	101	63	3.1		_	105.5	166.2				169.4	170.2	171.0		172.5	£73-3	174.1	174-9	175-7	176.5	177.3		0	9	4	181.2	00	2	103.0	184.2	185.0	186.7	187.5	188.3	189.1	189.9	190.7	191.5	102.0	200	193.0	1001	196.2	197.0	Dep
HI O	20I	3 6	A CHARGE	SEPTIME !	907	60	Mades		3	111	12	13	14	15	216	17]	18	161	20	221	22	23	44	25	226	27	200	29	SI SI	231		33	34	326	7	300		왕	241	43	43	4 ;	4	£	4. 4.8 4.8	49	250	Diff
Dep		93-0	04.8	95.4	0.96	1-96	97.3	97.9	98.5	1.66	99-7	1001	IOI.0	9.101	102.2	102.8	103.4	104.1	104.7	105.3	105-9	106.5	107.1	107.7	108.4	109.0	109.6	110.2	110.8	111.4	112.1	112-7	113-3	14.	III	115.8	116.4	117.0	117.6	118.2	118.8	119.4	7	120-7	121.0	122.5	123.1	Lat
1	0.61	0 0	21.3	22.I	22.9	23.7	24.5	25.3	70.I	50.0	27.6	128-4	129-2	130.0	130.9			133.2		134-7	135.5		137.5		138-7	139-5	140-2			143.0	ALC: A COMME	or translation	245.0	-	147.3	H	~	149.7	150.5	151.3	152.1	152.6		154.4	1,500	156.8	157.6	Dep
	ISI	52	545	55	1361	57	58	59	3	191	62 1	631	641	651	-	and order	683	69		171		73	74	7.5	1761	77	78	79	<u></u>	181	0 0	63	200	186	87	88	89	위	161	92	93	4 2	त्र	190	780	99	200	Diff
A STATE OF	0.014039	03.0	64.0	64.6	65.3	6-59	5.00	67.1	67.7	68.3	0.69	9.69	10.2	70.8	71.4	72.0	72.7	73.3	73-9	74.5	75.3	75.7	76-3	77.0	17.6	78-2	78.8	79.4	80.0	80.7	ØI.3	6.18	82.1	82,7	84.4	85.0	85.6	86.2	8.98	87.4	200	000	وا	89.9	200	91.7	92.4	Lat
Lat	29.6	8 2 2	81.0	82.7	130	84.3	85-1	85.9	86.7	87.5	88.2	89.0	89.8	90.06	91.4	93.2	93.0	93.8	94.5	95.3	1.96	6.96	97.7	98.5	99.3	1001	100-0	9.101	102.4	103-2	104.0	104-8	105.0	107.2	107.0	108-7	109.5	IIO.3	111.1	6-111	112.7	113.5		115.0	116.6	117.4	118.2	Dep
THE STATE OF	IOI	200	300	05	901	5	80	8	oi.	III	13	13	14	15	911	17	18	19	20	121	22	23	34	25	126	27	281	291	-				34	136	7	38	39	9	141	42	43	\$:	शं:	9	187	49	150	Diff
dəc	31.4	33.0	32.2	33-9	34.5	35.1	35.7	36-3	36.9	37.6	38.2	38.8	30-4	0.0	9.0	11.1	0.1	12.5	3.I	13.7	4:3	6.4	15.6	16.2	8.9	17.4	0.8	9.8	19.3	6-61	50.5	51.1	51.7		62.6	54.3	\$4.8	55.4	56.0	36.6	57.3	57.0	200	59.1	5000	61.0	61.6	Lat
Lat	10.2	00	42.5	43-3	44.1	6-41	15-7	46-5	47.3	1.8t	6.84	49.6	0.4	51.2	2.0	52.8	\$3.6	4.4	55.2	6.55	56.7	57.5	58.3	59.1	6-65	60.7	61.5	62.2	63.0	63.8	04-0	5.4	2009	212	68.5	60.3	70.1	70.9	71.7	72.5	73-3	74.1		75.0	77.2	78.0	78.8	Dep
Turd	SI	52	53	55	56	57	58	59	9	19	62	63	64	65	130	67	68	99	Sales Acc	71	72	73	74	75	76	77	78	79	8	8	80	80	200	86	82	88	8	8	16	92	83	\$ 2	3	96	7%	99	18	Diff
Dep	9.00	01.7	02.0	03.1	03.7	04.3	6-40	05.5	2.90	8.90	07.4	080	9.80	2.60	000	10.0	I.I.	11.7	12.3	12.0	13.5	14.2	14.8	15.4	16.0	16.6	17.2	17.9	18.5	1.61	1.61	20-3	20.0	22.2	22.8	23.4	24.0	24.6	25.2	25.9	26.5	27.1	1.12	20.3	20.6	30.2	30.8	Lat
Lat	8.00	0.10	02.4	03.9	04-7	05.5	06.3	07.1	6.40	08.7	9.5	10.2	II.0	8.11	12.6	13.4	14.2	15.0	15.8	16.5	17.3	18.1	18.9	19.7	30.5	21.3	33.I	22.9	23.6	24-4	25.5	20.0	20.0	28.4	20.2	29.9	30.7	31.5	32-3	33.I	33-9	34-7	33:3	30.2	27.00	38.6	39-4	Dep
Dift	-	4	204	5	9	7	00	6	Io	11	12	13	14	15	16	117	18	19	20	31	22	23	74	25	36	27	38	29	R	31	32	33	34	36	27	300	39	9	41	42	43	1;	3	40	4.8	49	50	Dia

for 52 Degrees.

															9								500	- 1									· ·					Ad									1			80
Dep	18	158.6	150.2	159.8	160.5	1.191	161.7	162.4	163.0	x63.6	164.2	164.0	165.5	166.1	8.991	167.4	168.0	168.7	169.3	6.691	170.5	171.2	171.8	172.4	173.I	173.7	174.3	174.9	175.6	170.2	176.8	177.5	178.7	179.4	180.0	180.6	181.2	6.181	182.5	183.I	183.8	184.4	87.6	200	100.3	187.5	188.2	188.8	Lat	Ī
Lat,	1983	200	9.9	7.	4	- Maria Anna	199.7		201.3				-	. 4		206.7		208.3	0	200.8	210.6	211.4	212.I	212.9	213.7	214.5	215.3	216.0	216.8	217.0	218.4	219-1	220-7		222.3	223.0	223-8	224-6	225.4		226.9	1-1-2	1000	91	73000	221.6	232.4	33.E	IMA	
Dift	1:	404	53	54	5	256	57	500	59	9	192	62	62	9	99	266	67	689	69	70,	271	72	73	74	75	276	77	200	79	8		0 00			286	-	-00	89	8	162	92	93	4	10	9	92	000	0	田	
Dep ,	2 921	127.	127.7	128.4	129.0	129.6	130.3	130.9	131.5	132.2	132.8	133.4	134.0	134.7	135.3	135.0	136.6	137.2	137.8	138.4	139.1	139.7	140.3	141.0	141.6	142.2	142.9	143.5	I44.I	144.7	145.4	140.0	140.0	147.0	148.5	149.1	149.8	150.4	151.0	151.7	152.3	152.9	153.0	154.4	154.8	1.691	156.7	157.3	Lat	
Lat	1.66.9	0	-	158.5	159-3	1091	160.0	9	4	163.2			166.6	166.3	167.1	167.0	168.6	169.4	170.2	171.0	171.7	172.5	173.3	174.1	174.8	175.6	176.4	177.2	178.0	178.7	179.5	181	181.8	182.6	183.4	184.2	185.0	185.7	186.5	187.3	1881	× × ×	189.0	190.4	191.2	191.9	103.5	104.3	Dep	
Diff	100	The second		9		206	07	80	60	10				141	IS	216	17	18	0I	20,	22I	. 10	23	24	2.5	226	27	78	29	위	23I	35	33	25	236	37	38	39	40	24E	43	43	44	45	240	47	4 4	6	Market Co.	I
Dep 1	10	200	06.3	96.9	97.5	98.2	98.8	99.4	1001	100-7	101.3	IOI.9	102.6	103.2	103.8	104.5	106.1	105.7	106.4	107.0	107.6	108.2	108.9	109.5	IIO.I	110.8	111.4	112.0	112.6	113.3	113.9	114.5	115.2	116.4	117.1	117.7	118.3	118.9	119.6	120.2	120.8	121.5	122.1	122.7	123-3	124.0		125.0	Lat	
Lat	119.2	200	K18.0	119.7	120.5	171.2	122.0	122.8	123-6	124-3	125.1	125.0	126.7	127.4	4	129.0	129.8	130.6	131.3	132.1	132.9	33.7		4	136.0	136.8	137-5	H	139.1	-	140.7	141.4	142.0	143	144.5	145-3	146.1	146.9	147.6	148.4	149.2	150.0	15000	23-55	152.3	153.0	154.6	155-4	Dep	l
Dift	10.1	10.	5	54	55	SHOOKS WAY	7	at the second	59	9			62	64		166	67	689	69	70	171	72	73	74	7.5	176	77	7.8	79		181	8 %	3 &	*	186	87	88	89	위	161	92	93	4 2	3)		92	99		lä	I
Dep 1	404	63.6	64.8	65.4	66.I	66.7	67.3	68.0	68.6	69.2	60.09	70.5	71.1	71.7	72.4	72.0	22.6	74-2	74.0	75.5	76.1	76.8	77.4	78.0	78.7	79.3	79.9	80.6	81.2	81.8	82.4	83.1	03.7	200	85.6	86.2	86.8	87.5	88.1	88.7	89.4	000	20.0	71:2	91.9	92.5	1000	1000	Lat	l
Lat	.8	10.07	80.0	80.8	81.6	82.4	83.1	83.9	84.7	85.5	86.3	87.0	87.8	88.6	89.4	1.00	000	01.7	92.5	93.3	94.0	94.8	95.6	96.4	-97.I	97.9	98.7	5-66	100.2	ioi	101.8	102.0	103.4	104.0	105.7	106.5	107.2	108.0	108.8	9.601	110.3	1.1.1	113.2		113.5	115.0	115.8	9.911	Dep	I
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Depl	1:0	34.4	22.4	34.0	34.6	35.2	35.9	36.5	37.I	37.8	38.4	30.0	20.6	40.2	40.0	41.5	42.2	42.0	. 4	4	44.7	45.3		46.6	v	4	48.5	49.I	49.7	50.3	51.0	51.0	54.4	22.5	54.1	54.7	55.4	560	000	57.3	57.9	50.5	59.8		00.4 6.7	61.7	62.3	62.0	Lat	١
Lati	1900	2 4	1.2	43.0	42.7	43.5	44.3	45.I	45.8	46.6	47.4	48.2	40.0	40.7	50.5	\$ I.3	52.I	52.8	\$3.6	54.4	55.2	56.0	56.7	5.1.5	58.3	1.65	59.8	9.09	61.4	02.2	65.0	64.5	66.2	1.99	6.99	67.6	68.4	2.69	झ	10.1	71.5	74.3	200		76.0	76.2	76.9	17.7	Dep	١
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Lat	00	91.0	02.3	03.1	03.0	04.7	05.4	2-90		07.8	08.5	00.3	IO.I	10.9	11.7	12.4	13.2	14.0	14.8	15.5	16.3	17.1	17.9	18.7	19.4	20.2	21.0	21 2	22.5	45.3	24.1	25.6	26.4	27.2	28.0	28.00	29.5	30.3	31.1	31.9	32.0	24.2	35.0	25.30	36.5	37-3	38.1	38.9	Lep	1
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for 51 Degrees.

40 Difference of Latitude and Departure for 40 Degrees.

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8	611	9	66.2	67.	68.1	88.8	69.4	o	ó	1	72	72.	73.3	73.9	74.	75.2	75.9	0	17.	77.8	78.	79.1	79.7	2	81.0	81.	82	82-9	83.	84.2	84.9	85.5	86.8	87.	88.1	88.7	9.00	40	. 6	6	6	0	6	9	10	, 0	-1
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for 50 Degrées.

Difference of Latitude and Departure for 41 Degrees. 41

A COLUMN		AND DESCRIPTIONS	A COLUMN	N. State Co.	AL WAY	SCHOOL S	13000	March Co.	90000	(bolto	6000	25.24	MIN'S	No. of Lot	Sec.	10000	4.300	Sec. 4	superior of	the Room	-	E. S. and		1000	37.42	19.47	1	The same	1000		de.			AND 19.5	e les			- Age		1000		25.53	2006	2000		500	1	Salas	- 000		1	10000	
Dep	16.6		5-59	9.99	167.1	167.0	168.6	169.2	169.0	170.5	171.7		- / 9	172.5	173.2	173.8	174.5	175.1	175.8	176.4	177.1	177.8	178.	170.1	- 17	179.7	100.4	0.101	181.7	181.4	183.0	183.7	184.3	185.0	165.0	100.3	0.00	107.0	1880	180.6	100.2	T00.0	TOL	102.2	193.8	193.5	194.2	194.8	195.5	1961	90.0		100
Lai	80.	4000	3 6	101.7	102.5	103.2	194.0	194.7	105.6	106.2	10,50	24/61	1.16	198.5	199.2	20000	200.8	201.5	202.3	203.0	203.8	2000	2000	2000	000	20000	5	.3	1	00	0 1	211.3	3.I	212.8	213.0	214.3	1.5.1	5.0	0.017	2.4	0	19			21.6	222.6	123.4	24-2	24.9	225.7	720.4	nebi	
Diff	1:	-2-	3.4	5.0	STATE OF THE PARTY.	PROJECTION	57	ASSESSED BY	A. Section	1900	6,000	COMPANY.								69				100	of Street,	74		270 2	77			_		82			3	SECONO MAN	_	80 2	OR PURPOS	-			042	95 2	2962	97.2	98.2	8	300		200
Dep	177 8		132.2	133.8	134.5	134.1	F35.8	136.4	137.1	137.7	1284	T 00 T	-39-1	139.7	140.4	141.0	141.7	142.3	F43.0	143.6	144.3	TARED	9 7 7 7	1.6.9	200	140-9	147.0	146.2	148.9	149.0	150.2	150.9	151.5	152.2	152.0	153.5	134.1	154.0	155.5	8 9 2	1 C 7.4	1.8.1	. 83	1.00.4	160.0	£60.7	161.4	162.0	162.7	163-3	104.0	13	
Lat	Ten & 4	Wilder.	1.69.9	154.0	STATE OF	1:	, 4	0			1			00.0	5		0		10	39	0.9	loc	164 6	2 8 9 1	6000	0.012	000	0	33	141	2	173.0	3	175.1	175.8	170.0	4.7.	176.E	6.024	180	181.1	1	7	182.4	4.2	6	185.7	6.4	7.7	6	188.7	neb	Service of the servic
סינו	100	PAGE P	Coloradousia Coloradousia	CONTRACTOR OF THE PARTY OF THE	GRANK SEC	STATE OF THE PARTY OF	MOTOR A	62 PMG		-	10000	10	1 4	13	The second		Mark Printers	17		[6I]		-		10000	and the same	44	5	0	10		6		H	32	3	4 ,	1000-200	0	/0	The sales	0	_	144			4.5			_		2.50		ť
Dep	000	200	100.4	0.101	IOI.7	102.3	103.0	103.6	104.3	Ior.o	105.6	106.3	5001	1000	107.0	108.2	108.9	109.5	IIO.2	FIO.9	III.S	TT2.2	110.8	1 4 7	6.0	114.1	114.0	115.4	116.1	116.8	117.4	116.1	118.7	119.4	120.0	120.7	171.4	122.0	122.7	124.5	124.6	1000	1726.0	126.6	127.2	127.9	128:16	129.2	129.9	13045	131.2	Tra	
Lat	LIA		200	116.2	Million States	15	STATE OF THE PARTY.	17	120.0	120.8	101.6	179.7	144.5	123.0	123.8	124.5	12,5.3	0 921	126.8	E27.5	128.3	120.1	120 8	1000	200	131.3	132.1	132.0	133.6	134.3	135.1	135.8	136.6	137.4	138.1	138.9	139.0	140.4	141.1	142.6	142.4	1000	7 4 4 4	146.7	146.4	147.2	147.9	148.7	149.4	150.2	150.9	Dep +	
Dift	177			2 4			5.7				141	40		03			NEWSCOOL SERVICE		_	69				_		Minusian III										64				0 0	-	1 12	1 0	7 6	0.4	95	1961	97	86	66	000	5	, ,
Dep 1	644	6 99	67.6	68.2	68.0	60.5	70.3	70.8	71.5	72.2	72.8	M.O. F.	13.5	74.1	74.0	75.4	76.1	76.7	77.4	78.I	78.7	70.4	100	000		01.3	05.0	82.0	63.3	84.0	84.0	85.3	85.9	80.0	87.2	62.0	0000	89.2	66.60	200	01.8	000	2	200	94.5	95.1	9.5.8	96.4	97.1	97.7	98.4	Lat	
Lat	26.0	100	77.7	78.5	70.2	80.0	80.8	81.5	82.3	83.0	82.8	000	2	05.3	0000	00.0	87.5	88.3	89.I	80.8	9006	01.3	02.1	02.8	7	0.56	74.3	95.1	95.8	0006	97.4	100	6.86	0.66	100.4	101		102.0	103.4	104.0	105.7	106.4	107.2	107.0	108.7	109.4	110.2	110.9	111.7	112.5	1.13:2	neb	
Dift	Treat	1 8	8	040	0	901	07	80	8	IO	1:	110	7 .	£3	14	1.5	911	17	18	19	20.	121	22	2.2	2	4 4		120	27	200	29	30	131	32	aladest.	34	ALC: UNKNOWN	-			-	and the second	4.2	THE PERSON NAMED IN	44	45	146	47	48	49	150		
Depl	72.5	0.00	2.4.8	35.4	36.I	36.7	37-4	38.0	38.7	39.4	0	0 0	5	41.3	42.0	45.0	43.3	44.0	44.6	45.3	45.9	46.6	44.2	14.0	4.0.	40.5	49:4	49.0	50.5	5I.2	51.0	52.5	53.1	53.0	54.4	55.1	3	50.4	57.1	200	0.0	10.1	200	61.0	61.7	62.3	63.0	63.6	64.3	64.0	65.	Lat	
Lat	18.c	20.0	40.0	40.8	41.5	42.3	43.0	43.8	44.5	45.3	16.0	× ×		٧٠٠	40.3	49·I	49-8	30.6	51.3	52.1	52.8	53.6	64.2	2 4 5	33.5	33.0	20:0	57.4	58.1	58.9	59.0	00.4	6I.I	6.19	05.0	03.4	04:7	04.0	05.7	67.9	67.0	484	, ,	70.2	70.0	71.7	72.5	73.2	74.0	74.7	75.5	Dep	
Diu	1	69	22	44	25	95	57	58	59	9	1y	42	7 7	03	04	श	99	67	89	69		11	. 43	1 2	ુ:	4	1	20	77	78	62	00	% W	82		04				000	00	15	1 8	2 0		95	96	97	86	66			1)
Dep	600		02.0	02.6	03.3	03.0	04:0	05.2	05.0	9.90	07.0	1 6	100	00.5	2.60	80	10.5	II.2	11.8	12.5	13.I	12.8		-	-0-1	13.1	10.4	17.1	17.7	18.4	19.0	19.7	20.3	21.0	21.0	22.3	51	23.0	24.3	25.6	26.3	26.0	2 2 2	28.2	28.0	29.5	30.2	30.8	31.5	32.1	32.0	Lat	
Lat	000		03.7	23.0	03.8	13	05.3	0.90	8.90	07.5	100	2	10	00.60	0	11.3	12.E	12.8	13.6	14.3	14.1	18.5	Y 91		1/.4	100	10.0	19.0	20.4	21.I	21.9	22.0	23.4	24.5	24.9	25.7	70.4	27.2	27.0	700	20.2	000	24.7	23.5	33.2	34.0	34.7	35.5	36.2	37.0	37.7	Dep	A 25 C
Diff	1	and the same				19									14		91	17	18	10	-	1.	1 6	7 .	-	24	25	20	27	700	29	30	31	33	33	34	35	30	37	30	40	1	4.	10000	44	4.5	46	47	48	49	50		

for 49 Degrees.

42 Difference of Latitude and Departure for 42 Degrees.

Dep		6-201	168.6	160.1	2 27	6-601	170.6	171.2	2	6.1/1	172.6		5.6/4	173-9	ì	174-0	176.2	0.0	175-9	176.6	177.0	7	177.9	178.6	T 70. 2	2 6 7	100.0	180.6	100	101.3	182.c	182 6	50400	183-3	184.6		104.0	186.1	2 / 2	3	180.0	187.3	300	000	188.7	189.3	100.0		7:07	191.3	192.0	102.7	TO 2. 2	173.5	194.0	194.7	106.2	3.4	7	1.000	197.4	108.0	108	100	199.4	2000	200.7	Lat	34.5
Lat	100	5	4	6	. 00		189.4	190.2		5067	191.7	X.	***	193.1	1	193-9	104.6		1961	1.961	0.9		197.0	198.3	1001	0	0-661	200.6	15	7	203.I	ox	5	203-5	204.3	1	205.0	205.8	300	2	207.3	208.0	1800	7:00	200-5	210.2	211.0	0110	1	212.5	213.2	213.0	214.7		215.4	2.16.2	216.0	219.7	101	7.017	219.1	210.0	220.6	221.4	1.600	1.222	222.9	Dep	
DIG	1	451	53	6.2	2	24	5.5	256		57	28	, ,	2.1	09	K	20I	62	77	03	Ž	99	*	200	67	89	77	60	10	1:	1/1	72		2	7	75	1	270	7.7	200	2	79	80	100	107	3	83	9	8	3	286	87	8	80	3	잃	201	0.2		3	*	95	206		200	7 6	7.	စ္က	DE	
Dep 1	1	134-5	135.1	125.0	. 70	130.5	137.1	117.8	000	130.5	139.1	100	43%.0	140.5		141.2	141.8		144.5	143.2	T. 2.8		144.5	145.2	746.8		140.5	147.2	0	14/00	148.5	T 40 0	7.64-	149.0	140.5		151.2	ICI.O	1,50	40 4.0	153.2	153.9	1	154.5	155-2	155.9	1.66.6	2	157:2	157.9	1.58.5	I CO.2		***	100.0	161.2	141	7 9 7 1	104.0	103.2	163.9	164.6	2 2 7 1		777-	100.0	167-2	Lat	
Lat		149.3	150.I	1 50.8		·	152.3	153.0	0	-22.0	154.5	Trees	c. ćc.	156.0	1	150.7	157.6		120.4	159.0	150.7		1000	161.2	161.0	7 - 7	104.	163.4	791	**	164.9	The		100.4	167.1	1	6-201	168.6	160		170.1	170.9	12.5	2	172.3	173.E	173.8	4 7 7 1		175.3	176.1	176.8	177.6	200	170.3	179.0	170.8	180		101.3	182,0	182.7	182	184.0	8		and I	Dep	,
Dift	13	707	03	2	3 ?	5	જ	306		3	8	6	3	OI	· Common	411	E2		43	14	1.6	1	210	17	00		49	30	13	777	22		*	24	.25	1	330	.27	200	2	-29	30	1:	431	.32	33	14		श	236	17	300		39	위	24I	4.2		•	1	45	246		,			250	Did Did	
Dep	13	0.101	101.7	FO2.4		20300	103.7	104.4		3	105.7	, 901	400	107.0		107.7	L08.4	-	0.601	100.7	TTO.4		0.111	111.7	LILT		11301	113-7		1	II5.I	116.7	2	LIOT	117.1		117.7	118.4	T.O.T		1.19-7	120.4	101	100	121.8	122.4	[22.1]	0 001	143.0	124.4	IZCE	125.8	1001	-	127.1	127.8	128.4		-	129.0	130.5	I3I.I	171 8	100	104.0	133.1	133-8	Lat	
Lat	100	7.77	112.9	TI 2.7		4.4.4	115.1	0.711	7 7	488	E17.4	1 2 1	-	118.9		0.611	120.1		14747	121.8	122.6		123,3	124-1	124.8		445.5	126.3	1000	2/4	127.8	1.38.	2	129.3	130.0		130.7	131.5	122.2	-	13300	133.7	Total	24.5	135.2	135.9	136.7	127.	-3/-	138.2	138.0	130.7	140.4	***	141.1	141.9	142.6		40.4	144.1	144.9	145.6	146.2	114	0		للم	Dep	
Diff	Ī	151	52	6.2	2	54	5.5	166	,	57	20	, ;	3,4	9	ŀ	191	62		03	49	4	1	100	67	89	2	60	70	1	17.1	72		13	74	75	1	170	47	70	0	3	03	0	101	82	003	8	0	6	186	87	88	8	6	भ	161	0.2		7,	7	95	901	0.7	200	7 6	66	8	DIE	
Dep	1	020	68.2	68.0	7 0 7	9.60	70.2	70.0	7	2.1	72.3	200	in a	73.6	1	74.3	74.9	y ::	75.0	76.3	16.0	1	77.0	78.3	78.0	7 04	2.67	80.3	000	7.00	81.6	87.3	2	83.0	83.6	1	04.3	85.0	8.6	200	00.3	87.0	8. K	200	88.3	89.0	80.6		200	0.16	01.7	02.2	200	2	93-7	94.3	0.0	200	27	20.3	97.0	97.7	200	200	77	7-66	100.4	Lat	
Lat	1	75.0	75.8	76.0	3	17.3	78.0	78.7		19.5	80.2	0. TO	0.10	81.7		82.5	82.2		03.9	84.7	8		2000	86.9	87.7	. 00	0004	89.1	100	K-Ko	9006		7	92.1	07.0		93.0	04.2	1110	2	95.9	9.96	13	5.00	98.1	08.00	900	3	3	O.IOI	S.IOI	102.5	TO 2. 2	2.0	0	104.7	Tot.	0 901		0.201	107.7	108.5	100.0	100.0		110.7	11:4	Dep	
Diff	ľ	101	02	03	3	3	05	901	1	200	80	0	3	10	1	III	42		13	11	Te	7	011	11	18		61	40		177	33		*3	-2.4	25	T	130	-27	100	2	-29	30	1	131	32	33	2.4		न	136	37	30	9	Sec.	9	171	12		5:	ţ	45	146		18	10	4	150	Diff	
Depl	1	34.1	34.8	36.6	200	30.1	36.8	27.6	200	30.1	36.8		39.3	40°I	1	10.0	ALLE		42-1	42-8	40.6	2	44-2	44.8		2	40.3	8-97		4/-5	48.2	0,0	40.0	49.5	50.2	١٥	50.0	C.T.C	2 6	7	52.9	53.5	1	24.4	54.0	5555	5602	26.0		27.5	1872	68.0	20.2	24.5	8	6000	ér.e	600	7	000	63.6	64.2	9	9 29	44.0	7.00	8	Lat	luctor
Lat		37.9	38.6	7.00	1.60	100	10.0	41.6		5.5	13./L	0	1300	9.4	I	15.3	197	0	0.0	17.5	8 2		0.6	8.61	200	2	5.1	54.0		100	13.5		7.4	55.0	56.3		50.5	57.2			28.7	4.6	1	3	6.00	51.7	124			53.9	9.79	55.52	1199	1	9	57.6	58.2	9	1.67	0000	20.0	7.1.3	1000			13.5	14.3	Dep	
Diff.	Ī	31	52	, .	5	54	35	93	, ;	57	20.5	,	34	9	k	119	62		03	79	hel	下	00	62	89		60	70	1	7	72	20	3	1	75	T	70/	.77	. 8			80	à	1 0	62	83	8.4	8	3	98	87	88	80		2	16	20	2	2 3	14	35	96		80	00		0 0		
Depli	1	00.7	01.3	3 6		02.7	03-3	0.40		04-7	1.70	7	200	06.7	1	07.4	08.0	0	600-7	1:60	TO.O		10.7	LIA	10.0		12.7	13.4	1	2	14.7	I	1	101	16.7	1	17.4	18.1	18.	700	19.4	20.I	13	-	2I.4	22.I	42.7		43.4	24:I	24.8	25.4	7.90	100	20.8	27.4	28.T	0 0	0	29.4	30-1	30.8	25.00	22.1	00	34.0	33.5	Lat	
Lat	The same of	00.7	2.10	200		03.0	03.7	04.6	-	05.4	05.0	1	200-7	4.10	-	08.1	08.0		09.7	10.4	1.1.1		11.9	12.6	12.4		-	14.9	7	20.0	16.3	17.1	-	17.8	18.6	13	19.3	20.1	20.2		24.5	22.3	100	200	23.6	34.5	25.3	office	31	26.7	27.5	28.2	20.0	200	29.7	30.5	21.2	21.0	7	34.	33.4	34.2	24.0	26.7	26.4	30	37:	Dep	
Dift	1	7	7	6	3	*	5	9	N. Contract of the second	7	200		^	Io	1	11	12		13	17	Tr	1	10	17	18	-	44	20	13	1	22	00		74	25	13	7.0	27	28		50	30	1:	3.	32	.33	37		33	36	37	800	20	27	श	14	42			;	45	46	1.0	. 8		*	2		

for 48 Degrees.

Difference of Latitude and Departure for 43 Degrees. 43

Ī	2.17	171.0	172.5	173.2	173.9	174.6	1000		175.9	176.6	177.2	7	176.0	178.6	170.2		200	180.7	181.4	T82.T	182. 1		103.4	184.1	184.8		5.501	180.2	186.8	187.5	188.2	188	180	7	1,00	190.9	191.6	192.3	193.0	193.6	194.3	10:01	10.5	7.56	1000	107.0	1972.4	198.4	199.1	199.8	200.5	201.2	201.8	202.5	203.2	203.9	204.6	1.98
700	103.0	*	185.0	185.8	186.5	187.2	187.0	000	100.7	189.4	1001	1	190.9	191.6	102.2	200	19301	193.8	194.5	106.2	2000		190.7	197.5	TOKO	200	6-061	199.7	200-4	201.I	201.0	9 000			204.0	204-8	205-5	206-2	207.0	207.7	208.4	1000	1986	-en	0.017	411.4	212.1	212.8	213.6	214.3	215.0	215,7	216.5	217.2	218.0	218.7	219.4	Den
	127	52	.53	5.4	55	256		5	50	65:	9	1	201	62	62		\$.	9	366	64	200		60	70	271		7/1	73	77	.75	276	1	184	-	2	8	28I	2	83	84	8.	186	0	90	90	66	ध	166	92	93	8	9.5	206	40	80	66	300	ارد
1	1.75	137.7	138.4	139.1	139.8	140.5	141	0	141.0	142-5	142.2		143.9	144.5	146.2		45.7	146.6	147.3	8	200	499	149.3	1500	160.7	-200	127.	152-1	152.7	153.4	154.1		- 20	200	150.2	150.8	157-5	158.2	158.9	150.5	160.2	1,60	7 - 7 -		രത		203.0	164-3	0.591	165.7	1.66.4	167.1	169.7	168.4	1.691	169.8	170.5	1
-		1-1-1	148.5	149.3	649.9	No.	K	2	1251	152.9	152.6	58	154-3	155.0	8 3 3 3 3	7	2000	157.2	158.0	1.8.7	200	2	100.2	16000	161.6		#-+ OT	103.1	163.8	164.6	165.2		1991		107.5	106.2	6.891	169,7	170.4	17IL	171.0	100		11303	174.1	17400	175.5	176.3	177.0	177.7	1784	179.2	179.0	180.6	181.4	182.1	182.8	1
	70	20	03	40	9	206		elizabera.	8	60	OF		2.1.I	12	1.2	?;	1	.I.S	216	17	2 2			30	121	_		.43	44	25	226	,	700	2 (49		23 I	all markets	33	34	35	1 3		200	.30	39	9	241	42	43	1	45	246	1	8	49	250	1
13	3		3.5	105.0	105.7	106.4	TO7.		107.7	108.4	LOOI		109.8	IIO.5	LIL	0	0-171	112.5	113.2	TT2.0	111	?	115.2	LI5.9	116.6		117-3	118.0	118.6	E19.3	120.0				122.I	122.7	123.4	124.1	124.8	125.4	126.2	8 901	2000	147.5	120.2	120,9	129.5	130.2	130.9	131.6	1,3203	133.0	123.6	134.2	135.0	135.4	136.4	1
	3	111-2	EII.9	112.6	II3.4	1.4.1	17. 8	7	15.0	116.3	117.0		117.7	118.5	LIG	000	1.4.7	120-7	12I.4	T.2.2.T	1000	A	123.D	124-3	126.1	100	0-574	120.5	127-3	128.0	128.7		4 6 5	300	1300	131.6	132-4	133.1	133.8	134.6	125.2		200	130.0	137.5	136.2	1390	139.7	140.4	141.1	I4L9	142.6	142.3	1	144.8	145.5	146.3	1
1			53			156		~0	20	5.9	99	1	191	20	62	2.7		65	166	28			6	70	171		77	73	7	7.5	176		700	0 1	,79 ,79	2	ISI	82	83	2	ě	186	6	000	000	9	थ	161	92	93	94	95	106	0.7	8	66	100	Ī
. 07	5.00	09-5	70-2	70.9	71.6	72.2	200	2	73.0	74.3	75.0	1	75.7	7.92	777		77:7	78.4	70.I	20%		200	8I.2	%.1% 0.1%	82.5	2.00	63.2	83.9	84.5	85.2	85.0	96.6	000	5.00	0.00	88.6	89.3	0.000	90.7	9.I.4	02.1	100		3	10	*	95.5	96.2	8.96	97.5	98.2	98.9	00.0	100.2	100.0	101.6	102.3	1
	73.9	74.0	75-3	76.1	76.8	17.6	0	3	200	79.7	80		81.2	81.0	84.6		03.4	84-I	84.8	8. 6	0,00	5.00	×7.0	87.8	88	5.00	2000	0006	1.06	9.I.0	02.1	1	6.26	73.0	94.3	95.1	95.8	2.96	07.3	080	08.7	1	250		60001	101.7	102.4	103.1	103.9	104.6	105.3	106.0	106.8		108.2	109.0	1001	1
İ	101	8	.03	ð	90	106	100	30	90	60	IO	1	111	12	1.2	? ;	**	15	116	4.4	1 0	9	67	20	101	1	77	-43	7	25.5	126		100	9	56	30	131	32	33	3.4	35		100	37		33	9	E	42	43	4	4.5	971	4.7	8	49	150	1
10	0.1	35-5	36-3	36.8	37.5	28.2	200	30.0	39-5	40.2	40.0		41.6	42.3	2	,	43.0	44.3	45.0	7 4 4		4 0 4	47-I	47.7	0	4004	49-I	49.8	50.5	51.2	KT. 8	3 0	52.5	•	53.9	54.5	55-4	5.5-9	9.95		80	70.	20.0	6	000	00.7	61.4	62.I	62.7	63.4	64.1	64.8	66.6	66.2	8.99	67.5	68.2	1
	37.3	30.0	38.8	39.5	40.3	41.0	Ŧ.	-	45-4	43.I	42.0	1	44.0	45.3	, ,	0 /	40.0	47.5	48.3	9 0		1	50.5	51.2	-	2	52.7	534		54-9	9:33	2	3 (200	57.0	58.5	59.2	0.09	60.7	61.4	62.2	100		03.0	4.4	05.1	3	9.99	67.3	0.89	68.7	69.5	70.2	70.0	71.7	72.4	73.1	ĺ
L	21	52	53	54	55	193		20	50	59	9	3	I9	62	43	2,4	40	65	99	Ly	700		60	70	1:	17.1	12	- 73	74	7.5	36	1	7	_		8	8	82	83	4	00	٦		0			8	16	.92	93	46	95	90	.07	80	66	100	1
13	4	4.10	03.0	52.7	03.4	04.I	8		05.5	1.90	8.90		07.5	08.2	080	1	5	10.2	IO.0	7.1		2007	13.0	13.6	14.2	7	15.0	15.7	16.4	17.1	17.7	. 0	10.4	10	19.0	20.5	21.2	21.8	22.5	23.2	23.0	1:	24.5	45.4	25.9	20.0	27:3	28.0	28.6	29.3	30.0	30.7	31.4	32.1	32.7	33.4	34.1	1
18		01.5	02.2	07.0	03.7	04.4	1.30	3	50.0	9.90	07.3	?	200	08.8	00.5	80200	3	0.11	11.7	12.4	100	200	43.9	14.0	15.4	2	1	10.0	17.6	18,3	10.01	10.7		200	41.52	21.9	22.7	23-4	24.I	24.9	25.6	192	3 4 6	100	70	40.5	29.3	300	30.7	31.4	32.2	32,9	33.6	34-4	35-1	35.8	36.6	1
	1		3	4	2			0							I		14	15	101		1 2		19	20	10	1		23	24	25	26		1 0	3	70	3	31	32	33	45	35	15	7 .	30	9	3,	9	1	42	43	4	45	94	47	84	49	50	1

for 47 Degrees.

44 Difference of Latitude and Departure for 44 Degrees,

Dep '	74.3	75.0	75.7	70.4	1 ×	78.5	79.2	6.62	80.6	181.3	182.0	182.7	183.4	84.E	184.8	185.5	1001	187.4	188.2	188.9	189.6	190.3	191.0	7.161	192.4	193.I	193.8	100.02	0,701	196.6	197.3	1980	198.1	199.3	2000	201.4	202.1	4	203.5	204.2	200	7.4.7	205.6	205.6	205.6
Lat 1	180.5 1	81.3 I	82.0 I	182.7	84.	84.9	85.61	86.3	2	7	8.5	3.5	6	190.0	3	н о	0 4	193.5	10	2.6	6.4	14	001	198.5	199.2	2000	2000.7	202.1	202.8	203.6	204.3	205.0	205.7	200.4	207.0	208.6	200.3	210.0	210.8	211.5	212.2				
)iū	115	13	53 18	4 4	19	57 I	58 I	39 1	Service of			-				007		100		_		74	7.5	276	77	78	200	3	82	83	-	10.00	17	800	0 00	0	1 291	1 92	8 93	6	9.5		7	9.0	0 10 to 0
Dep [1	139.6	140.3	141.0	141.7	43.1	43.8	144.5	45.2	45.9	146.6	147.3	147.9	148.6	149.3	150.0	150.7	151.4	172.8	162.6	154.2	154.9	155.6	156.3	157.0	157.7	158.4	159.1	Teor	161.1	161.8	162.5	163.2	163-9	164.	166.0		-			H	120		=	17	HHH
lat 1	14.6 I			47.61	नन	48.9		150.3	ZI:I	31.8	52.5	53.2	53.9	54.6	55.4	50.1	50.0	28.3	10.02	1.005	160.4	161.1	8.191	162.6	163.3	164.0	164.7	1,00	166.9	167.6	168.3	169.0	169.8	170.5	171.0	172.6	173.4	174.1	174.8	75.	176.2		17	177.	177.178.
Dift	107	02 17	H	900	H	-	1 80		임	111 I	121	131	141	151	2161	70	0 0	20.	221	22	23	24	25		27	38		4	515		34	35	236	37	20 20		7 241	4 42	1 43	44	र ा		1 240	100	4 4 4 4
Deb	6	-	106.3	107.7	108.4	109.	1001	110.4	111.1	111.8	112.5	113.2	113-9	114.6	115.3	07011		11811	8.811	119.5	120.2	120.9	121.6	122.2			124.3				1227.	128	129.	129	131	132	IH			H	3 135	4	0130		1133
Lat					1 19	6		4		00	-	_			19.4	120.1	2000	122.3	123.0	123.7	124.4	125.2	125.9	126.6	27	128.0	128.8	1 103	0	131.6	132.4	133.1	-	H +	136.0	1 2		138:1	138.8		140		141	141	1 1 4 4
Did	131		531	241	193	7	_	6	_		62 1				100	600	3 &	75	12	72	73	74	7.5	17	77	78	79	١٥	00	8	00		-	2 00 00 00 00 00 00 00 00 00 00 00 00 00	N. Par	0	15		3 93	0	7	7 4 4	4 190	4 H X	1
Dep	70.2	70.8	71.5	72.0	73.6	74.3	75.0	75.7	76.4	77.1	77.8	78.5	79.2	79.9	80.6	01.3	0 00	83.4	84.0	84.7	85.4	86.1	86.8	87.5	800		89.0		91.	92.7					999		97.9	98.	~	2	m .		don't	ALL PROPERTY OF	AND DESCRIPTION OF THE PARTY OF
Lat	72.6	73.4	74.1	75.5		77.0	77.7	78.4	1.64	29.8	80.6	81.3	82.0	82.7	83.4	04.2	8.5	86.3	87.0	87.8	88.5	89.3	89.9	9006	91.4	92.1	92.8	04.2		95.7	96.4	97.1	97.8	98.5	100.0	100	101	102,1	102.	103	104		103.0	105	105.
Diff	IOI	03	03	7 0	100	6	80	60	의 의	III	12	13	14	F	1.16	17	9 6	200	121	22	23	4	2	126	27	78	29	2 2	32	7 33	3 34	35	7 136	37	200	5 40	141	9 42	6 43	3 44	0 45	77.41.4	140	4 4 7 4 7	4 4 4 4
Dep	35.4	36.1	36.8	37.5	28.0	39.6	40.3	41.0	41:7	43.4	43.I	43.8	44.5	45.	45.0	40.5	47.4	48.6	40.7	8	5 50.7		25.0	7 52.8	53.5	54.2	54-6	200	0 57.0	7 57.	4 58.	5	9 59.	0000	0 61	7 62.	5 63.	2 63.	9 64.	.6 65.		47.4	000	8 67	9.867
Lat	36.7	5 60	38.1	3 6	No. of Lot	41.0	41.7	42-4	043.2	(43.9	44-6	3 45-3	4 46.0	240.5	047-5	40.0	0 0	0 00		2 51.8	3 52.5	3	5 53.9		7 55.	5	79 50-		82 59.	, 50			\$6 6I.	88 67	80 64	0	916	92 66.	93 66-	94 67	25	4140	90 00	97 69	99 79 99 79 99 79 99 79 79 79 79 79 79 7
p Dift	7 51	4 52	3 -53	54	10	91 57	6 58	3 . 59	5	9	.3 6.	9	.7 6	4	0 1.	0 7	5.0	10	1 9	.3	0.	7 7	1.4 7	8.1 7	8.8	4.	M 00		2.5	2.9	3.6	4:3	5.0	5.7	7:1	2.00	8.5	9.3	6.6	9.0	1.3		2.1	2.6	3.3
t De	.700	.4 OT.	.202.	600	5 6	000	.800	.5 06.	.2 06	1.907	809.8	60 4.0	0	10.8	1.5 11	7.5	7 6 7	4.4 1 2	15	8.8	6.5 16	7-3 16	000	8.7 11	9.4 1	T-0	6.0	2.2	3.0	3.7.2	4-5 2	5.2 2	15.92	20.0	2 2 2	28.82	29.5	30.2	30.9 2	31.63	2.43	4 0 0	33.0	33.00	33.00
A 1.2	00	ROI	3 02	4 02	9 9	7 05	805		입	-	12 08	13 09.	IA IC	15	191	1 0	101	20 1	211	22 1	23 1	24 1	25 I	26 1	27 1	20	200	210	32	33 2	34 2	35 2	362	200	30 2	40	7	42	43	\$	7		2	144	1 4 4 4 1 2 0 0

for 46 Degrees.

-		264	2.4	200	3223		Tiple (II)	150000	SARRIO	1010	4395	LOSSO D	100	400	140,700		(SALE)	dr age	U)SE	-	-	1			100		NA.	the Co		-		12	2		~	100		-	4	*		~	20	-		5	25	0	7	1	1	6600
Dep	177.5	178.2	178.9	179.0	180	181.0	181.7	182.4	183.1	183.8	284.5	186	200	100	100.	187.4	188.	188.	189.5	190.2	190.0	191.6	102.	193.0	103	194	195	IOK	106.	197.	198.	198.	199.	200.	200	201.	202	202-	203-	204	205.	205	206.	207.	207.	208.	200	210.	210.	211.	101	
Lat	177.5	77		29.0	180.3	181.0	181.7	182.4	183.1	183.8	84.5	186.3		0.001	100.7	187.4	188.I	188.8	189.5	190.2	190.9	191.6	192.1	101.0	103.7	194.4	105.2	105.0	106.6	197.3		198.7	199.4	2,00°E	200.8	201.5	202.2	202.9	203.6		205.I	205.8	206.5	207.2	207.9	208.6	200.3	210.0	210.7	411.4	Con	-
Did	251	52	53	dinosts dinos	SCORE OF	250	57	58	59	99	192	6.9	;;	-		5	266	67	89	69	10	271	7.2	7.3	74	75	276	77	78	79	80	281	82	83	84	85	286	87	88	89	9	291	92	93	94	9.5	962	97	98	99		
Dep [1		47.8	43.5	44.2	44.9	45.7	40.4	47.E	47.8	48.5	40.2	40.0	4	200	51.3	52.0	152.7	53.4	1.461	154.8	155.6	166.3	17.0	167.7	1.8.4	1.69.1	150.8	160.5	161.2	161.9	162.6	163.3	164.0	164.7	165.5	166.2	6.991	167.6	168.3	0.691	169.7	170.4	171.1	171.8	172.5	173.2	173.9	174.6	175.4	170.1	17000	No. of Concession,
Lat 1	12.1	12.8 I	43.5 I	44.2 I	44.9 I	45.7 I	46.4 I	47.I	47.8 I	48.5 1	100	40.01	4,64	50.0	51.3	52.0	152.7	53.4	54.1	54.8	35.6	56.3	67.0	1.67.7	58.4	1.00 E	8.03	60.0	61.2	61.0	62.6	163.3	64.0	164.7	165.5	166.2	6.991	67.6	168.3	0.691	169.7	170.4	171.1	171.8	172.5	173.2	173.9	174.6	175.4	170.1	170:0	1.00
Dift-1	101	02 I	03 1	04 E	2	200 I	07 I	180	1 60	IOI	12	12.		13	141	15	316 I	17 1	181	1 61	20 1	221	22	21	2.4	25	226		28		30	231	32	33	34	35	236	37	38	and the same		241	42	43	44	45	246	47	48	49	2,50	
Dep	8.90	07.5	08.2	108.9	109.0	110.3	0.111	IIII)	112.4	113.1	117.8	14.6			110.0	1.00.7	117.4	118.1	2.811	119.5	120.2	120.9	121.6	122.3	143.0	123.7	124.4	124.2	125.0	126.6	127.3	128.0	128.7	129.4	130.I	130.8	131.5	132.2	132-9	133.6	134.3	135.1	135.8	136.5	137.2	137-9	138.6	139.3	140.0	140-7	1410	
Lat	106.8	107.5			1000000	SECTION.		.7	112.4	13.1				200	0 1	110.7	117.4	181	118.8	119.5	120.2	120.9	121.6	122.3	123.0	123.7	124.4	125.2	125.0	126.6	127.3	128.0	128.7	129.4	130.I	130.8	131.5	132.2	132.9	133.0	134.3	135.1	135.8	136.5	137-2	137-9	138.6	139.3	140.0	140.7	Den	Such as
Did	131	52 1	531	54	21	0			59	9	161	29	;	100	4 4		9	7	2000		70	171	72	7.3	74	75	176	77	78	79	80	181	87			85	186	87	88	89	श	161	92	93	94	95	961	97	86	66		
Dep 1	71.4	72.I	72.8	73.5	74.2	74.9	75-7	70.4	77.1	77.8	78.€	70.2	10.0	200	3 3	4:10	85.0	62.7	63-4	84.1	84.8	85.6	86.3	87.0	87.7	88.4	89.1	80.8	90.5	91.2	91.9	92.6	93.3	94.0	94-7	95.5	96.3	6.96	97.6	98-3	800	66-7	100.4	IOI.I	8.101	102.5	103.2	103.9	104.6	105-4	10	Section 1
Lat	71.4	72:1	72.8	73.5	74:5	74-9	75.7	4.6	77.1	77.8	78.5	70.2	70.0	400	2	41:4	82.0	62.7	63-4	84.1	84.8	85.6	86.3	87.0	87.7	88.4	89.1	80.8	90.5	91.2	91.9	93.6	93-3	94.0	94.7	95.5	96.2	6-96	97.6	98.3	99.0	2-66	100.4	IOI.I	8.101	102.5	103.2	103.9	104.0	105.4	100	Sheeks an
J)'U	IOI	070	03	04	(S)	00	6	80	60	IO		12	1,	? :	* :	नं	OII	17	21	19	2	121	22	23	24	2.5	126	27	78.	29	30	I3I	32	33	34	35	136	37	38	39	9	141	42	43	44	45	146	47	48	49	1	
Dep	36.1	30.8	37.5	30.7	30.9	39-0	40.3	41.0	41.7	42.4	42.I	4 2 00		2	45.3	40.0	40.1	47.4	48.1	48.8	49.5	50.2	50.9	\$1.6	52.3	53.0	53.7	54.4	55.2	55.9	56.6	57.3	58.0	58.7	59.4	100 100	8009	61.5	62.2	67.0	63.6	64.3	65.I	65.8	66.5	67.2	67.9	989	69.3	70.0	非	
Lat	36.1	800	37.5	30.0	200	39.0	0.3	0.1	41.7	43.4	4 2.I	43.8			5.5	000	40.7	47.4	48.I	48.8	49.5	50.2	50.0	5 I.6	52.3		53.7	54.4	55.2	55.9	56.6	57.3	58.0	58.7	59.4	60.I	8.09	61.5	62.2	67.0	63.6	64-3	65.1	65.8	66.5	67:2	62.0	9.89	29-3	70.0		S. Belleville
Dift	SI		53		55	20	57		39	-	67	62	6.3	3.	4.4	5	0,	07	90	69	2	71	72	73	74	75	76	77	78	79	80	81	87	83	4	2	86	87	88	68	8	91	92	93	94	25	96	97	98	700		
Depl	2.00	OI.4	02.1	07.8	3.5	04.2	04-0	03.7	6.4	07.1	8.40	28.0	200	7.60	6-60	10.0	II.3	12.0	12.7	13.4	14.1	14.8	15.6	16.3	17.0	17.7	18.4	IO.I	10.8	20.5	21.2	21.9	22.3	23.6	24.0	24.7	25.5	26.2	26.9	27.0	28.3	29.0	29.7	30.4	31.1	31.8	32.5	33.2	33-9	34.0	3 5	
Lat	00.7	0I.4	03.1	07.8	57	04.2	6-40	05-7	06.4	07.I	07.0	80	200	3	6-60	000	II.3	13.0	12.7	13.4	I4.1	14.8	15.6	16.3	17.0	17.7	18.4	1.61	19.8	20.5	21.2	21.9	22.3	23.6	24.0	24.7	25.5	26.2	26.9	27.6	28.3	29.0	29.7	30.4	31.I	31.8	32.5	33.2	33.9	34.0	1000	
Diff	F		ñ	4	-	•	~	x	6	10	1	12		2:	4:	7	91	17	18	19	30	21	22	23	24	2.5	26	27	200	29	30	31	32	33	34	35	36	37	38	39	9	41	42	43	44	4	40	4	4	404	No.	

for 45 Degrees.

Numbers for the readier finding the Course in the foregoing Tables of Difference of Latitude and Departure.

Dep.	100	3	86	80	2	8	200	*	83	83	81	100	2	26	78	77	26	7.5	7.4	;	2:	1	11	20	69	89	67	99	65	64	63	29	19	8	59	28	57	So	55	24	53	52	51	20	4	40	4,	ę:
t. and		1000	5882	2855	2061	1432	1145	950	919	711	612	13	200	212	470	433	401	373	340	328	300	4	290	275	700	248	236	225	214	205	196	188	180	173	166	100	154	148	143	138	133	128	123	611	115	111	107	103
Diff. of Lat. and Dep	T. Sec.	常	H	es.	6	•	ימי	•	7	∞	•	1:	2 :	1	17	13	14	15	91	17	- ox	:1:	61	8	21	22	23	24	2,5	3 6	27	28	29	30	31	32	33	34	35	36	37	38	39	4	41	42	43	4:
Diff.	2	10000	d	3	5	7	6	9	12	14	91	10	9 5	61	2.1	23	2.5	2.7	20	2	, ;	1	34	36	38	9	43	45	47	49	31	53	- 55	28	0	62	S'o	02	20	73	7.5	78		*	87	8	93	96
			-								*											ALC:						7																				
ture.	1	100	68	00 c	200	8	200	**	83	83	81	100	2	79	78	77	26	7.5	7.4	12	2 5	1	71	20							63				59		le le		55	7	.53	52	SI	င္သ	49	48	47	\$:
Depar	N		1000	666	866	664	966	995	993	066	980	100	200	706	978	974	970	996	190	900	120	-	945	940	934	927	921	914	906	899	891	883	875	900	857	648	633	626	819	의 의	799	788	777	700	755	743	731	719
Diff. and Departure.	0		1	et	63	+	, ,	٥	7	∞	٥	1:	01	:	13	13	14	11	91	1.1		3	19	20	2.1	22	23	24	2.5	3.6	27	28	29	30	31	32	33	34	35	36	37	300	39	9	+	4	43	\$
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and	-		-	*	3	4	s)	•	7	00	0	1:	0 1	1	12	13	14	1.5	91	.52	10	ei.	19	30	21	23	23	24	2.5	26	27	78	29	30	31	32	33	34	35	위	37	38	39	9	41	42	43	1:
Dif.	200	BIG.	1000	666	866	266	066	995	993	066	088	او	200	902	978	974	970	996	190	930	200	il il	945	940	934	927	921	914	906	899	891	883	875	998	857	848	839	829	819	80	799	788	777	200	755	743	731	719

The Use of the Tables of Difference of Latitude and Departure, in working any of the Cafes of Plane Sailing.

contains 50 miles in each column, the first beginning at 1, and ending at 50; the second beginning at 51, and ending at 100, and so to 300 miles distance; and to each of these columns of distances there to observe, that if your course be found at the top of the tables, then you are to take the difference of latitude and departure as they are In these Tables, the course, if less than 4 points, or 45 degrees, will be found at the top of the tables; but, if it is more than 4 points, or 45 degrees, it will be found at the bottom of the tables; and on every fide there are fix columns for the distances, marked Dist. which being two other columns, shewing the difference of latitude and departure to any of the distances marked Lat. and Dep. in which you are marked at top; but, if your course be found at bottom, then you must take them as they are marked at bottom. Note, In any case where the course is given in points, half points, or quarters, you must make use of the following tables of difference of latitude and departure, which are calculated for points, &c.; but where must make use of the foregoing tables of difference of latitude and the course is given in degrees, or where it is not given at all, you

PLANE SAILING.

CASE the First.

Course and Distance being given, to find the Difference of Latitude and Departure.

RULE

latitude and departure answering to that distance, will be the difference Find your course as before directed, and look in some of the distance columns belonging to that course, for your distance, the difference of of latitude and departure required.

EXAMPLE

A Ship fails NNE. 136 Miles, I demand the Difference of Latitude and Departure.

Having found my course, which is 2 points, in the table for points, find my distance 136 in the third column for distances, and right against that, I find 125.7 for my difference of latitude, and 52.0 for my departure.

Note, In all cases whatsoever, if the given side or sides be in miles, then the sides found by the table, will be also in miles; but, if the given side or sides be leagues, then the sides found will also be leagues.

Plane Sailing. Cafe the Second.

Course and Difference of Latitude being given, to find the Distance and Departure.

Find your course as before, then look in some of the difference of latitude columns belonging to that course for your difference of lati-tude, the distance and departure answering to that difference of latiwill be the distance and departure required.

EXAMPLE.

A Ship fails S. 48 Deg. o Min. E. until her Difference of Latitude be 164 Leagues, I demand her Distance and Departure?

look in some of the columns marked Lat. at bottom, for the nearest I can find to my difference of latitude, which is 163.9, and answering to that, I find for my distance 245 leagues, and for my departure 182.0 Having found my course 48 degrees at the bottom of the tables,

Plane Sailing. Cafe the Third.

Course and Departure being given, to find the Distance and Difference of Latitude.

RULE.

columns belonging to that course, for your departure, the distance Find your course as before, then look in some of the departure

and difference of latitude answering to that departure, will be the distance and difference of latitude required.

EXAMPLE.

A ship sails south west by south until her Departure be 165 miles: I de-mand her Distance and Disference of Latitude.

Having found the course, which is two points, at the top of the table of points, I look in fome of the columns marked Dep. at top, for the nearest I can find to my departure, which is 165.0, and answering to that, I find for my distance 297 miles, and for my difference latitude 246.9 miles.

the table, then divide it by 2, 3, 4, or any other number that will make it small enough to be found, and then the required sides, when found, must be multiplied by the same number; but the course must Note. In any case where the given side is too large to be found in never be multiplied nor divided.

Plane Sailing. Cafe the Fourth.

Distance and Difference of Latitude being given, to find the Course and Departure.

RULE.

tenths, as for example, 111.4, 207.9, &c. fo that if at any time either of them should be given in miles without tenths, as 117, 124, &c. you are then to put a cypher to them, to supply the place of tenths, and call them 117.0, 124.0, &c. and then put two cyphers the course is to be found by the table of numbers, the difference of latitude and departure are supposed always to be in miles and Put two cyphers to the difference of latitude, and divide it by the the miles and tenths) and note the quotient: Then look in the table of numbers (at the end of the tables of difference of latitude and departure) in the columns belonging to distance and difference of latitude, for the nearest number to that quotient, the degrees answering to that number will be the course. Then, to find the departure, proceed as in case the first. But here you are to observe, that in all cases where more, according to your other rules, to find the number for the distance, (without taking any notice of the point that stands between

EXAMPLE.

A ship sails between north and west, until her Distance is 276 miles, and her Difference of Latitude 211,4 miles: I demand her Course and Departure.

Having put two cyphers to the difference of latitude, which makes it 211400, I divide by the distance 276, and find the quotient to be 766 nearly; then I look in the table of numbers (under Dist. and Diff. grees for my course, and with that course, and my given distance, I find my departure to be 117.4 miles, by case the first. of Lat.) for the nearest to it, which is 766, against which I find 40 de-

Plane Sailing. Case the Fifth.

Distance and Departure being given, to find the Course and Difference of Latitude.

R II L E.

Put two cyphers to the departure, then divide it by the distance, and look in the table of numbers, in the columns belonging to distance and departure, for the nearest number to the quotient; the degrees answering to that number will be the course, and then the difference of latitude may be found, by cafe the first.

EXAMPLE.

ship sails between the South and East, until her Distance is 546 miles and her Departure 412 miles: I demand her Course and Difference of

for my course; and with that course and my distance (divided by 2, because it is too big to be found in the tables) I find a difference of distance was divided by 2, gives 358.2 for my whole difference of la-546, and find the quotient to be 754, against the nearest to which, viz. 755, in the table of numbers, under Dist. and Dep. I find 49 degrees which makes it 412.0, and then two more cyphers, according to the rule for this case, which makes it 412000, I divide it by the distance Having put a cypher to my departure, to supply the place of tenths,

Plane

Plane Sailing. Cafe the Sixth.

Difference of Latitude and Departure being given, to find the Course and Diftance.

RULE

Put two cyphers to the departure, and divide it by the difference of to difference of latitude and departure, for the nearest number to the quotient, the degrees answering to that number will be the course, then to find the distance, proceed as in case the second or third. latitude, then look in the table of numbers, in the column belonging

A so is a so it is between the north and west, till her Difference of Latitude is 184 miles, and her Departure 115 miles: I demand her Course and Distance.

find the quotient to be 62; against which, in the table of numbers, under difference of latitude and departure, I find 32 degrees for my course, and with that course, and my difference of latitude (by case them 184.0 and 115.0, I then put two cyphers to the departure, which makes it 115000, and divide it by the difference of latitude 1840, and Having supplied the place of tenths in both these sides, which makes the fecond) or with that course, and my departure (by case the third) I find my diffance to be 217 miles.

case in traverse, mercator, parallel and middle-latitude, only by supposing the names of the sides and angles in mercator, parallel, and middle latitude, to be changed into the sides and angles they represent By these foregoing rules for Plane Sailing, you may work any

TRAVERSE SAILING.

The several Courses and Distances a ship sails being given, to find what direct Course and Distance she has made good, and her Difference of Latitude and Departure.

Make a table as on the following fide, and fet down in it your Make a table as on the following fide, and fet down in it your dake a table as on the first of the first of diameters: then, by the rule for case the first of several courses and distances; then, by the rule for case the first of Plane Sailing, find the difference of latitude and departure to each

to the courses they belong to, taking notice that the difference of latitude must always be set in the north column, if the course be northerly, and in the south column, if the course be southerly; and the of the courses and distances, and set them down in the table opposite

column; and if you have but one column of northing or fouthing, and but one of calling or welting, then their fums will be the difference of latitude and departure of the fame name with the column they stand under: That is, the difference of latitude will be northerly, if it stands under the north column; and the departure easterly, if it stands undeparture must always be put in the east column, if the course be casterly, and in the west column, if it be westerly.

Then add up all your columns of north, south, east, and west, separately, and set down their respective sums at the bottom of each

der the east column, &c.

of latitude, of the same name with the greater of them: Also do the same with the sums of the cast and west columns for the departure; . But, if you have numbers in all the columns of north, fouth, eaft, and west, then take the sums of the north and fouth columns, and then, with that difference of latitude and departure, find the course subtract the less from the greater, the remainder will be the difference and distance, as in case the fixth of Plane Sailing.

EXAMPLE.

A ship sails the following Courses, viz. S. S. W. 54 miles, W. by S. 39, N. W. by N. 40, N. E. by E. 69, and N. N. W. 60 miles: I demand her direct Course, Distance, Disference of Latitude, and Departure.

Note, 'Tis by this method that

46.7 23.0 38.2 22.2 20.7 104.1 Weft Departure. 69.5 Dep. Wly. Eaft Diff. of Lat. 49.9 North Sout. Diff. of lat. Nly 69 Q

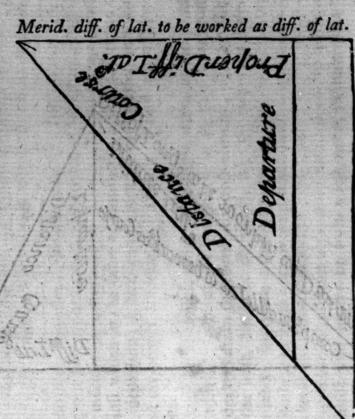
longitude made; all which will be further explained in the rules for the difference of latitude and departure are found in working any difference of latitude and departure fo found, we find the courfe, reckoning, meridian distance and day's work at sea; and from the distance, and latitude by deadkeeping a journal. Courfe 34.00 W. distance 84 miles.

To work any Right-angled Triangle by the foregoing Rules for PLANE SAILING.

In all right-angled triangles that are to be worked by the tables, you are to suppose four things, viz. Course, Distance, Difference of Latitude and Departure, two of which must always be given to find the if you would work any other failing by them, as mercator, parallel, middle latitude, or any other right-angled triangle, you must suppose that the sides and angles of that triangle are to be called by the same name that the fides and angles they reprefent in Plane Sailing are called other two: Then, as these rules are wrote for working of Plane Sailing, by, and then work them as if it was a cafe of Plane Sailing.

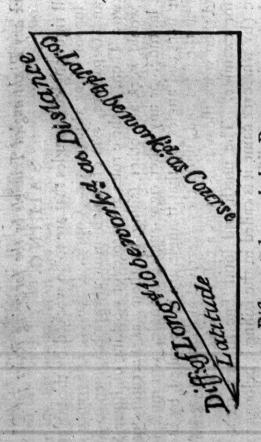
As for example. The north and fouth line in any right-angled triangle (by whatever name it is called in the failing it belongs to) must be worked as if it was a difference of latitude in Plane Sailing: The For example, take eaft and west line as departure; the long side as distance, and the angle opposite to the east and west line as course. the following figures.

Figure for Mercator's Sailing.

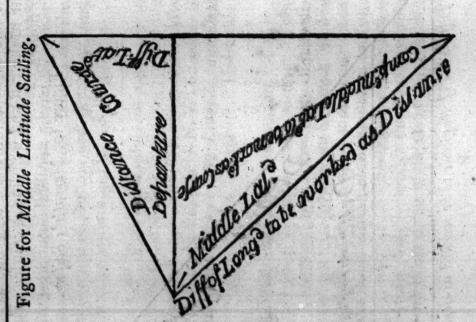


Difference of longitude to be worked as departure.

Figure



Distance to be worked as Departure.



Mercator's

The latitude and longitude of any two places being given, to find what course and distance a ship must sail from one place to the other.

RULE

Having the two latitudes and two longitudes given, find the proper difference of latitude, the meridional difference of latitude, and the difference of longitude, as by the rules for that purpose; then, with the meridional difference of latitude, and the difference of longitude (taken as difference of latitude and departure) find the course by the fixth cafe of Plane Sailing, and with that courfe, and the proper difference of latitude, find the distance by case the second of Plane Sailing.

EXAMPLE.

What course and distance must a ship sail from a place in latitude 50.00 north, and longitude 03.10 west, to a place in latitude of 17.10 north,

Lat. failed from _____ 50 00 N. Meridional parts. | Long. failed from __ 93 10 W. Lat. bound to ____ 17 10 N. | 3474 | Long. bound to ___ 59 11 W. 3474 1046 and longitude 59.11 west.

56 or W.

tude and departure) I find 54 degrees for my course, and with that course and my proper difference of latitude, I find my distance to be it by the meridional difference of latitude, I find the quotient to be 138, against which in the table of numbers (under difference of lati-Proper diff. of lat. 1970 miles. J Mer. diff. of lat. J Diff. of Long. 3361 miles. Having put two cyphers to the difference of longitude, and divided 3348 miles.

The course being thus found in degrees, I want, in the next place, to know which quarter of the compass it is in, that is, whether it be so many degrees from the north towards the east, or from the north towards the west, &c. To do which, take the following Rule. If you are to sail from a greater north latitude to a less, or from

north latitude into fouth; or from a leffer fouth latitude to a greater, then you must fail to the fouthward.

But if you are to fail from a greater fouth latitude to a left, or from fouth latitude into north; or from a left north latitude to a greater, you must fail northward.

less well longitude to a greater, or from east longitude into west, you must fail to the westward, except the difference of longitude be more than 180 degrees, and then you must fail to the eastward. If you are to fail from a greater east longitude to a lefs, or from a

a lefs cast longitude to a greater, or from west longitude into east, you must sail to the eastward, except your difference of longitude be more than 180 degrees, and then you must sail to the westward.

E X A M P L E. But if you are to go from a greater well longitude to a lefs, or from

In the foregoing case of Mercator's sailing, I find by the two latitudes, that I am bound from a greater north latitude to a lefs, viz. from 50.00 N. to 17.10 N. then by the Rule I must sail to the southward; gitude to a greater, viz. from 3.10 well, to 59.11 well; then by that Rule I am to go to the wellward, therefore, my course will be fouth and I find by the two longitudes that I am bound from a lefs well lon-

54.00 west, or SW. three quarters west nearest.

This first case of Mercator, being the case that is always made use of to find the course and distance from place to place, or to find the bearing and distance of any place from the ship at any time, I have set down the work of it at large, and shall leave the other cases for the reader to exercise himself with, by working them by the rules already given him. A Table of the Angles which every Point and Quarter-point of the Compass makes with the Meridian.

N. 60 5 5	23.00
. 6 % 7.85 . 6 % 7.85	81 84 87 90
7222	なななる
M. 388 20 15 15 15	53 41 30
55 55 4 D.	62.45
4440	
M. 19	#4:8
3 8 8 8 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9	4 2 3 9 5 4 5 5
44-hat 60	apakat 4
7.02 5.0 T. 5.0	34.20
G 4 20∞ I	49.02
the plant	The man of

as follows: Suppose I would know how many deg. 5 points are, then I look for 5 points, and against it I find 56 d. 15 m. Or, if I would know how many points, 42 d. 17 m. are, I look for the nearest to it, which is 42 d. 11 m. and against that stands 3‡ points. The use of this Table is to turn points into deg. or deg. into points,

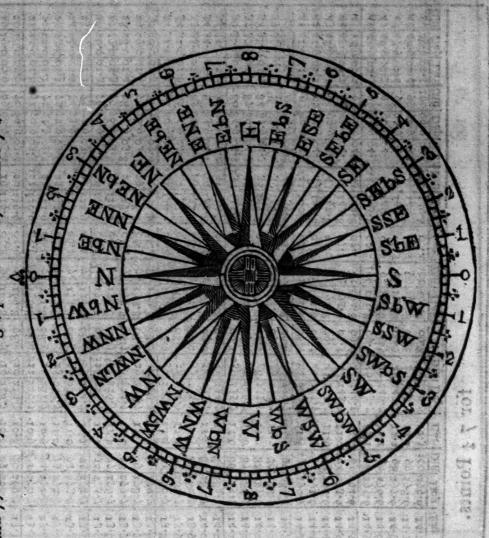
The courses and distances being set down in a traverse-table, as in page 52, it will be found necessary, for the ready looking them out in the table of difference of latitude and departure, to know what angles they make with the meridian, or (as we commonly fay) to know how many points there are, for which reafon I have here given the figure of the Mariner's Compass, which is to be used as follows.

Example 1/1. Suppose I would know how many points I must look out for in the tables of difference of latitude and departure, for a

SW. by W. courfe.

Look in the figure below, and against the point marked with SW. by W. you will see the figure 5, which shews that you must look out 5 points.

Example 2d. How many points is E. by N. # E. Against E. by N. find 7, and my course being # points more, it mkes 7 #.



TIOOOOOOOOOOOHHHHHHHHHHHHHHHHHHHHHHHHHH	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
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for 7 4 Points.

Dep	24.6	24.7	24 8	24.9	25.0	25.1	25.2	25.3	25.4	25.5	36.6	26.7	200	25.0	25-9	26.0	26.1	26.2	26.3	26.4	26.5	990	2000	7.07	20.0	40.0	27.0	27.1	27-2	27.3	27-4	27.5	27.0	27-7	27.0	27.9	20.07	28.I	79.7	28.3	20.4	20.5	28.0	28.7	20.00	28.9	29.0	29.1	29.7	29.2	29-3	29.4	Lat
Fat	240.8	250.8	251.8	252.8	253.8	254.8	255.8	256.8	257.8	258.8	260.7	260.2		201.7	202.7	263.7	264-7	265.7	266.7	267.7	268.7	7 090	7.607	270.7	271.7	272-7	273.7	274-7	275-7	270-7	277.7	278.7	279.6	280.6	281.0	282.6	283.0	284.6	285.6	286.6	287.6	288.0	289-6	200.0	291.6	392.6	293.0	304.6	295.0	296.6	297.0	298.0	Dep
	25 I	52	53	54	55	256	57	500	59	9	196	13	3	63	64	65	266	67	68	99	70	1	1/1	72	73	74	73	276	77	78	79	8	28I	80	83	%	100	286	87	88	89	위	162	92	93	16	36	962	97	98	66	8	3
dan	19.7	19.8	19.0	20.0	20.1	20.3	20.2	20.3	20.4	20.5	30.6		1	20.8	20.0	21.0	21.1	21.2	21.3	21.4	27.6	2	21.0	21.7	21.8	21.9	22.0	22.1	22.2	22.3	22-4	22.5	22.6	22.7	22-8	22.9	23.0	23.I	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23-9	24.0	24.1	24-3	24.3	24.4	24.5	Lat
	0000	201.0	0.20	03.0	204.0	0.50	20000	207.0	0.800	200.0	110.0			77.0	213.0	214-0	215.0	216.0	217.0	217.0	218.0		6.617	220.9	221.9	577.0	223.9	224-9	225.9	570-6	227.9	228.9	429-9	430.0	431.9	432-9	233.9	234-9	435.9	436.9	237.9	238.9	239.8	240.8	241.8	242.8	243.8	244-8	245.8	246.8	247-8	248.8	Den
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	14.8	14.9	15.0	15.1	15.2	15.3	15.4	15-5	15.6	15.7	1:	2	13.0	15.9	16.0	16.1	16.2	16.3	16.4	16.6	16.6		10.7	10.0	10.9	17.0	17.1	17.2	17-3	17.4	17.5	17.0	17-7	17.8	17.9	18.0	18.1	18.2	18-3	18.4	18.5	18.0	18.7	18.8	18.9	19.0	19.1	19.2	19.3	19.4	19.5	19.0	Lat
No. of Lot	150.3	151.3	152-3	153-3	154.3	155.3	1,56.2	157.2	158.2	159.2	1,000		7.17	102.2	163.2	164-2	165.2	166.2	167.2	168.2	160.2		170.2	171.2	172.2	173.2	174.2	175.2	176.2	177.1	178.1	179.1	180.1	181.1	182.1	183.1	184.1	185.1	186.1	187.1	188.1	189.1	1,061	191.1	192.1	193-1	194.1	195.1	1961	EX. 30	0.861	199.0	Den
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Marked and	6.60	0	IO.I	10.2	10.3	10.4	10.5	10.6	10.7	IO.8	10.0		2	11:1	11.2	11.2	11.3	11.4	II.e	9-11		/	11-8	11.9	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	14.0	14.1	14.2	14.3	14-4	14.5	14.6	14:7	101
s.	1001	IOI.S	102.5	103.5	104.5	105.5	106.5	107.5	108.5	100.F		5	5.11.5	112.5	113.5	114.4	115.4	116.4	1.57.4	2		1.7.4	120.4	121.4	122.4	123.4	124.4	125.4	126.4	127.4	128.4	129.4	130.4	131.4	132.4	133-4	134-4	135-3	136.3	137-3	138.3	139.3	140.3	141.3	142.3	143-3	144-3	145-3	146.3	147.3	148.3	149.3	Den
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	6.0	Z.S	5.2	5-3	05.4	05.5	05.0	05.7	05.8	0.50	15	,	1	2.00	06.3	26.4	5.90	9.90	2.90	200	90		6-00	02.0	27.1	07.2	67:3	7.4	5-10	27.6	07.7	07.8	6.40	080	08.1	08.2	08.3	08.4	08.5	9.80	08.7	8.8	98.9	0000	1.60	09.2	09.3	9.4	09.5	9.60	60.7	8.60	100
	0.80	1.80	2.7	3.7	34-7	55.7	26.7	57.7	58.7	59.7				02.7	7	64.7	65.7	66.7	67.7		200	3		71.7	72.0	73.0	74.6	75.6	20.07	9.24	78.6	9.62	9	T.6	3.6	3.6	84.0	85.6	86.6	87.6	88.0	89.6	9006	91.6	92.6	93.5	94.5	95.5	96.5	97.5	98.5	25.52	Den
	715	52	5.3	54	55	56	57	58	59	9	T.			-		65	99	67	200000			238,000	71	72	73	-	-	76	77		79	8		-	83	**	ळ्	98	87	000	89	90	16	92	93	2	9.5	96	97	98		8	Did
	1.00	200	20.3	4-00	5.00	9.00	00.7	00.0	6.00	0.10	1.10		***	01.3	4.10	01.5	0.10	OI.7	8.10	01.0	02.0		7.70	02.2	02.7	02.3	62.4	02.5	07.0	02.7	07.8	57	03.0	03.1	03.2	03.3	3:4	03.5	03.0	03.7	03.0	श	040	04.1	04-3	04.3	4.4	04.5	04-6	04.7	04.8	04.9	124
	01.0	02.0	03.0	04.0	05.0	0.90	0.70	0.80	00.60	10.0	TO.0	No		12.9	13.9	14.9	15.9	16.91	17.0	18.e	TO.0	13	50.0	21.9	22-9	23.9	24.9	25.9	50.0	27.9	28.9	Sign Sign Sign Sign Sign Sign Sign Sign	30.0	31.0	32.8	33.0	34.8	35.8	36.8	37.8	30.0	39.8	40.8	41.8	42.8	43.8	44.8	45.8	40.8	47.8	48.8	황	Den
	I	7	and the last	14	2	9	7	00	6	OI	-			13	14	15	91		× 1		20			2.2		4	2.5	26		700		R	31	33	33	34	श्र	36	37	300	39	위	41	42	43	1	4	46	47	4	49	왕	Diff

for 7# Points.

36165		e e e e e e e e e e e e e e e e e e e	Name of Street	ndage	ering	rations		i i je i na	toko	95.00	r-		elami	gran.	Salta	636		25 10			i i									Wales -		Sin Marin	Links.	1				45%	day N		190 5	Code		(III)	M- 1/	Sale:	45	dispray		5, 40	ter? to	1000
Dep	36.8	37.0	37.1	37.3	37.4	37.5	37.7	37.8	18.0	38.1	180	200	30.4	38.0	38.7	38.0	39.0	39.2	30.3	30.5	39.6	39.7	30.0	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	41.5	41.6	41.8	41.9	42.1	42.2	42.4	42.5	42.7	42.8	43.0	43.1	433	43.4	43.0	43.7	43.0		-
Lat	33	249.3	a	2	252.2	19	254.2	255.2	246.2	257.2	2.8.2		439.1	200.I	191192	262.1	263.1	264.1	265.1	266.I	1.67.I	1.897	269.0	270.0	271.0	272.0	273.0	274.0	275.0	276.0	277.0		278.9	279.9	280.9	201.9	282.9	283.9	284.9	405.9	280.8	287.8	288.8	209.0	290.0	274.0	292.8	293.8	294.0	206.7	4700	430
	(Britisana)	522	-	CONTRACTOR D	55 2	1562		582				CHARGE STORY			64	5	992		89	69	70	271	72	73	74	75	276	77	300	79	8	281	87	83	× 4	न्न	286	82	800	60	ध	162	92	93	4	3	290	97	2,5	200		
Dep I	_	29.6	8.62	29.9	30.I	30.2	30.4	30.5	30.6	30.8	2		31.1	31.2	31.4	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.8	33.0	33.1	33.3	33.4	33.6	N	33.9	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.0	35.2	35.3	35.5	35.0	35.0	1	30.1	30.2	30.4	30.5	100	7007
SEE SE	98.8	8.661	200.8	8.10	202.8	203.8	204.7	205.7	206.7	207.7	208.7			210.7	211.7	212.7	213.7	214.6	215.6	216.6	217.6	218.6	219.6	220.6	221.6	222.6	223.5	224.5	225.5	226.5	227.5	228.5	229.5	430.5	231.5	232.4	233.4	234.4	235.4	430-4	237:4	238.4	239.4	240.4	241.3	244.5	243.3	244-3	245.3	247.2		430
	201	NAP-SH	Sec. of	4		2062		080	60	IO		1.0		13	14	12	917	17	180	61	20	122	22	23	24	25	226	27	500	29	3	231	32	33	34	35	236	37	30		위	241	4.2	43	4 ;	4	240	47	40	740	北	
SEG 1	-	22.3	22.5	22.6	22.7	The same of	~	23.2	23.3	23.5	95.56	00	43.0	23.9	24.0	24.2	24.3	24.5	24.6	24.8	24-9	25.1	25.2	25.4	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.5	26-7	26.8	27.0	27.1	27-3	27.4	27.0	27.7	27.9	900	20.5	20.3	20.5	7000	28.7	28.9	29.00	20.0	3:	True
Lat	46.4	150.3	151.3	52.3	153.3	54.3	55-3	156.3	47.1	200	200	20092	***	101.2	102.2	163.2	164.2	165.2	166.2	167.2	1.89)	1.691	1,04	171.1	172.1	173.F	174.1	175.1	176.1	177.1		0.641	180.0	181.0	182.0	183.0	184.0	185.0	186.0	180.9	1823	188.9	6-681	6-061	6-161	77.7	193-9	194-9	195.0	107.8	1	737
핅	ISI	52 I		4	55 1	561		581			147	- MANUE	one of	03		65	1993	67	68	69	70	141	72	73	74	7.5	176	77	78	79	80	181	83	83	*	Sel.	186	87	× 0	69	위	161	92	93	4	3	196	97	200	99	316	Tare!
deb	No.	15.0	1.5.1	I5-3	15:4	15.51	15.7	15.8	0.91	1.91	5.200a	14.4	7 7	10.01	10.7	16.9	17.0	17.2	17.3	17.5	17.6	17.71	17.9	18.0	18.2	18.3	18.5	18.6	18.8	r8.9	1.61	19.2	-	-	200	19.8	19.9	20.1	20.2	20.4	20.5	20.7	20.0	21.0	21.1	21:3	21.4	21.6	21.7	21.0		Lat
Ti ti	6-66	100.9	6.101	103.9	103.9	104.8	05.8	8.901	8.40	108.8	T00.8	0	000	6.111	112.8	113.7	14.7	115.7	116.7	17.7	118.7	119.7	120.7	121.7	122.7	123.6	124.6	124.6	126.6	127.6	128.6	129.6	130.6	131.6	132.5	133.5	134.5	135.5	136.5	137.5	138.5	139.5	140.5	141.4	142.4	1	144.4	145.4	140.4	47.4	140.4	vep.
힐	10	02 1	parq	04 1	띩	190	07 1	80	60	IOI		-		13	14		91	171	18	191		121	22	23	24	2.5	126	27	78	29	30	131		33	34	35	136	37	38	39	위	141	42	43	4:	4	146	47	40	47	4	
	19.5 I	9.40	8.40	6-40	%.I	18.2	98.4	28.5	9.80	8.80	0.80		7.60	2.60	4-60	5.60	1.60	8.00	10.01	IO,I	10.3	10.4	10.6	10.7	10.8	11.0	E	II.3	11.4	31.6	11.7	11.9	13.0	12.2	12.3	12.5	12.6	17.0	12.9	13.0	133	I3-3	13.5	13.0	13.8	13.9	14.1	14.2	14.4	14.5	1	LIBE
ig	10.4	5 I.4	52.4	53-4	<u>54.4</u> 0	55.4	56.4	57.4	48.4	60.3	3	6 2 3	6	02.3	63-3	64.3	65.3	66.3	67.3	68.2	69.2	10.2	71.2	72.2	72.2	74.2	75.2	76.2	17.1	78.I	79.I	80.1	81.1	82.1	83.1	84.1	85.1	86.1	87.0	88.0	89.0	90.0	91.0	92.0	93.0	잃	95.0	656	6006	97.9		Dep
	31	52	53	54	5.5	56	57	58	59	9	13	44	37	03	04	ञ	99	67	89	69	70	11	72	73	74	7.5	26	77	78	79	80	81	82	83	84	100	86	87	80 6	68	8	16	92	93	94	3	96	97	96	35	非	3
Dep	1.00	00.3	60.4	9.00	00.7	6.00	0.10	01.2	01.3	01.5	19	0	010	6.10	02.1	02.2	02.3	02.5	02.0	02.8	0.10	1:0	01.2	01.4	01.5	03.7	02.00	0.40	04.1	04.3	04.4	04.5	04.7	04.8	050	3	05.3	05.4	05.0	05.1	3	0.90	06.2	00.3	00.5	9	2.90	6.90	07.1	07:20	3	TORK
Lat	0.10	07.0	03.0	040	04.0	6.50	6-90	0.40	080	0000	15		6-11	12.9	13.8	14.8	15.8	8.9I	17.8	18.8	8.01	20.8	21.8	22.7	22.7	24.7	25:2	26.7	27.7	28.7	29.7	30.7	31.7	32.6	33.6	34.0	35.6	36.6	37.6	38.0	30	40.0	41.5	42.5	43.5	4	45.8	46.5	47.5	40.5		DEP
Did	-	77	. 3	4	5	9	1	-00	0	10		::	17	13	14	IS	91	17	18	IO	20	12	22	2.2	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	위	41	42	43	4	4	46	47	40	4	*	

for 74 Points.

																											2546	300									1	200						400						0.00			-
Dep	1	49.0	49.2	49.4	0.64	49.0	20.0	50.1	50.3	50.5	1000	1	50.0	51.1	51.3	51.5	51.7	C.T.O	52.1	50.7	2	2.00	7.7.	52.9	53.1	53.3	53.5	53.7	53.9	54.0	54.2	54-4	54.6	54.8	55.0	55.4	55.4	3	55.6	50.0	26.4	6.6	66.8	67.0	57.2	\$7.4	57.6	57.8	58.0	58.1	58.3	58.5	1
Lat	K	1.04	1.4.4	148.I	49.1	200-	121.1	252.0	253.0	254.0	255.0	1	43000	72009	257.9	258.9	259.9	260.0	261.8	262.8	8 6 9 8	000	0	205.0	2000-7	207.7	268.7	269.7	270.7	271.6	272.6	273.6	274.6	275.0	270.5	277.5	278-5	279.5	2.00.5	201-5	282.4	284.4	285.4	286.4	287.1	288.3	289.3	290.3	291.3	292.2	293.2	294.2	dor I
Did		51	52	53	54	53	120	57	58	59	99	14			-		65	266	69	289	3		थ	271	72	73	74	7.5	276	77	78	79	8	281	82	83	84	न	280	000	Ro	00	201	17.	02	0.4	9.5	206	97	86	66	300	
Dep 1	13	39.5	39.4	39.0		0.04	40.3		40.0	40.8	4I.0	1:	****	41.4	41.6	41.8	43.0	42.I	42.3	42.6	12.3	100	77	43.1	43.3	43.5	43.7	43.9	44.I	44.3	44.5	44-7	44.9	45.I	45-3	45.5	45-7	43.7	40.0	40.2	9.91	46.8	47.0	.47.2	47.4	47.6	47.8	48.0	48.0	48.4	48.0	48.0	1
Lat	I	1.26°	1.06	1.66	1.00	01:0	202.0	203-0	04.0	205.0	205.0	1900	6.00	6-102	208.9	209.9	210.8	211.8	8 110	8.11.6	0		1757	210.7	217-7	218.7	219.7	320.6	221.6	232.6	223.6	224.6	325.6	226.5	227.5	228.5	229.5	2,30.5	231.4	232.4	2.24.4	235.4	2.36.2	424.2	2.38.3	230.3	240-3	241.2	242-2	243-2	244.2	245.2	don't
Dift	Ī	10/	70	03	40		-			00		-	1	12	13	14	IS	216	Ī	181	1 5		श	ZZI	22	23	34	25	226	27	28	29	3	23I	32	33	34	न	230	37	300	200	12.4	44	1 7	44	45	246	47	48	49	250	
Dep [I	50.6	29.7	50.6	3000	30.2	30.4	30.0	30.8	31.0	31.2	1:	34	31.0	31.8	34.0	32.2	32.4	22.56	22.8	22.0	900	29.7	33.4	33.0	33.8	34.0	34.1	34.3	34.5	34.7	34.9	35.1	35.3	35.5	35-7	35-9	30:1	30.3	30.5	36.0	27.1	27.2	37.5	27.7	17.0	38.0	18.2	38.4	38.6	38.8	39.0	Trac
Lat	1	40.I	49.1	50.0	24.0	52.0	53.0	24.0	54.9	55.9	6.95		20.4	50.0	159.8	160.8	161.8	162.8	162.8	164.7	144	7,7	7-00	107.7	108.7	1.691	170.6	171.6	172.6	173.6	174.6	175.5	176.5	177.5	178.5	179.5	E80.4	101.4	182.4	163.4	104-4	186.2	187.2	188.7	180.2	100.2	191.2	102.2	193.2	194.2	195.2	196.1	Dep
Dir	Ī	.51	52	53	54	3	196	57	561	591	9	1200			Leg. SE			1991		ALMERICAN CO.				17.	72	73	74	7.5	176	77	78	79	8	181	87	× ×	40	ी	186	000	0 00	0	12	100	9 2	9.0	90	106	- 07	98	66	200	
Dep 1	Ī	19.7	6-61	20.1	50.0	20.5	20.7	20.0	21.1	2.1.3	21.5	11	6000	21.9	22.0	2.2.2	22.4	22.6	00	22.0	000		4.4	23.0	23.8	24.0	24-2	24-4	24.6	24.8	25.0	25.2	25.4	23.6	23.8	26.0	26.I	20.3	20.5	20.7	60.0	27.2	97.2	01.0	27.0	28.1	28.2	28.5	28.7	28.9	29.1	29.3	Trat
Lat	1	1-66	0.00	01.0	0.40	03.0	04.0	104.9	6-501	6.90	07.0	100	6.00	2.601	110.8	8.11	8.711	8.21					1.7.7	118.7	0.611	07061	121.6	122.6	128.6	124.5	125.5	126.5	127.5	128.5	129.5	130.4	131.4	132.4	133.4	134-4	185.3	1000	108.2	200	140.2	141.2	142.2	141.2	144.2	145.1	146.1	14:	neb
TUIC	l	0	20	03	*	a Mili	oghallis. Selejisti	es.EX	and a	60	ro		I	7.5	13	141	15	913	ALC: N	18	1 2	7	MIGH. IN	-	77	23	24	25	126	27	_	29	Alcohol	District of the last	Sec. 25.534	3	34	35	130	37	000	30			1 2	4	4.5	146	47	48	49	Si	
Depi	1	0.0	6	10.3	3	2	10.01	1.1.1	II.3	11.5	11.7	1		17.1	12.3	12.5	12.7	12.0	TO.T	T 2.2	0 6	0.0.	7-8-7	13-0	14-0	14.2	14-4	14.6	14.8	IS.O	15.2	15.4	15.6	15.8	16.0	16.2	10.4	10.0	10.8	17.0	7./-	10.6	22.2	18.0	18.1	18.2	18.5	18.7	18.0	1.61		19.5	Tat
Lat	18	0 0	0	200	300	25	4.9	2.9	6.0	1.9	80	O C	0	0.0	61.8	62.8	63.7	64.7	66.7	66.4	64.4	7 8 9		0.60	70.0	71.6	72.0	73.6	74.5	75.5	76.5	77.5	78.5	79.4	80.4	81.4	82.4	63.4	84.3	05.3	000	200	80.0	000	0.1.2	02.2	93.2	1.40	95.1	96.1	97.1	8	ng.
Dift	ľ	SI	52	53	54	55	So	57	58	59	9	13	1,	02	63	64	65	99	69	89	9	3 6	2	71	78	73	74	75	16	77	78	20	2	× 4	S C	, co	84	6	000	000	5 00	00	10	20	020	0.4	95	90	97	96	66	8	
Depl	ľ	0.0	00.4	0.0	0 0	01	1.2	21.4	01.0	8.IC	0.20	10	1	5.70	24.5	7.20	6.20	23.1	32.2	30.8	20.00	000	78.	04.1	04.3	04.5	04.7	04.9	05.I	05.3	5-50	05-7	6.50	0.90	2.00	4.00	0.00	000	07.0	2.40	49.20	07.8	80	80	4.80	9.80	8.80	00.00	00.5	09.4	9.60	हैं।	
Lat	Ï	0.1	2.0	5.0	3.9	4.95	5.0	6.00	07.8	08.80	00.810	100	000	II.8	12.7	13.7	14.7	6.7	1	1.1	2	7	3	0.02	0.I.	23.6	23.5	24.5	25.5	26.5	27-5	28.4	29.4	30.4	31.4	32-4	33.3	34:3	35.3	30.3	37.0	20.2	40.3	41.0	42.2	19.2	1.0	15.1	46.I	47.5	48.1	49.0	dan
Fail D	T	010	2	8	*	5	9	70	9	06	IO	1	-	12	I3 1	141	ISI	191	1	8	9		3	2.1	22	23	24	25	26	27	28	29	e e	31	32	33	46	3	30	37	000	40	1		. 4	4	45	94	4.7	48	49	श्र	

awiful to not

62 Difference of Latitude and Departure for 14 Points.

																			10.						240			5 63											-		4,66						1116						
Dep	6T.0	47.2	4	6.19	62.0	6.69		2.09	1.70	03.0	63:2	62.4	6.2.7	7.00	, ,	,	104:4	04.0	64.6	65.1	65.4	65.6	650	66.1	66.1	66.6	66.8	67.1	***	24.5	8	0 0		200.00	000	60.0	69.3	60.0	69.7	70.0	70.2	70.5	70.7	71.0	71.2	71.4	71.7	71.9	72.2	73.4	72.7		100
Lat	142.5		I	7.97	7.4.7	8		0 0	2000	221.3	152.2	162.2	1 7 7 7		35	200	17.75	158.0	250.0	2,000	6.00%	61.9	262.9	263.8	264.8	264.8	8.997	267.7	168.7	260.7	20.6	277.6	7	272.6	274.5	275.5	276.5	277.4	278.4	279.4	280.3	281.3	282.3	283.2	284.2	282.2	286.2	187.I	288.I	189.1	290.0	24:2	125
Diff	200		200	2,	2 2 2	7		20,	50	59	9	261	6.9		3	4 4	नं	200	67	80	60	70	271	72	73	74	7.5	1942	1	18	104	20		100	80.0	. 8	85	286	87	88	89	96	291	92	93	94	95	362	97	96		300	171111
Dep [8.8	107	40.7	40.6	40.8			2 1	30.5	50.0	\$1.0	1	61.0	200	3	52.0	27.7	52.5	52.7	53.0	53.2	53.5	53.7	\$3.0	54.2	64.4	54.7	64.0	6 6 0	33.2	23.4	200	25.4.	26.4	6.6	\$6.0	57.1	\$7.3	\$7.6	57.8	58.1	58.3	58.6	58.8	59.0	59.3	59.5	\$9.8	9000	60.3	00.5	100.7	-
Lat	0.00	0.00	000	02.0	108.0	700	9000	2 2	0 1	102-7	203.7	204.7	4000	2,40	2 4	207.0	2000	200.5	210.5	211.5	212.4	213.4	214.4	215.3	216.3	217.2	218:3	210.2	2000	27.7.2	222.1	1.00.0		225.0	226.0	227.0	228.0	228.0	229.9	230.9	231.8	232.8	433.8	34.7	235.7	136.7	237.7	238.6	239.6	240.0	241.5		400
3100	0	3	3 6	NORTH THE	464	200	- Date of	200192			IO	2116	122		?;	1;		310	17			20	221	22	2.3	24	2.5	226	2.7	28	207	30	भें	222	33	34.	35	236	37	00	39	40	241	43	43	44	土	346	47	40	449		1
Dep	16.7	26.0	27.2	27.4	17.7	27.0	200	200	3004	38.0	38.9	10.I	20.4	400	34.0	34.0	40.1	40-3	40.0	40.8	41.1	41.3	41.6	41.8	42.0	42.2	42.5	42.8		43.0	40.0	43.5	13:1			44.7	45.0	45.2	45.4	45.7	45.9	46.2	46.4	46.7	46.9	47.1	47.4	47.6	47.9	48.1	48.4	100	Tory
Lat	146.8	2.64	8	40.4	40.4		0 0	0.00	23.3	154.2	155.2	Te6.2	1.69.1			259.1	1001	0.101	162.0	163.0	163.0	164.9	168.9	8.991	167.8	168.8	8.091	170.7	7 1 1	179.7	172.6	7.7.6		176.5	177.6	178.4	179.5	180.4	181.4	182.4	183.3	184.3	185.3	186.2	187.2	188.2	189.2	1,061	1.161	192.1	193.0	1	757
Diff	E	6.0		200	2	18	2	-	30	59	9	191	records.	498/25	3	and the same	-	2000			69	70	171	Service Co.	7.2	7.4	1 2	12		78	2 0	200	3	800	3 6	3	8	186	87	80	89	90	161	92	93	94	25	96I	97	96	99.	200	1
Dep	24.6	00	26.0	2.6.2	26.6	8 2 6	94	2	***	20.5	26.7	27.0	27.2		2	1.1.	47.57	79.7	28.4	28.7	28.9	29.2	29.4	29.6	20.0	10.1	30.4	30.6	000	31.1	27.2	37.6	10	37.1	22.2	32.6	32.8	33.0	33.3	33.5	33.8	34.0	34.3	34.5	34.7	35.0	35.2	35.5	35.7	36.0	30.2		Tract
Lat	08.0	08.0	0000	100.0	101.0	202.8	0	0	1	105.7	106.7	107.5	108.6	7	7	0.01		112.5	113.5	14.5	115.4	116.4	117.4	118.3	110.1	120.2	121.3	122.2	1000	174.2	12.6.7	2,40		1280	120.0	110.0	131.0	141.0	132.0	133.9	134.8	135.8	136.8	137.7	138.7	139.7	140.7	141.6	142.6	143.0	144-5	743.5	120
JIII	101		3 6	Mary	4	Jv	-	-0	-800	60	IOI		I		?	1.	MICHIGAN	911	17		161	20	121	-	-		2.5	10	Name and Address of the	2 6	2 6	and the same of th		131	32	24	35	126	37	300	39	40	14	42	43	*	45	146	47	48	49	315	-
Dep		9	12.0	1 2 1	12.4	1				14.3	14.6	2	k		2.5	15.0	15:0	10.0	16.3	16.5	16.8	17.0	17.3	17.5	17.7	18.0	18.1	2		10.7	7 5	7 6 7	3	19.7	10.7	20.4	20.7	20.0	21.1	21.4	21.6	21.9	22.1	12.4	22.6	22.8	23.1	23.3	13.6	23.8	24.1	34.5	-
Lat	0.6	2 2					2 .	2 4	500	2-1-5	\$8.2	60.2		, ,		1.70	3	04.0	0.59	0.99	60.9	6.69	68.0	8.09	20.0	71.8	90	1:	2	74.7	13.4	70.07		70.0	200	2 2	82.5	82.4	2.7	8	86.3	87.3	88.3	89.2	90.2	91.2	92.2	93.1	94.1	95.1	90.00		100
Dia	E	2	6.3	30	27	15	2	200	30	59	9	67	24	7.7	53	0 4	न	99	67	89	69	10	1	72	73	77	75	196	2:	72	2 6	200	2	0 0	2 2	3 %	8	188	8	88	89	96	16	92	93	94	9.5	96	97	86	66	8 2	1
Depl	20.2	9	20.0	01.0	01.2		2	100	4.10	07.7	02.4	22.7	0.20	1000	2	03-4		03.9	04.1	04.4	04.0	04.0	1.50	04.3	9.00	00.00	1.90	190	940	000	3 5	27.0		27.5	000	08.2	08.5	28.7	000	00.3	09.5	09.7	10.01	10.2	10.4	10.7	10.9	II.2	31.4	11.7	11.9		A.146.
Lat	10.70	9	0	200	200	100	200	000	02.0	08.7	09.7	10.7	19.11	7	7.7	13.0	1	15.5	16.5	17.5	18.4	19.4	20.4	21.3	22.1	21.1	24.3	75.5	2 4 4	27.5	28.1	100	1	300	22.0	11.0	34.0	12.50	35.0	36.9	37.8	38.8	39.8	40.7	41.7	42.7	43-2	44.6	45.0	40.0	47.5	500	Val.
Diff		100				1	,	0	0 (6	IO		13		2	1	7	91	17	18	61	20	2.1	22	23	24	25	26	1 6	18	2 2	, ,	यः	33	22	3.4	35	36	37	38	39	9	41	42	43	44	45	94	47	40	49	华	

for 64 Points.

Dep	72.8	73.1	73.4	73.7	74.0	74.2	74.5	74.8	75.I	75.4	75.7	26.0	76.3	26.6	76.9	77.1	17.4	1:01	9 0	78.6	78.0	79.2	79.5	79.8	0.0	000	000	81.2	81.5	8.1.8	2.7	200	82.0	000	83.5	83.8	84.1	84.4	04.7	05.0	200	86.8	86.1	86.4	86.7	87.0
Lat	240-3	241.2	242.I	343.1	244.0	245.0	245.9	546.9	247.9	248.8	246.8	250.7	251.7	53.	253.0	254.6	255.5	250.5	407	1000	260.3	261.3	262.2	263.2	264.I	205.1	267.0	268.0	268.9	369.9	270.8	271.8	7:12	1.0/4	275.6	276.6	277.5	278.5	279.4	280.4	282.2	282.2	284.2	185.1	186.1	287.II
Dift	152	53	53	54	5.5	250	57	200	59	8	261	62	63	4,	न	200	02	9 9	A 0	100	72	73	74	72	276	77	70	80,	281	82	83	× 0	श्र	20,00	200	89	8	162	93	93	94	302	97	98	66	100
Dep +	58.3	58.6	58.9	59.2	59.5	59.7	0.09	60.3	9.09	6.09	61.2	61.5	8.19	63.I	62.4	62.6	62.9	63.2	2000	179	64.4	64.7	65.0	65.3	65.5	65.8	66.4	66.7	67.0	67.3	67.6	67.9	7.00	4.87	0.09	69.3	9.69	6-69	70.7	70.5	71.0	11.2	71.6	71.9	72.2	72.5
Lar	192.4	193.3	194.3	195.2	196.2	1.651	1.861	1.661	200.0	201.0	6.101	202.9	203-8	204-8	205.8	200-7	207-7	CORR	210.6	311.	212.5	213.4	214.4	215.3	216.3	217.2	210.2	220.I	221.1	222.0	113.0	223-9	224.9	225.9	227.8	228.7	229-7	130.6	431.6	232-5	233-5	226.	236.4	237-3	238-3	220.2
Dia	101	03	and the latest the lat	and risk	05	CONTROL OR		80	A CONTRACTOR OF THE PARTY OF TH	위	211	12	13	11		216	17	100	40	ीः	22	23	24	25	4	27	9.6	30	231	32	33	34	क्ष	230	28	39	4	241	42	43	44	246	47	48	49	2.50
Dep	43.8	44.1	44-4	44-7	45.0	45.2	45.5	45.8	46.I	46.4	46-7	47.0	47.3	47.6	47.9	48.1	4.0	46.7	49.0	3	49.0	50.2	50.5	80.03	\$1.0	51.3	51.0	52.2	52.5	52.8	53.1	53.4	23:7	53.9	54.4	54.8	55.1	55.4	55.7	26.0	50.3	66.8	17.1	57.4	57.7	CX.S
Lat	144.5	145.5	146.4	147.4	148.3	149.3	150.2	151.2	152.2	153.I	154-1	155.0	156.0	150-9	157.9	158-9	159.6	2 4 9 4	162.7	1626	164.6	165.6	166.5	167.5	168.4	109.4	171.3	172.3	173.2	174.2	175.1	176.1		170.0	170.0	180.9	181.8	182.8	183.7	184.7	186.6		188.5	189.5	190.4	LOIL
Dift	151	52	53	54	55		57		59	-	191	62	63	64	6	166	60	8 %	3 6		172	73	74	25	176	12	9/0	800	181	82	83	× 0	50%	1001	80	89	90	161	. 92	93	94	106	97	98	66	200
Dep [1	SHOW THE	CEUSICIA!	29.9	30.2	30.5	30.7	31.0	31.3	31.6	31.9	32.2	32-5	32.8	33.I	33.4	33.6	33-9	34.2	34.5	34.0	33.4	35.7	36.0	36.3	36.5	36.8	37.4	37.7	38.0	38.3	38.6	38-9	39:2	39.4	39.7		40.6	40.0	41.2	41.5	41.8	42.7	42.6	42.9	43.2	41.5
		97.6	98.6	8-66	100.5	IOI.4	102.4	103.4	104.3	105-3	106.2	107.4	1.801	1.601	ITOTI	O'III	112.0	112.9	200	100	116.8	117.7	118.7	119.6	120.6	121.5	122.5	124.4	125.4	126.3	127.3	128.2	700	121.1	132.1	133.0	134.0	134.9	135.9	130.9	128.8	139.7	140.7	141.6	142.6	143.5
Dift	101	Riples.	03	eticoshi Sesa	05	900077000	DECEMBER 1	-		의	III		13			911	17	10	1	गः	22	23	24		126	27	90	30	131	32	33	34	न	130	200 700 700 700	39	40	I4I	42	43	44	146	47	48	49	140
Dep	14.8	15.1	15.4	15.7	16.0	16.2	16.5	16.8	17.1	17.4	17.7	18.0	18.3	18.6	20 120 120	1-61	19.4	19.7			20.0	21.2	21:5	21.8	22.0	22.3	22.0	23.2	23.5	73.8	24.I	24.4	24.7	24.9	25.5	25.8	26.1	26.4	26.7	27.0	27.3	2,18	28.1	28.4	28.7	20.C
Lat				51.7	975	53.6	54.5	5.5	2				60.3		_	3.7	04.1	1 (20.00	27.0	68.0	0	00	71.8	72.7	73.7	9.4	26.6	77.5	78.5	79.4	4.00	5.10	2,00	2 64	85.2	86.1	87.1	88.0	89.0	000	01.0	92.8	93.8	94:7	05.7
Jill	-		53	548	5.5	56	57	58	59	or the said	CONTRACTOR .	4	63	4	5	99	07	000	3 6	415	12	73	74	73	16	77	20	80		82	93	***	ાં	8 6	000	89	90	16	92	93	440	90		98	66	100
Dep I	00.3	9.0	6.00	01.2	15.5	7.10	07.0	04-3	07.0	07.0	03.2	03.5	03.8	74.I	41	04.0	6.4.0	7.00	200	19	06.4	2.90	0.40	07:3	5.40	0.00	4.80	08.7	0.60	60.60	9-60	6-60		1 0	11.0	11.3	9.11	6.11	12.2	12.5	13.1	13.3	13.6	13.9	14.2	14.5
Lat	01.0	OF-10	06-20	03.8	8:40	05.7	.7	07.70	0,	900	10.5	11.5	4.7	13.4	14.4	15.3	20.3	100	10.1	20.1	H	22.0	23.0	23.9	and the same	25.0	27.00	18.7	29.7	30.6	31.6	32.5	???	34.5	36.4	37.3	38.3	39.3	40.7	41.2	13.1	140	45.0	45.9	46.9	47.9
Diff		4			5	arachanan .	and the same	00		힑	II	12	13	14	12	10	17	9 5		117	1 27	23	24	25	70	70			31	32	33	34	3	33	385	39	40	41	4 2	43	4 4	46	47	48	40	20

for 64 Points.

dan a	84.5	84.9	85.2	85.5	85.9	86.2	9.98	86.0	0 40	7.10	87.6	84.0	100	2999	988	88.0	0	2.60	89.6	80.0	1	500	90.0	0000	100	2	91.0	616	02.3	9.20	3	73.0	93-3	93.0	94.0	94-3	94.6	0.00	04.2	200	73.0	90.0	96.3	96.7	97.0	97.3	97.7	080	08.1	08.7	0.00	99.4	99.7	100.0	1001	100.7	IOI.0	Lat
Lat	36.3	37.3	246	239.I	2000	41.0	42.0	200	0,606	44.9	44.8	4.4			15	88	883	49.5	ALCOHOL:	-	Waste .	2	253-3	2	1:		250.I	0	2.58.0	0	18	20	0	1	262.7	263.6	264.6	266.1	266.4	264.8	407	200.3	200.3	270.2	271.2	272.1	273.0	274.0	274.0	275.0	276.8	277.7	278.7	279.6	280.6	281.5	282.5	Dep
	251 2	522	53 2	542	55 2	562	572	483	,	27	00	6119		07	63 1	64		5	-		48	0 ,	60	70	200		72	73	74	7.5	276		107	70	at States	20	28I	82	83	84	à	4	280	87	88	89	90	291	92	93	94	95	296	97	86	66	300	DIA
	_		68.4	68.7	0.69	69.4 2	69.7	10.1		4.0	70-7	91.16	1	71.4	71.7	12.1		72.4	72.7	1.14	2.5	13.4	73.8	74.1	1	0	74.0	75.I	75.4	75.8	16.1	1	70.5	70.0	77.1	77.5	77.8	78.1	78.4	78.8	100	1:17	79.5	2.62	80.2	80.5	80.8	81.2	81.4	81.8	82.2	82.5	82.9	88.2	83.5	83.9	84.2	Lat
Tat-	89.2	2.06	1.16	92.I	193.0	0.46	6.46	8.30			197.7	08.7	7 00	1990	2002	20I.c		4:00	203-4	04.1	200	3.5	2000	1.10	08.1	1	0.60	210.0	210.9	211.8	8.61		413.7	2-412	0.511	216.5	217.5	218.4	2.10.4	220.3	200	C	222.2	223.I	224.7	225.0	226.0	226.9	227.8	228.8	229.7	230.7	231.6	232.5	233-5	234-4	235.4	Dep
	1 10	02 1	-	1 10	05	190	1 40	180	ORGANIA PAR	-	IOI	ATT	CORNE	121	I3 2	TAZ	ł	7	216 2	17 2	.00	-	19 2	202	100	Î	22	23	24	2.5	192		100	90	62	S	13I	32	33	200000	,	3	230	37	38	39	40	241	42	4.2	44	4.5	246	47	48	49	250	Did
	50.9 2	51.2	5 E. S	51.9	52.2	52.5 2	54.9	53.2	* 4.6	33.0	53.9	C. 1.2	7	54.0	54.9	44.2	7	2		56.2	46.6	2	50.0	57.3	67.6		57.9	58.3	58.6	58.9	100	27.0	5900	000	60.3	9009	61.0	6I.3	61.6	62.0	6.00		07.0	63.0	63.3	63-7	64.0	64.3	64.7	64.0	65.3	65.7	66.0	66.3	66.7	67.0	67.4	Lat
<u></u> 5]	42.2	43.1	44.0	45.0	6.54	6-94	47.8	8.84	Mari		\$0.0	61.6		52.5	53.5	Teach		95-	2	49.2	•	2000	1.651	1,091	61.0	7 - 7	6.10	102.9	63.8	8.49	62.7	7 7 7	0.00	0.20	108.5	169.5	170.4	171.4	172.3	177.2	T. 4. 2		175.1	176.1	177.0	177.9	178.9	179.8	180.8	181.7	182.6	183.6	184.5	185.5	186.4	187.4	188.3	Dep
뉡	SIL	52.1	53 1	541	55.1	198	57 I	×8×	1	39	100	TAN		-3		64 1			1991	67 1	707			70 1	191		72	73	74	75	18		77	70	29	2	181	82	83	84	-	a's	180	82	88	89	90	161	92	93	94	9.6	196	97	98	66	200	DIE
	34.0 1	34.4	34-7	35.0	35.4	35.7	36.0	46.4	. 4	30.7	37.0	200		37.7	38.1	28.4			39.1	1000		27.6	40.I	40.4	100		41.1	41.4	41.8	42.I	42.4	0	0.74	43.I	43.4	43.8	44.1	44.5	44.8	44.1		45:5	45.8	46.1	46.5	46.8	47.2	47.5	47.8	48.2	48.5	48.8	49.2	49.5	49.8	50.2	\$0.5	Lut
	95.1	-		6-16		8.66	7.00	01.7			03.0	O.L.		-	06.4	07.2	86V	न	2.60	10.2		Pility	-	113.0	12.0		7	15.0	16.7	17.7	28.6	OLS.	19.0	20.5	21.5	122.4	13.3	24.3	124.2	126.2	1		0.97	0.62	6-621	130.9	131.8	132.8	133.7	134.6	135.6	136.5	137.5	138.4	139.3	140-3	141.2	Dep
i	10	20	03	to	ठ	90	140	180	5	3	임	A TOTO		777	131	IA		<u> </u>	1917	171	484		161	201	133	Ï	777	#3 T	44 1	25 1	195		107	m.BR	29	30	131	32	23	44	0	4	130	37	38	39	40	171	4.2	4.3	74	4.5	146	47	84	49	ISO	Dig
	7.3	7.5	6.4	8.2	8.5	8.9	0.5	9.6		7.4	0.2	0.6	2	60	1.2	9.1		5	2.2	2.6			3.2	3.6	0.5	2.7	4.5	4.0	4.9	5.3	13	1	2.9	0.3	9.9	26.9	7.3	7.6	8.0	8.4	2 4	000	0.61	2	9.63	30.0	30.3	10.6	11.0	9.I.	3x.7	32.0	32.3	32.7	33.0	33-3	33.7	Lat
의 기	3.0 I	100	1 6-6	5.8 I	1.8	2.7	3.7 1	9		3.3	5.5 2	1.10		5.4 2	9.3 2	0.22	0	777	2.12	4.1.2	2	2	2.05	5.92	6 8 5		7.0 %	8.72	9.72	0.62	1:		2.5	3-4 2	4.4	5.3	6.32	1.27				0	0.	1.9	2.0	30	4.7	1	9.9	87.6	38.5	39.4	4.0	1.3	3.3	33-2	24.2	Dep
뵑	31 4	52 1	53 4	54 5	55 5	56 5	47 4	00		59 5	00 5	19	3 3	02 5	63 5	9 79		20	999	6716	KEK	9 3	0060	706	11.	7 - 7	7.40	736	746	1517	3,6		727	707	797	807	817	827	82.7	87.	0		99	878	888	868	906	0.1	92	03	948	9.5	96	97	86	66	100	Dia
O ep la	0.3	0.1	1.0	or.3	1.7	07.0	12.4	12.7	1	33.0	3.4	1	1.0	0.40	24.4		1	100	5.4	4.30	K A	2	199	26.7	1		4.70	27.7	7.8c	58.4	9	0.00	1.60	29.4	8-60	TO.I	10.4	8.01	LIL	11.0		911	13.1	12.5	12.8	13.1	13.5	13.8	14.1	14.4	14.8	19.2	15.5	15.8	16.2	16.5	16.8	Dat
Lat	96.00	or.oc	02.8	03.8 c	04.7	9.50	06.66	07.60	200	00.5	09.4			11.3	12.2	19.26	2		ISI	16.0		2/1	17.9	18.81	20.0		20.7	21.7	22.6	23.5	1	44.5	25.4	20.4	27.3	28.2	20.5	30.I	11.1	22.0	200	2	33-9	34.8	35.8	36.7	37.7	38.6	30.5	40.5	41.4	42.4	43.3	44.3	45.2	46.1	47.1	Dep
Dig	-	7	3	4	3	19		8	1	6	CI	1		12	LI	14		7	97	LI		9	19	20	1		77	23	34	25	12		72	20	29	2	31	32	11	3.4		4	30	37	38	39	40	7	42	4.3	4	Š	46	47	4.8	4	.50	Ď

for 64 Points.

Dep	7 40	7 40	8.90	07.2	97.6	080	98.4	98.7	1.00	00.0		6-66	100.3	1001	IOI.0	IoI.4	s.ioi	IO2.2	102.6	TO2.0	103.0		103.7	104.1	104.5	104.9	105.2	105.6	106.0	106.4	8.90I	107.2	107.6	107.9	108.3	108.7	1.601	109.5	109.8	110.2	110.6	III.0	111.4	8.111	112.1	112.5	112.9	113.3	113.7	114.0	114.4	114.0	
Lat		200	100	100	_	Diam'r.	237.5	238.4	220.3	240.2		-131		243.0	243.9	244.8	245.8	246.7	247.6		230.6		250.4	251.3	252.2	253.2	254-I	255.0	255.9	256.9	1 20	258.7	259.6	260.6	261.5	262.4	263.3	264.2	265.2		267.0	267.9		8.692		1.6		3.5	274.4		-	277.2	
Dia	2.6.		Table 100	44	THE MOST	19	57	58	03	99	13	707		63	64	65	266	67	89	9	70	1	7/7	72	73	74	7.5	276	77	78	79	80	281	82	83	84	85	286		88	89		162	92	93	94	95	296	97	98	99	300	
Dep	76.0	97.2	17.5	78.1	78.5	78.8	79.2	79.6	80.0	80.4	0 0	0.00	1.10	81.5	81.9	82.3	82.7	83.0	8 3.4	00	200	0.0	04.0	0.50	65.3	85.7	86.1	86.5	86.9	87.2	87.6	88.0	88.4	88.8	89.2	89.6	89.9	90.3	90.7	91.1	91.5	616	92.2	95.6	93.0	93.4	93.8	94.1	94.5	94-9	95.3	95.7	-
Lat	185.7	86.0	87.6	88.	189-4	190.3	191.3	192.2	193.1	104.0	13	194.9	195.9	196.8	197.7	9.861	9.661	200.5	201.4	202.1	202.2		404.4	205.1	200.0	207.0	207.9	208.8	209.7	210.7	211.6	212.5	213.4	214.4	215.3	216.2	217.1	218.0	219.0	6-617	220.8	221.7	222.7	223.6	224.5	225.4	226.4	227.3	228.2	229.1	230.E	231.0	1300
Dift	201			0.0		902							77	13	14	1.5	216	17	18	Organism		110	-	77	23	24	2.5	226		28	-	30	231		33	34	35	236	7	38	39	40	241	42	43	44	45	246	47	48	49	2.50	
Dep.	57.8	58.2	\$8.6	58.0	59-3	59.7	60.I	60.5	6009	61.2	AT A	2009	0.70	02.4	62.8	63.1	63.5	63.9	64.3	64.7	7		05.4	02.0	00.3	999	67.0	67.4	67.7	68.1	68.5	68.0	69.3	69.7	70.0	70.4	70.8	71.2	71.6	72.0	72.3	72.7	73.1	73.5	73.9	74.2	74.6	75.0	75-4	75.8	70.7	100	i
Lat	130.5	40.4	141.4	[42.3	143.2	[44.I	145.I	146.0	146.9	147.8	100	0.04	149.7	150.6	51.5	152.5	153.4	154.3	155.2	1.66.I	1.69.1		150.0	150.9	159.8	8.00	161.7	162.6	163.5	164.5	165.4	166.3	167.2	168.2	1.691	170.0	170.9	6.171	172.8	173.7	174.6	175.6	176.5	177.4	178.3	179.2	180.2	181.1	182.0	182.9	183.9	104.0	-
	IGI	52			55	156	57	58	65	9	147	7	70	63	64	65	1991					-	ACCOUNT.			74			77	78	79	03	181										161	92	93	94	25	961	97			2007	
Dep	38.7	30.0	30.4	30.8	40.2			41.3				2.4	44.9	43-2	43.6	44.0	44.4	44.8	45.2	45.5	46.0	7,4	5.04	40.7	47.1	47.5	47.8	48.2	48.6	49.0	49.4	46.8	50.1	50.5	50.9	51.3	51.7	52.0	52.4	52.8	53.2	53.6	54.0	54-3	54.7	55.1	55.5	55.9	56.3	50.0	57.0	1	
Lat	03.2	04.2	05.2	96.1	97.0	97.9	98.9	8.66	100.7	9.IOI	100	2	103.5	104.4	105.3	106.3	107.2	1.80I	0.601	100.00	110.0	100	0.11	1.7	0	0	101	+	117.3	18.3	119.2	120.1	121.0	122.0	122.9	123.8	124.7	125.7	9.921	127.5	128.4	129.4	130.3	131.2	132.I	133.0	134.0	134.9	m	130.7	137.7	130.00 Den	
100	IOI	02	03	04,	0.5	901	07	80	60	IOI	E	-	PARTIE								20	1	1	77	43	24	2.5	126	27	28	29	30	944		3	4	tr.	136	7			mirror.		42			45		COLUMN	-	49	010	
Dep	10.5	19.0	20.3	20.7	21.0	21.4	21.8	27.2	22.6	23.0	1:	•	7.5.	24.I	24.5	24.9	25.3	25.6	26.0	26.4	26.8	1	7.1	-	7.9	8.3	200000	CONTRACTOR .	9.5	Maritin B	100000	30.6	31.0	31.4	31.8	32.1	32.5	32.9	33.3	33.7	34.1	34.4	34.8	35.2	35.6	36.0	36.4	36.7	37.1	37.5	37.9	1	
Lat	47.I	18.0	40.0	40.0	50.8	51.7	52.7	53.6	54.5	55.4	14	4.4.4	6.10	58.7	29.1	20.I	0.19	61.6	52.8	53.8	54.7	13	2.5	2000	27.5	08.4	69.3	70.2	71.1	72.1	73.0	73.9	74.8	75.8	76.7	17.6	78.5	79.5	80.4	81.3		83.2	84.I	85.0	85.9		87.8	88.7	89.6	90.0	91.5		
DIR	H	77	NUMBER OF	4	55	56	57	58	59	9	, v	, ,	7 7	03	64	65	99	67	89	60	70	1;	1 .	17	73	74	15	16	77	78	19		81	85	83	4	85		87	00		8	16		93	-	-	1000	97		100	210	S. California
Dep	20.4	8.00	OI.I	2.Ic	0.10	02.3	02.7	03.1	03.4	03.8	100	4	04.0	05.0	05.4	05.7	1.90	06.5	6.90	07.3	07.7	100	000	400	0000	2.60	8.6	10.0	ro-3	10.7	II.I	11.5	11.9	12.2	12.6	13.0	13.4	13.8	14.2	14.5	14.9	15.3	15.7	16.1	16.5	16.8	17:2		0 °	10.4	10.7	北	
Lat	0.00	8.10			04.6	05.5	.5		-	-	15	_			12.9	13.9	14.8	15.7	9		V	1	+ (3	21.3	27.7	23.1	24.0	24.9	25.9	26.8	27.7	28.6	29.6	30.5	31.4	32.3	33.3	34.2	35.1	36.0	37.0	37.9	38.8	39.7	40.0	41:0	42.5	43.4	44.4	45.3	Den C	
Dift				, ₄		100	-	000	0				7			15			THE RES		_			7.7	23	4	5	26	27	78	29	30	31	32	33	34	35	36	37	38	39	9	41	42	43	44	4	46	47	40	40	北	

No.		69044							all a		1000			200				41		1					1		1	1,000			_	_	_		_	-	_			_		-	_	-
107.3	107.8	108.6	109.0	109.5	109.9	200	111.2	111.6	112.0	112.5	112.9	113.3	113.7	114.2	114.6	115.0	115.5	115.9	110.3	110.7	117.6	118.0	118.4	118.9	119.3	1.9.7	126.6	121.0	121.4	121.9	122.3	122.7	7.22.	124.0	124.5	124.9	125.3	123.7	126.1	126.6	127.4	127.8	128.3	Lat
226.9	27.00	~9	230.5	231.4	232.3	234.1	235.0	235.0	236.8	237.7	238.6	239.5	240.4	241.3	242.2	43.	244.0	245.0	245.9	240.0	248.6		. 50	20	5	53.	254.0	55.	256.7	257.6	258.5	259.4	261.3	262.1	263.0	263.9	-	30	266.6	267.6	260.4	270.3	271.2	Dep.
251	4	53	55	256	52	0	CONTRACTOR OF	100000	62				266		89	and the same of	01		72	73	1;	S. DEVEN	7		6										162	92			95	296	0.8	66	300	Did
85.9	86.4	87.2	87.7	88.1	2000	000	80.00	90.2	9006	1.16	91.5	91.9	92.4	92:8	93.2	93.0	94.1	94.5	94.9	95.4	06.2	9.90	97.1	97.5	97.9	90.3	00.2	9.66	1001	100.5	207	101.3	102.2	102.6	103.0	103.5	103.9	104.3	60 S R	105.2	105.0	106.5	106.9	Lat
181.7	82.0	184.4	185.3	86.2	187.1	1880	189.8	190.7	9.161	192.5		194.3	195.2	1.961	197.0	197.9	98.8		200.7	201.0	202.4	204.3	205.2	1.902	0-200	207.9	000	210.6	ALCOHOL: A COM	212.4	213.3	214.2	1.6.0	216.9	217.8		9.6	220-5	221.4	222.4	223.3	225.I	10	Dep
20I		200			000			-	CONTRACTOR OF THE	13 1	_	151		17 1		161							GREEN COMM	A PRINCIPAL	29		Billions	33	34	35	236	37	300	40	241	42	43	PERMITTER	45	346	4 4	49		Diff
64.6	65.0	6.5	66.3	66.7	67.6	689	68.4	8.89	69.3	69.7	70.1	70.6	71.0	71.4	71.8	72-3	72.7	73.1	73.5	74.0	74.8	× 2	大公	76.I	76.5	77.0	22	78.2	78.7	79.1	79.5	0000	0 00	81.2	81.7	82.1	82.5	83.0	83.4	83.8	84.2	85.1	85.5	Lat
100000	137.4	A STATE OF	DOSCOBIL.	41.0	41.9	42.4	9	145.5	46.4	147.3	7	149.1	2000	151.0	151.9	152.8	153.7	154.0	155.5	150.4	158.2	I 59.1	160.0	6.091	161.8	7.70	164.5	165.4	166.3	167.2	1.891	0.601	170.0	171.7	172.6	173.6	174.5	175.4	176.3	177.2	178.1	179.9	180.8	Den
		53		156 1	52	202	9	191	62	63	64	TRANSPORT OF	1991	ACCUPATION OF		-	श	H	action made	13	7.7		11	78	79	2 6	200					0 X			161	and the same	93	94	95	961	92	66	100	D: (4)
L-TERRORING PR	43.6	44.5	44.9	45.3	45.0	9.94	47.0	47.5	47.9	48.3	48.7	49.2	49.6	50.0	50.5	50-9	51.3	51.7	52.2	52.0	23.5	53.0	54.0	54-7	55.2	55.0	2 4 4	56.9	57.3	57.7	58.2	58.0	5.00	50.0	60.3	60.7	61.1	61.6	62.0	62.4	62.9	63.7	64.1	Lat
91.3	92.2	93.1	94.9	95.8	90.7	08.6	4.66	100.3	roi.2	10201	103.0	103.9	104.8	105.8	10001	107.0	108.5	109.4	IIO.3	111-2	112.0	113.0	114.8	115.7	9.911	117.5	110.7	120.2	121.I	122.0	122.9	123.8	124.7	126.5	127.4	128.4	129.3	130.2	I3I.I	132.0	132.9	134.7	135.6	Dan
IOI	000	0 0	2000		0%			III	12 1	nacifora está	erionente ex	15	1161	17.	181	161					25				29		1200000	33.3	34	35	136	37	30	40	H	42	43	44		oto estado	4 8	49	150	The factor
8.1.	2-2	13.E	13.5	13.9	4.4.	6.3	25.7	1.92	26.5	6.92	27-4	27.8	28.2	58.6	29.I	29.5	29.9	30.4	30.0	31.2	31.0	32.5	32.9	33.4	33.8	34.2	24.0	35.5	35.9	36.3	36.8	37.2	2 × c	300	38.0	39-3	39.8	40.2	40.6	41.0	41.5	42.3	42.8	CO. SERVICE
6.1 2	7.02	8.8	49-7	0.6	I.5	100		I.	6.0	7.0	7.9	8.8	1.6	9.00	3	2.4	4.1	64-2	in	0.00	700	68.7	9.69	.0.5	4	2.3	3.5	0.5	13.9	16.8	17.1	78.0	20.00	81.4	82.3	83.2	84.1	85.0	85.9	8.98	88.4	89.5	90.4	100
514	52 4			Blue B	57.	200		919	62 5	63	64 5	and the same of	66 5	BENESONS	Section Section	Ophicane	No report	71	No. of Concession,	or Street	75				79	0 3	82	833	84	<u>∞</u>	98	82	000	NO	IO	92	93	94		A STATE OF THE PARTY OF		etroste etilo		A N. O.
10020400	6.00	01.3		07.0	03.0	200	04.3	04.71	05.1	05.6	0.90	06.4	8.90	07.3	07.7	08.I	08.00	0.60	9.4	0000	10.7	13	11.5	12.0	12.4	17.	12.7	14.1	14.5	15.0	15.4	15.8	16.2	17.1	17.5	18.0	18.4	1000	19.2	H	20.1	21.0	21.4	The second second
6.00	01.8	03.6	04.5	05.4	00.3	08.1	0.60	99.9	00	11.8	12.7	13.6	14.5	15.4	16.3	17.2	1.8.1	0.61	19.9	0 F	22.6	23.5	24.4	25.3	26.2	17,7%	00	29.8	30-7	31.6		33-4	25.2	CORNE		38.0		39.8	40.7		42.5	DESCRIPTION OF THE PERSON OF T	45.2	1011
1	4	ان م	3.		~~	and the same of th			12	13				17	18					23	-	_	27					33.		5	36	37	30	40	4	42	43	44	45	46	48	49	50	Bitt

for 54 Points.

A COLORAGE

ep	8.3	8.7	9.2	2.6	7	9.0	I.I	1.0	2.0	2.5	100	2.0	- 0		4.4	2	5.3	2.8	6.3	6.7	7.2	7.7	8.2	9.8	1	9 9		3 6	2 0		200	1	1 0		200	4.3	000	- 6	6	2.5	9.9	E	9.	3.1	3.3	0.	.5	6.	4:	6.0	* 1:	=1
a la	TI t	3 II 8.	611 1	6110	2 120.	8 12		0 121.	4 12	3 12	12	12	1 5	* :	17.		5 12	5 12.	1 12	3 12	1 12	J 12) I 2	8 I 2	7 120	120	1:	130	127	101	121	3 5	120	2 2 2	123	134	12	120	136	136	136	137	137	138	138	139	139	139	140	140	41	1
Lai	22I.	222.	223.	224-	224.	225.	226.	227.	228.	229.3	230		2000			433	234.	235.	236.	237-	238.	239.0	"	240.		242	١٠٠	2.4.5	246	246	247		2 2 2			251.	252.	252	254.0	254.0	255.8	256.7	257.5	258.4	259-3	260.2	26111	262.0	262.8	203-7	264.6	Dep
Did	2,51	52	53	54	55	256	.57	0	6	9	261	63	7	3	04	10	799	67	89	69	70	271	72	72	2,0	1 1	न्	2/1	78	2 6	200				200	***	186	200	8	80	00	201	02	93	100		3002	97	98	66	300	DIE!
Dep	94-7	95.2	95.6	96.1	90.0	97.1	97.5	0.26	98.5	98.9	00.4	0000	77.7	4.00	0001	101.3	8.101	102.2	102.7	103.2	103.7	104.1	104.6	IOCI	TOFFE	To6.0	3	104.5	107.0	101	1001	1000	000	200	1109.0	110.7	11.3	, 11	TT2.T	112.6	II 3.I	113.5	114.0	14.5	115.0	115.4	15.9	116.4	116.8	117.3	17.8	Tar.
Lat	177.3		0.671	29.9	80.8	181.7	182.6	83.5	84.3	85.2	86.1	187.0	0 %	6./00	~	01	and the latest	4	.3	193.2	194.0	0	104.8		7	8	11	199.3	4 1	. (2 6	7.2	03.7	9 1	205-5	4 0	ा	4 (2 6	December 1	7 6		7	- "	215.2	H	0	6		9	220.5	Jeb I
Tura	201 I	wan ward	LOCOPSAINAN	04 I	maumoko		07 1			IOI	211		1 C		14		316 I		181	1 61		221 I	6		7	+ +	214	7 0	7 00	0 0	7	517		3 6 6	33.2	2 2 4 4	2000	4304	2000	200	402		42 2	42.4		45 2	246 21	47 21	48 2	49	2502	=
Dep	71.1	71.6	72.1	72.6	73.0	73.5	74.0	74.4	74.9	75.4	75.0	16.0	26.00	0.0/	77-3	77:7	78.2	78.7	79.2	79.6	80.1	80.6	81.0	81.5	82.0	8	000	0.4.0	03.4		8.0	04.0	05.3	05.0	2000	84.0	82.4	0.70	000	80.7	80.5	0000	c	0000	91.4	91.9	92.4	92.8	93-3	3.00		teed St
Lat	33.2	34.1	134-9	S	130.7	137.6	138.5	139.4	140.2	41.1	42.0	42.0	0	43.0	44.0	45.5	40.4	47.3	48.3	1.64	149.9	150.8	141.7	\$2.6	62.6	54.5	0 4	23.4	1000	200	200		159.0	2,44	162.9	162.2	1 191	64.0	6	166.7	67.6	168.5	169.1	70.2		72.0	72.9	73.8	74.6	-	20	deb
Toid	ISI	52 1	53 1	1000000	los	1561	1	×	59 1	0	191	60	4.0	55	04		1991	67 1	68 1	69	0	171	72	7.2		480	1	200	1000	7.5	80,7	318	101	0 0	000	**	784	2 1	~~	50			1 6	4 00	7 4	95 1	1961	97 1	98 1	CHEST PRINTED	200	500 SE
Dep	47.6	48.I	48.5	49.0	49.5	49.9	50.4	50.0	51.4	51.8	52.3	200		4.00	53.7	54.2	54.7	.55.I	55.6	56.1	56.5	57.0	57.5	000	8.8	100	70.7	29.4	20.00	200	6,00	2 - 2	7.10	7.70	62.7	4.50	1 19	1 1	66.0	2	66.0	66.4	66.0	67.4	67.8	68.3	68.8	69.3	69.7	70.2	70.7	Tat
Lat	89.I	0.06	8.06	61.7	92.0	93.5	94.4	95.3	1.96	97.0	07.0	08.8	200	7.46	5001	101.4	102.3	103.2	104.1	105.0	105.8	1	.9	108.4	7 5	+ 0	211	1.1.1) (700			5	+ (117.3	-	110	1200	101	122.6	122.5	124.4	25.2	126 1	127.0	127.9	128.8	129.7	30.5	3	32.3	Dep.
Diff	IOI	.02	DA PERSON	Constitute Constitute	CHECKER, S	901	02	80	60	OI	1	1 6		13	14	10 Table 1	POCKS.		Ornal States	-				2.2	COMMON TO SERVICE STATE OF THE PERSON NAMED IN COMMON TO SERVICE STATE OF THE PERSON NAMED STATE STATE OF THE PERSON NAMED STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE	A STATE OF THE PARTY OF	NAME OF STREET	3 0	100	2 .0	2	CONTRACTOR	-1 (7 († ¥	14	27	~oc	0	0	of Total State	42	DOM: N	44	WINGSHEDS	NEWSKIDE !	47 1	THE PARTY	6	150	
Dep	24.0	24.5	25.0	25-4	25.9	26.4	20.9	27.3	27.8	28.3	28.7	20.2	2000		3000	30.0	31.1	31.6	32.0	32.5	33.0	33.5	33.0	34.4	24.0	25.2	200	35.0	2000	0.10	27.7		3000	300	39.00	100		2 4	1	4 T.O	42.4	42.0	42.4	43.8	44.3	44.8	45.2	45-7	46.2	46.6	47.1	Tat
Lat	45.0	45.9	46.7	47.0	48.5	49.4	50.3	SI.2	52.0	52.9	53.8	54.7	4		50.4	2/3	58.2	59.I	0.09	6009	61.7	62.6	63.5	64.4	66.2	66.2	100	0.19	× × × ×	4.09	70.0		70.7	300	7.0.T	0	100	10.7	77.6	78.0	70.4	80.3	81.1	82.0	82.9	83.8	84.7	85.6	86.4	87.3	88.2	Dept
	51	52	53	54	55	50	57	50	59	9	19	62	69	33	4,0	als	9	67	9	69	70	71	72	73	74	75	भे	77	184	70	80	81	× ×	200	3 00	8	× 86	82	80	80	90,	16	02	93		9.5	96	97	98	66	001	
Dep	00.5	6.00	0I.4	6.10	02.4	02.8	03.3	03.0	04.3	04.7	05.2	05.7	2	999	24.0	1	07.5	0.80	08.5	0060	9.4	6.60	IO.4	10.8	11.3	811	12.2	12.7	I 2.2	12.7	14.1	7.1.6	IKI	1 5.5	16.0	16.5	17.0	17.4	17.9	18.4	18.8	19.3	19.8	20.3	20.7	21.2	21.7	22.I	22.6		23.6	Frank
Lat	6.00		7.0	8	4:4		7		02.0	08.8	60.4	9,01	-	PERMIT	2 0					×	7	18.6	19.4	20.3	21.2	22.I	22.0	23.00	24.7	25.6	26.5	27.3	200	10.	0.0	30.0	31.8	32.6	33.5	4-4	35-3	200	37.0	37.9	38.8	39.7	40.6	11.5	12.3	13.2	HIG	Iden
	H	CHONOS	က	4	0000	0	COMPTONION	0		입	II	-	13	14	. 1 4		10	17		61	20	2.1	22	23	24	25	26	27	700	20	30	1	22.	22	24	2 6	26	37	300	30	40	41	42	43	44	45	46.4	474	484	494	50	

for 52 Points.

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Dep	103.3	103.8	104.3	105.4	105.9	106.4	106.9	107.4	107.9	108.4	100.0	1001	IIO.O	IIO.	111.		112.	112.	II3.	113.6	114.	114.	115.	IIÇ.	116.1	116.	117.	B. SC. MAN	ALC: U	118.	S. co. Alle	and the same of th	120.		141	122				124	124	125	125	CONTRACTOR INC.	126.9	128		1
at	172.4		4-1	00	1	177.5		179.3		181.0	and distances		Commode			186.1	187.0	187.8	188.7	189.6	190.4	191.3	192.1	193.0	193.8	194.7	195.6	196.4	197.3	198.1	0.661	8-661	2000.7	201.0	202.4	203.3	205.0	205.8	206.7	207.6	208.4	209.3	210.I	211.0	211.9	2.12.6	214.	Dep
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는 I	~	+	7 1	• 10 1000		7						953E	System of		1 4	- 67			1	6.7	7.5		9.2	H	0	151.8		2	154.4	155.2	126.1	157.0	157.8	0	159.5	100.4	162.1	163.0	163.8	164.7	165.5	166.4			169.0	70.4	171.5	
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Dep	51.9	52.4	52.9	54.0	54.5	55.0	55.5	56.0	56.5	57.0	57.6	58.I	\$8.6	40.I	100	60.1	60.6	61.2	61.7	62.2	62.	63.	63.	64.2	64.8	65.3	65.	99	90	67.	67.8		13 13		6-60	70.4		.,	72.5	<u>, , , , , , , , , , , , , , , , , , , </u>	7	7	74	75			77	La
MODELLA.	9.98	67.5	80.2	90.I	6006	91.8	95.6	93.5	94.3	95.2	1.96	0.96	97.8	9.80	00.0	100.4	IOI.2	102.1	102.0	103.8	104.6	105.5	106.4	107.2	1.801	108.9	109.8	110.6	111.5	112.4	113.2	114.1	114.9	115.0		117.5	119.2	120.1	120.0	121.8	122.7	123.5	124.4	125.2	126.1	127.8	128	Dep
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Jep	6.2 1	0.7	7 00	8.3	8.8	9.3	8.6	0.3	8.0	31.4	31.9	32.4	32.9	33.4	13.0	14.4	35.0	36.5	36.0	36.5	37.0	37.5	38.0	38.6	39.1	39.6	40.1	40.6	41.1	41.6	42.I	42.7	43.2	43.7	44.2	44.7	45.7	46.3	46.8	47.3	47.8	48.3	48.8	49.3	49.9	400	51.4	Lat
Lat	3.7 2	4.0	5.5	7.2	8.0	48.9	49.7 2	20.03	51.5	52.3	8	0			19	V	58.3	50.2	10000	6009	61.8	9	63.5	3	65.2	0.99	6.99	67.8	08.0	69.5	70-3	71.2		72.9	7.3.0	74.0	76.3		78.1	78.9	79.8	80.6	81.5	82.3	83.2	84.0	-	are named &
Dift	514	524	53	53	564	57					62		4	9	99	67	89	99	70	7.1	72	73	74	75	76	77	78	20	8	81	82	8	84.0	6 3	0 0	000	89	06	16	92	1 93	94	195	96	200	00	001	Did
Depl	9.00	o.io	01.0	02.6	03.1	03.6	04.I	04.6	05.1	05.7	06.2	06.7	07.2	07.7	08.2	08.7	00.3	800	10.3	10.8	11.3	11.8	12.3	12.9	13.4	13.9	14.4	14.9	15.4	15.9	16.4	17.0	17.5	10.01	10.5	19.0	20.0	20.6	21.1	21.6	122.	7 22.0	523.1	5 23.6	3 24-	25.	9 25.	La
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Dift	I	7	es «	* "	9	7	00	6	IO	II	12	I3	14	IK	191	17	18	TO	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	3	37	3 60	4	4	42	4	4	4	4	4 ,	+ 4	. 5	ia

for 54 Points.

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Color Colo	Control Color Co	2 4	02.2		7.4	44.0	10.0	0.0	86.5		opposite the	128.0	86.6		160.6	112.2	50	271.2	177
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25.8 17.2 81 67.3 45.0 131 108.9 72.8 181 150.5 100.5 231 192.0 128.3 281 233.6 25.6 17.8 82 68.2 45.6 32 119.6 73.9 83 151.1 101.1 33 193.7 129.4 82 235.3 28.3 18.9 82 151.3 101.1 33 110.6 73.9 83 152.1 101.1 33 193.7 129.4 82 235.3 29.1 19.4 84 153.0 102.8 35 193.7 129.4 82 235.3 29.1 19.4 84 153.0 102.8 35 193.7 129.4 82 235.3 29.1 19.4 85 70.7 47.2 35 112.2 75.5 186 154.6 103.3 25 195.4 130.5 85 235.3 29.9 20.0 86 71.5 47.8 136 113.1 75.5 186 154.6 103.3 25 195.4 130.5 85 235.8 239.4 23.2 88 73.2 48.9 38 114.7 76.7 88 156.3 104.4 38 197.9 13.2 8 8 239.4 32.4 20.5 87 72.2 89 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 33.3 22.2 90 74.8 50.0 40 116.4 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.4 107.8 44 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43 118.9 79.4 93 160.4 107.8 44 202.8 135.5 94 244.4 39 18.5 20.5 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 22.2 90 77.8 51.7 87.9 160.8 100.8 31.5 50.0 135.0 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 22.2 90 77.8 18.9 79.4 107.8 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 22.2 95 75.5 103.9 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 22.2 95 75.5 103.9 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 22.2 95 75.5 103.9 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 22.2 95 75.5 103.9 94 161.3 107.8 44 202.8 135.5 94 244.4 39.1 20.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 1	25.8 17.2 81 67.3 45.0 131 108.9 72.8 181 150.5 100.5 231 192.0 128.3 28123.5 26.6 17.8 82 68.2 45.6 32 109.7 73.3 82 151.3 101.1 33 193.7 129.4 83 235.3 28.3 4.4 82.6 17.8 82 68.2 45.6 32 110.4 74.4 84 153.0 102.2 34 194.5 130.0 84 236.1 29.1 19.4 85 70.7 47.2 35 112.2 75.0 85 153.8 102.8 35 199.7 129.4 83 235.3 29.1 19.4 85 70.7 47.2 35 112.2 75.0 85 153.8 102.8 35 199.7 129.4 82 29.1 19.4 85 70.7 47.2 35 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 31.6 21.1 87 72.2 87 153.9 76.1 87 153.9 76.1 87 123.8 81 76.5 109.5 109.5 131.1 286 237.8 32.4 21.7 87 238.6 32.4 38 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 33.4 32.2 90 74.8 49.0 126.4 77.8 90 158.0 105.5 40 199.5 131.3 90 241.1 33.4 22.2 90 74.8 50.0 40 116.4 77.8 90 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.5 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.5 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.5 51.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 41.0 78.0 92 162.1 108.3 44 202.8 135.5 94 244.4 41.0 78.0 10.3 81.0 5.3 137.2 97 246.9 39.2 25.6 96 79.8 53.3 146 122.4 81.1 196 162.9 108.9 246 207.5 136.9 92 245.8 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10	30	2	80000	80	66.5	44.4		10801	72.2	80	149.6		3	191.2	127.8	80	272.8	I55.
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24.18.3 83 69.0 46.1 33 110.6 73.9 83 153.1 101.7 33 193.7 129.4 83 235.3 28.3 18.9 84 69.8 46.7 34 111.4 74.4 84 153.0 102.2 34 194.5 130.0 84 236.1 29.1 19.4 85 70.7 47.2 35 112.2 75.0 85 153.8 102.8 35 195.4 130.5 85 236.9 29.0 199.4 85 70.7 47.2 35 112.2 75.5 186 154.6 103.3 256 196.2 131.1 286 237.8 30.8 20.6 87 72.3 48.3 37 113.9 76.1 87 155.5 103.9 37 197.0 131.1 286 237.8 30.8 20.6 87 72.3 48.9 38 114.7 76.7 88 156.3 104.4 38 197.9 132.2 88 239.4 33.3 22.2 90 74.8 50.0 40 116.4 77.8 90 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.8 91.7 57.5 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.0 33.3 22.2 90 77.3 51.7 43.1 18.9 79.4 93 160.4 107.8 43 202.0 135.0 93 243.6 35.8 23.9 93 77.3 51.7 43.1 18.9 78.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 70.0 52.8 45 120.5 80.5 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 70.0 52.8 45 120.5 80.5 94 161.3 100.8 3.1 100.0 83.1 55.0 150 124.7 80.0 105.4 110.5 49 20.7 0 138.3 99 248.5 44.4 48 123.0 82.2 81.7 97 165.3 111.1 250 20.7 8138.9 300 244.7 74.0 72.7 81.0 83.1 55.0 150 124.7 83.3 20.0 165.3 111.1 250 20.7 8138.9 300 249.4 110.0 10.0 83.1 55.0 150 124.7 81.3 111.1 250 20.7 8138.9 300 249.4 110.0 10.0 10.0 10.0 10.0 10.0 10.0 1	28.3 18.9 84 69.8 46.7 34 III.4 744 84 153.0 102.2 34 194.5 130.0 84 236.1 29.1 19.4 85 70.7 47.2 35 III.4 744 84 153.0 102.2 34 194.5 130.0 84 236.1 29.1 19.4 85 70.7 47.2 35 III.2 75.5 186 154.6 103.3 236 196.2 III.1 286 23.7 83.0 20.0 86 71.5 47.8 136 III.2 75.5 103.9 37 197.0 III.1 286 23.7 83.6 20.0 86 71.5 47.8 136 III.2 76.1 87 155.5 103.9 37 197.0 III.1 286 23.7 83.3 23.4 21.7 89 74.0 49.4 39 III.5 76.1 88 156.3 104.4 38 197.0 III.1 286 23.7 89 24.0 33.3 23.2 23.2 90 74.8 93 III.4 76.7 88 156.3 104.4 38 197.0 III.1 28.8 19.8 75.8 23.9 93 77.3 51.7 42 118.1 72.3 78.3 191 158.8 106.1 241 200.4 III.3 90 244.1 37.8 23.9 93 77.3 51.7 4 21 III.2 78.9 92 159.0 106.4 77.8 8 160.4 107.3 43 20.0 III.2 20.0 I	32	7	17.8		00.3	45.0		10001	73.3	5000	151.3	IOI.I	32	192.9	128.9	82	234-4	150.
29.1 19.4 85 70.7 47.2 35 112.2 75.0 85 153.0 102.2 34 194.5 130.0 84 236.1 29.1 19.4 85 70.7 47.2 35 112.2 75.0 85 153.8 102.8 35 195.4 130.5 85 236.9 30.8 20.6 86 715.5 47.8 136 113.1 75.5 186 154.6 103.3 236 196.2 131.1 286 237.8 30.8 20.6 87 72.3 48.3 37 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 31.6 21.1 88 73.2 48.9 37 113.9 76.1 88 156.3 104.4 38 197.9 132.2 88 239.4 32.2 2.2 90 74.8 50.0 40.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.8 33.3 22.2 90 77.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 245.8 35.8 23.9 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 245.8 35.8 23.9 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 245.8 35.8 23.9 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 245.8 35.8 23.0 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 245.8 35.8 23.0 93 77.3 51.7 42 118.1 72.2 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 33.0 20.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 245.9 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.0 44.5 136.7 296 246.1 39.9 20.7 138.3 99 248.5 47.7 40.7 27.2 198 81.5 51.0 10.1 10.1 10.1 10.1 10.1 10.1 1	29.1 19.4 84 69.8 46.7 34 117.4 74.4 84 153.0 102.2 34 194.5 130.0 84 236.1 29.1 19.4 85 70.7 47.2 35 112.2 75.0 85 153.8 102.8 35 195.4 130.5 85 236.9 30.8 20.0 86 715.5 47.8 136 113.1 75.5 186 154.6 103.3 236 196.2 131.1 286 237.8 30.8 20.6 87 72.3 48.3 37 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 31.6 21.1 88 73.2 48.9 38 113.0 76.7 88 156.3 104.4 38 197.9 132.2 88 239.4 32.4 21.7 89 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 33.3 22.2 90 74.8 50.0 40 116.4 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.5 51.2 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.5 51.2 42 118.1 78.9 92 159.6 106.7 42 201.2 134.9 92 244.4 33.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 33.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 33.6 24.4 94 72.5 51.1 45 122.2 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 24.5 51.0 97 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 205.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 124.7 82.8 89 10.6 51 11.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep	33	2	18.3		0.69	46.I		110.6	73.9	200	I52.I	IOI.7	33	193.7	120.4	83		157.
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29.9 20.0 86 71.5 47.8 136 1311 75.5 186 154.6 103.3 236 196.2 131.1 286 237.8 30.8 20.6 87 72.3 48.3 37 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 33.2 48.9 38 114.7 76.7 88 156.3 104.4 38 197.9 132.2 88 239.4 33.2 22.2 90 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.8 23.3 92.76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43.1 89.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 36.2 44 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.8 100.8 3.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 10.1 10.1 10.1 10.1 10.1 10.1 10.1 10	29.9 20.0 86 71.5 47.8 136 1311 75.5 186 154.6 103.3 236 196.2 131.1 286 237.8 30.8 20.6 87 72.3 48.3 37 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 33.2 48.9 38 114.7 76.7 88 156.3 104.4 38 197.9 132.2 88 239.4 33.2 22.2 90 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92.76.5 51.1 42 1181 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43.1 89.9 79.9 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43.1 89.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43.1 89.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 22.5 6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 165.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 55.0 49 123.9 82.8 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 44.4 72.7 138.3 99 248.5 72.7 130.8 22.5 120.8 22.8 135.0 106.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff	5				10 1						0					1000	3	0
29.9 20.0 86 77.5 47.8 I 36 II3.1 75.5 I 86 I 54.6 I 03.3 236 I 96.2 I 31.1 286 237.8 30.8 20.6 87 72.3 48.3 37 II3.9 76.1 87 155.5 I 03.9 37 I 97.0 I 31.7 87 238.6 33.8 230.8 20.6 87 72.3 48.9 38 I 14.7 76.7 88 I 56.3 I 04.4 38 I 97.0 I 31.2 88 239.4 32.4 21.7 89 74.0 49.4 39 I 15.6 77.2 89 I 57.1 I 05.0 39 I 98.7 I 32.8 89 240.3 34.1 22.8 91 75.7 50.6 I 41 I I 7.2 78.3 I 91 I 58.8 I 06.1 241 200.4 I 33.9 291 241.9 34.9 23.3 92 76.5 5 I 1 42 I I 81.7 2 78.3 I 91 I 58.8 I 06.1 241 200.4 I 33.9 291 241.9 35.8 23.9 93 77.3 5 I 7 43.1 I 89.9 92 I 59.6 I 06.7 42 201.2 I 34.4 92 242.8 35.8 23.9 93 77.3 5 I 7 43.1 I 89.9 92 I 59.6 I 06.7 42 201.2 I 34.4 92 242.8 35.8 23.9 93 77.3 5 I 7 43.1 I 89.9 80.0 94 I 61.3 I 07.8 44 20.2 8 I 35.5 94 244.4 37.4 25.0 95 79.0 52.8 45 I 20.5 80.5 95 1 105.1 I 08.9 1 108.9 47 20.5 I 35.7 296 246.1 39.9 245.6 1 20.5 5 I 20.5 5 I 20.5 80.5 95 I 105.1 I 08.9 1 105.0 83.1 55.6 I 50 I 10.8 10.8	29.9 20.0 86 71.5 47.8 136 113.1 75.5 186 154.6 103.3 236 196.2 131.1 286 237.8 30.8 20.6 87 72.3 48.3 37 113.9 76.1 87 155.5 103.9 37 197.0 131.7 87 238.6 33.8 230.8 20.6 87 72.3 48.9 38 114.7 76.7 88 156.3 104.4 38 197.0 131.2 88 239.4 32.6 21.1 88 73.2 48.9 38 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 33.3 22.2 90 74.8 50.0 40 1164. 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.1 22.8 91.75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43.1 88.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 36.2 24.4 94.78.8 152.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 70.0 52.8 45 120.5 80.5 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 70.0 52.8 45 120.5 80.5 94 162.9 108.9 108.9 246.0 135.0 95 245.1 105.0 83.1 150.0 83.1 55.6 150 124.7 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.0 82.8 81.8 99 165.4 110.5 49 207.0 138.3 99 248.5 44.6 27.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Pep Lat Diff Dep Lat Diff Pep Lat Diff Dep Lat Diff Dep Lat Diff Pep 3	-	SEL S	3		4/5	10.10			grider.	233		न	173.4	1300	65	श	100	
30-8 20-6 87 72-3 48-3 37 113-9 76-1 87 155-5 103-9 37 197-0 131-7 87 238-6 31-6 21-1 88 73-248-9 38 114-7 76-7 88 156-3 104-4 38 197-9 132-2 88 339-4 33-4 21-7 89 74-0 49-4 39 115-6 77-2 89 157-1 105-0 39 198-7 132-2 89 240-3 34-1 22-8 91 75-7 50-6 141 117-2 78-3 191 158-8 106-1 241 200-4 133-9 241-1 24-8 33-8 23-9 93 77-3 51-1 42 118-1 78-9 92 159-6 106-7 42 201-2 134-4 92 24-2 33-8 23-9 93 77-3 51-7 42 118-1 78-9 92 159-6 106-7 42 201-2 134-4 92 24-2 83-2 92 76-5 51-1 42 118-1 78-9 92 159-6 106-7 42 201-2 134-4 92 24-2 83-2 92 76-5 51-1 42-1 18-2 89-1 16-1 10-1 10-1 10-1 10-1 10-1 10-1 10	30-8 20-6 87 72-3 48-3 37 113-9 76-1 87 155-5 103-9 37 197-0 131-7 87 238-6 31-6 21-1 88 73-248-9 38 114-7 76-7 88 156-3 104-4 38 197-9 132-2 88 339-4 321-7 89 74-0 49-4 39 115-6 77-2 89 157-1 105-0 39 198-7 132-8 89 240-3 34-1 22-2 90 74-8 50-0 40 116-4 77-8 90 158-0 105-5 40 199-5 133-3 90 241-1	36		-		71.5	47.8		113.1	75.5	1000	154.6	103.3	236	196.2	131.I	286	237.	158.
31.6 21.1 88 73.2 48.9 38 114.7 76.7 88 156.3 104.4 38 197.9 132.2 88 239.4 33.4 21.7 89 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.2 90 74.8 50.0 40 116.4 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.9 23.3 92 776.5 51.1 177.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.0 35.8 23.9 93.775.5 51.1 42 118.9 79.4 93 160.4 107.8 43 201.0 135.0 93 243.8 35.8 23.9 93.775.5 51.1 43.118.9 79.4 93 160.4 107.8 43 200.0 135.0 93 243.8 36.0 24.4 478.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.6 53.9 47 122.2 80.5 95 162.9 108.9 246 204.5 136.7 296 246.1 39.1 25.0 197 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 165.4 110.5 49 207.0 138.3 99 248.5 47.7 40.7 27.2 10.8 31.5 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4	31.6 21.1 88 73.2 48.9 38 114.7 76.7 88 156.3 104.4 38 197.9 132.2 88 239.4 33.4 21.7 89 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.2 90 74.8 50.0 4 0116.4 77.8 90 158.0 105.5 40 199.5 133.9 90 241.1 34.1 22.2 90 74.8 50.0 4 116.4 77.8 90 158.0 105.5 40 199.5 133.9 90 241.1 34.4 32.3 92 776.5 51.1 42 118.1 78.9 92 159.6 106.7 43 20.0 133.9 291 241.3 36.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 20.2 133.5 94 244.3 36.2 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 20.2 133.5 94 244.4 37.4 25.0 95 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.7 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.5 49 207.0 138.3 99 248.5 40.7 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Dep Lat	17	33	20.6		72.3	48.3		113.9	76.1	GEO L	155.5	103.0	c	197.0	IZI.7	87	238.	I 50.
33.4 22.2 99 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 33.3 22.2 99 775.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 39 140.3 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43 118.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 56.4 44 77.8 51.7 43 118.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 165.3 111.1 250 207.8 138.3 399 248.5 47.7 74.0 27.8 138.3 300 249.4 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10	34.4 21.7 89 74.0 49.4 39 115.6 77.2 89 157.1 105.0 39 198.7 132.8 89 240.3 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.8 34.0 33.3 22.2 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43 118.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 200.2 137.8 99 248.5 47.7 40.7 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	000	216			72.2	18.0	-		76.9	1000	1,60		, ,	1040		00	,	140
32.4 21.7 69 74.8 49.4 39 115.0 77.2 69 157.1 105.0 39 195.7 132.8 89 240.3 33.3 22.2 90 74.8 50.0 40 116.4 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.1 22.8 91.75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92.76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93.77.3 51.7 43.1 18.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 36.2 44 94.78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 162.9 108.9 245 204.5 136.7 296 246.4 39.1 256.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 82.8 110.5 49 20.7 0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	32.4 21.7 69 74.0 49.4 39 115.0 77.2 69 157.1 105.0 39 195.7 132.8 89 240.3 33.3 22.2 90 74.8 50.0 40 1164 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.1 22.8 91.75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43.1 18.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 36.2 4.4 94.78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 162.9 108.9 246 204.5 136.7 296 246.1 39.1 25.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 82.8 99 165.4 110.5 49 20.7 0 138.3 99 248.5 47.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 89 165.4 110.5 49 20.7 0 138.3 99 248.5 47.7 40.7 27.2 99 82.3 55.0 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 30 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	30	-		3 0		1				100000	13000	104.4	36	44/6	134.4	00	4.29.4	•
33.3 22.2 90 74.8 50.0 40 116.4 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92 76.5 51.1 42 188.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.6 52.8 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.8 99 165.4 110.5 49 20.7 0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep	33.3 22.2 90 74.8 50.0 40 116.4 77.8 90 158.0 105.5 40 199.5 133.3 90 241.1 34.1 22.8 91 75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 243.6 36.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 163.9 108.9 246 204.5 136.7 296 246.1 39.1 25.0 95 79.0 52.8 45 120.2 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 89 165.4 110.5 49 207.0 138.3 99 248.5 41.6 27.8 10.0 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	39	and in the of		60	74.0	49.4		112.0	17.2	90000	157.1	105.0		198.7	132.8	68	24	100
34.1 22.8 91.75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.8 34.9 22.3.3 92.76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 133.9 291 241.8 36.2 23.9 93.77.3 51.7 43.18.9 79.4 93.160.4 107.3 43.202.0 135.0 93.243.8 36.2 24.4 94.78.152.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.6 52.8 80.5 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.8 53.3 146 121.4 81.1 196 162.9 108.3 44 203.7 136.1 95 245.3 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.2 6.7 97 80.6 53.9 47 122.2 81.7 97 165.8 110.0 48 206.2 137.8 98 247.7 40.7 27.2 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 40.7 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 10.0 12.7 8 10.0 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 10.0 12.7 8 10.0 83.1 57.6 15.0 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 10.0 12.7 8 10.0 12.2 10.0	34.1 22.8 91.75.7 50.6 141 117.2 78.3 191 158.8 106.1 241 200.4 133.9 291 241.9 34.9 22.3.9 22.5 106.1 241 200.4 133.9 291 241.8 35.8 23.9 92.76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 133.9 291 241.8 36.2 24.9 92 159.6 106.7 42 201.2 133.9 291 241.8 36.2 24.9 93 160.4 107.8 42 20.0 135.0 93 243.6 36.2 24.9 94.78.152.2 44 119.7 80.0 94 161.3 107.8 44 20.2 8 135.5 94 244.4 37.4 25.0 95 79.6 52.8 45 120.5 80.5 94 161.3 107.8 44 20.2 8 135.5 94 244.4 37.2 25.0 95 79.6 52.8 45 120.5 80.5 94 162.9 108.3 45 203.7 136.1 95 245.3 38.2 25.6 96 79.8 81.5 120.5 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 165.4 110.5 49 207.0 138.3 99 248.5 40.7 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep	40	-	22.2	90	74.8			116.4	77.8	6	158.0	105.5	40	199.5	133.3		24I.I	191,
34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.7 43 118.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.8 36.2 4.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.6 52.8 45 120.5 80.5 95 162.1 108.3 45 203.7 136.1 95 245.3 38.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 10.0 12.1 10.11 10.0 12.1 10.11 10.0 12.1 10.11 10.0 12.1 10.11 10.0 12.1 10.11 10	34.9 23.3 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 92 76.5 51.1 42 118.1 78.9 92 159.6 106.7 42 201.2 134.4 92 242.8 35.8 23.9 93 77.3 51.2 44 119.7 80.0 94 161.3 107.8 44 202.0 135.0 93 243.6 37.4 25.0 95 77.8 18.2 5.6 95 79.6 52.8 45 120.5 80.5 95 162.1 108.3 45 203.7 136.1 95 245.2 35.0 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 47.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	1	24.7	200	10	75.7		Decision 1	TI7.2	78.	15	1.88	Top	1	1000	100	1	100	14.
35.8 23.9 93 77.3 51.1 42 1100.1 70.9 92 159.0 100.7 42 201.2 134.4 92 242.0 35.8 23.9 93 77.3 51.7 43.18.9 79.4 93 160.4 107.2 43.20.2 135.0 93 243.6 36.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 20.7 0 138.3 99 248.5 47.7 40.7 27.2 99 82.3 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 100.1 Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	35.8 23.9 93 77.3 51.7 43.18.9 79.4 93 160.4 107.2 43.20.0 135.0 93 242.6 36.6 24.4 94 78.152.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 20.4.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.0 82.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 399 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	爱		-					1011	200		-200	1	- 4.7	1	+33.4	767	441.9	
35.8 23.9 93 77.3 51.7 43 IT8.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 36.2 24.4 94.78.1 52.2 44 I19.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 162.9 108.3 45 203.7 136.1 95 245.2 35.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 20.7 0 138.3 990 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	35.8 23.9 93 77.3 51.7 43 IT8.9 79.4 93 160.4 107.2 43 202.0 135.0 93 243.6 36 24.4 94.78.1 52.2 44 I19.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 162.1 108.3 45 203.7 136.1 95 244.4 37.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 98 81.5 54.4 48 123.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 89 165.4 110.5 49 207.0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	4	34.7	4			34.4		1001	1009	7	159.0	10001	4	20107	-	92	44%0	102.
36.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 37.4 25.0 95 79.0 52.8 45 120.5 80.5 95 162.1 108.3 45 203.7 136.1 95 245.2 38.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 245.2 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	36.6 24.4 94 78.1 52.2 44 119.7 80.0 94 161.3 107.8 44 202.8 135.5 94 244.4 38.2 25.0 95 79.0 52.8 45 120.5 80.5 95 162.1 108.3 45 203.7 136.1 95 245.2 38.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 117.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	43	35.6	4		1	51.7	43	118.9	79.4	6	160.4	107.2	4.3	202.0	135.	93	243.6	162.
38.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 168.9 246 204.5 136.7 296 245.3 39.9 26.7 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	38.2 25.6 95 79.0 52.8 45 120.5 80.5 95 162.1 108.3 45 203.7 136.1 95 245.2 33.6 95 79.0 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 40.9 120 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	44	36.6	a		1	52.2	44	119.7	80.0	0	161.3	107.8	44	202.8	125.5	0.4	244.4	162.
38.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 20.7 0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	38.2 25.6 96 79.8 53.3 146 121.4 81.1 196 162.9 108.9 246 204.5 136.7 296 246.1 39.9 26.7 99 80.6 53.9 47 122.2 81.7 97 163.8 199.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 40.7 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep		24.6	6	0		52.8	Ac	120.5	80.5	٠.	162.1	1080	V	202.7	1.96.1	0.0	245.0	162
36.2 25.0 90 79.0 53.3 140 121.4 01.1 190 102.9 108.9 240 204.5 130.7 290 240.1 30.1 30.1 26.1 97 80.6 53.9 47 122.2 81.7 97 165.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 20.7 0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	33.225.0 90 79.0 53.3 140 121.4 01.1 190 102.9 108.9 240 244.5 130.7 290 244.1 39.1 26.1 97 80.6 53.9 47 122.2 81.7 97 163.8 109.4 47 205.3 137.2 97 246.9 39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep		50.4		1	1		9		3	9.8			1		\sim		1	600
39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 205.2 137.8 98 247.7 40.7 27.2 99 26.7 98 81.5 55.4 48 123.0 82.2 98 164.6 110.0 48 205.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 20.7 0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Dep Lat Diff Dep 4	3	45.0	90	>0				1.10	-88			240	204.5			240.1	104	
39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	39.9 26.7 98 81.5 54.4 48 123.0 82.2 98 164.6 110.0 48 206.2 137.8 98 247.7 40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Dep Lat Diff Dep	4		13	97	0 0	53.9		7 4 4 . 4	20	6	103.0	H.	47	205.3	137.2	97	240.0	105.
40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 124.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	40.7 27.2 99 82.3 55.0 49 123.9 82.8 99 165.4 110.5 49 207.0 138.3 .99 248.5 41.6 27.8 100 83.1 55.6 150 144.7 83.3 200 166.3 111.1 250 207.8 138.9 300 249.4 Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	45	-		98		54.4		123.0	220	6	164.6	II	48	2002	137.8	98	247.7	165.
	Dep Lat Din Dep Lat D. Lat Din Dep Din	49	-	4	66	82.3	55.0	49	123.9	500	6	165.4	110.5	49	300		.99	248.5	166.
Dep Lat Din Dep Lat Dift Dep Lat Dift Dep Lat Dift Dep Lat Dift Dep	Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep Lat Diff Dep	SC		4	100	83.1	55.6	150	124-7	83.3	20000	91	III.I	250	7			240.4	166.
	for c	1	-	Lat	100	Dep	Lat	DO	Dep	Lat	No. of Contrast	ME	Lat	12	er.	1,000		Den	Lat
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S			Chicago Indiana	The Person Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, whi		White Options						VARIOTECH CONTRACTOR MICH.	2 Shrannon-					THE REAL PROPERTY.	The same of the sa

70 Difference of Latitude and Departure for 34 Points.

Lat Dep Diff Lat Dep Diff Lat 41.0 30.4 10.1 84.6 31.0 0.2 81.9 60.8 2.7 124.4 31.0 0.2 81.9 60.8 2.7 124.4 31.0 0.2 81.9 60.8 31.0 0.2 81.9 60.8 31.0 0.2 81.9 60.8 31.0 0.2 81.9 60.8 31.0 0.2 81.9 60.8 31.0 0.2 81.9 60.8 31.0 0.2 81.3 61.0 0.2 81.3 61.0 0.2 81.3 61.0 0.2 81.3 61.0 0.2 81.3 61.0 0.2 81.3 61.0 0.2 81.3 61.0 0.2 81.3 61.3 61.3 61.3 61.3 61.3 61.3 61.3 6
Lat Dep Diff Lat Dep Diff Lat 41.0 30.4 10.1 84.1 60.2 51 124.3 43.6 31.0 02, 81.9 60.8 52 124.1 43.6 31.0 02, 81.9 60.8 52 124.1 43.6 31.0 02, 81.9 60.8 52 124.1 43.6 31.0 02, 81.9 60.8 54 124.2 45.6 33.4 00 85.1 63.1 156 123.3 45.8 34.0 02 85.1 63.1 156 123.3 45.8 34.0 02 85.1 63.1 156 123.3 45.8 34.0 02 85.2 64.3 53 124.1 50.6 37.5 12 88.3 65.5 65 134.2 50.6 37.5 13 90.7 67.3 63 130.9 51.4 35.1 10 88.3 65.7 64 131.7 52.2 38.7 12 89.9 65.7 64 131.7 53.0 39.3 116 93.2 69.1 166 133.3 53.6 34.2 12 90.7 67.3 63 130.9 51.4 38.1 13 90.7 67.3 63 130.9 51.4 38.1 14 91.5 67.9 64 131.7 52.2 38.7 12 90.7 67.3 63 130.9 53.6 34.2 22 98.8 72.7 72 138.1 53.6 34.2 23 100.4 74.5 72 138.1 53.6 44.1 24 99.6 73.9 74 139.7 52.4 44.1 24 99.6 77.5 77 72 138.1 53.6 44.2 24 100.2 75.1 77 143.7 65.2 44.1 24 99.6 77.5 77 72 138.1 54.4 47.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 72 138.1 55.4 44.1 24 99.6 77.5 77 77 77 77 55.4 44.1 24 100.2 75.1 77 77 77 77 55.4 44.1 24 110.0 81.6 81.0 81.6 81.6 55.4 44.1 24 24 24 24 24 24 24 2
Lat Dep Diff Lat A1-6 30-4 101 81-1 41-6 30-4 101 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 03 81-1 41-6 31-6 31-6 31-6 31-6 31-6 31-6 31-6 3
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for 44 Points.

360											4									1																																	
Dep	159.2	159.8	160.4	161.1	161.7	162.3	163.0	103.0	164.2	164.9	165.5	166.1	166.8	167.4	168.0		100.7	109.3	170.0	170.6	171.2	171.0	172.5	172.1	177 8	-13.0	174.4	175.0	175.7	176.3	176.9	177.0	178.2	178.8	179.5	180.1	180.7	181.4	182.0	182.6	183.3	183.9	184.5	185.2	185.8	186.4	187.1	187.7	188.3	189.0	9.681	190.2	Lat
Lat	194.0	194.7	195.5	196.3	197.1	197.8	198.0	199.4	200.1	200.9	201.7	202.5	203.2	204.0	204.8		202.0	200.3	207.I	207.9	308.6	200.4	210.2	211.0	0.11.0	1	412.5	213.3	214.1	214.8	215.6	210.4	217.1	217.9	218.7	219.5	220.2	221.0	221.8	222.6	223.3	224.I	224.9	225.6	226.4	227.2	228.0	228.7	229.5	230.3	231.1	231.8	Dep
Dift	251	52	53	54	55	256	57	58	- 59	9	261	62	63	Py .	Ke	SIS	200	67	89	69	70	271	42	7.2	3 :	* ;	17	270	77	78		8	281	87	83	84	85	286	87	88	89	90	162	8	93	94	95	206	97	86	66	300	Diff
Dep 1	127.5	128.1	128.7	129.4	130.0	130.6	131.3	131.9	132.5	T33.2	133.8	I 34.4	I 3 K. I	125.7	1.96.7	000	137.0	137.0	138.2	138.9	139.5	I40.1	140.8	TATA	1000	2440	142.7	I43.3	144.0	144.6	145.2	145.9	146.5	147.1	147.8	148.4	149.0	149.7	150.3	150.9	151.6	152.2	152.8	153.5	154.1	154.7	155.4	156.0	156.6	157.3	157.9	158.5	Lat
Lat	155.3	156.1	156.9	157.6	158.4	159.2			161.5	162.3	163.1	163.8	164.6	165.4	1.991	1	100.0	107-7	168.5	169.2	170.0	170.8	171.6	172.2	147.1	1/3.1	173:9	174.0	175.4	176.2	177.0	177.7	178.5	179.3	180.1	180.8	181.6	182.4	183.1	183.9			186.2	187.0	187.8	188.6	189.3	1001	1900	9.161	192.4	193.2	Dep
Diff	201	02	03	STREET	०	300	000	80	60	위	21F	12	13	14	1.5	ीं	017	Ĭ,	18	19	20	22I	22	2.2	2.0	1 7	3)	226	27	700	29	38	231	32	33	34	35	236	37	38	39	40	241	42	43	44	45	246	47	48	49	250	Diff
Dep	8.30	96.4	97.0	97.7	98.3	6.86	99.0	100-2	100.8	101.5	102.1	102.7	103.4	TO4.0	104.6		105-3	105.9	106.5	107.2	107.8	108.4	1001	1001	1000	110.3			112.2		113.5	114.1	114.8	115.4	0.911	116.7	117.3	118.0	118.6	119.2	119.9	120.5	121.1	121.8	122.4	123.0	123.7	124.3	124.0	125.6	126.2	126.8	Lat
Lat	116.7	117.5	118.2	0.611	119.8	120.6	IZI-3	122.I	122.9	123.6	124.4	125.2	125.0	1987	127.5	70	120.3	129.1	129.8	130.6	I31.4	132.1	T22.0	122.7	100-	134.5	135.2	136.0	136.8	137.6	138.3	139.1	139.9	140.6	141.4	142.2	143.0	143.7	144.5	145.3	146.1	146.8	147.6	148.4	149.1	149.9	150.7	151.5	152.2	153.0	153.8	154.6	Dep
100	131	52	53	54	55	156	57	58	59	8	191	62	63	62	29	1			89	69	70	171	72	72	3.5	* ;	?	170	77	78	29	000	181	000	83	× 4	85	186	87	000	89	90	161	92	93	94	95	961	99	98	66	200	Diff
Dep	64.0	64.7	65.3	0.99	9.99	67.2	62.0	00.5	1.69	8.69	70.4	71.0	71.7	72.3	72.0		13.0	74.2	74.8	75.4	76.1	76.7	77.4	78.0	78.6	0 0	79:3	79-9	80.5	81.2	%I.%	82.4	83.1	83.7	84.3	85.0	85.6	86.2	86.9	87.5	88.1	88.8	89.4	000	90.7	91.3	92.0	92.6	93.2	93.9	94.5	95.1	Lat
Late	78.1	78.8	29-6	80.4	%I.I	81.9	82.7	63.5	84.2	85.0	85.8	86.6	87.3	88.1	88.0	700	2.40	90.4	91.2	92.0	92.7	93.5	04.3	05.2	0	2,40	2007	97.4	98.1	6.06	2.66	100.5	101.2	102.0	102.8	103.0	104-3	10501	105.9	106.6	107.4	108.2	109.0	109.7	110.5	111.3	112.1	112.8	113.6	114.4	115.1	115.9	Dep
Diff	IOI	02	03	40	05	901	60	ô	60	위	III	12	13	TA	71	ी	110	17	Į8	61	20	121	22	2.2	3 6	1 .	3)	126	27	700	29	ကျ	131	32	33	34	35	136	37	38	39	40	141	42	43	44	45	146	47	48	49	150	
Depl	32.3	33.0	33.6	34.2	34.0	35.5	30.1	30.0	37.4	38.0	38.7	39.3	40.0	40.6	41.2	£30e	4.		43.I	43.8	44.4	45.0	45.7	46.3	16.0	7		48.2	48.8	49.5	50.I	50.7	51.4	52.0	52.6	53.3	53.9	54.5	55.2	55.8	56.4	57.I	57.7	58.3	59.0	59.6	60.2	6.09	61.5	62.I	62.8	63-4	Lat
Lat	39.4	40.2	41.0	41.7	42.5	43.3	44.1	44.0	45.0	40.4	47.1	47.9	48.7	49.5	50.2		200	24.0	\$2.0	53.3	54.1	54.9	55.6	56.4	67.2	0		50.7	59.5	00.3	1.10	1:	03.0	63.4	04.I	04.0	05.7	66.5	67.2	68.0	68.8	9.69	70.3	71.1	6.14	72-6	73.4	74.2	75.0	75.7	16.5	77.3	Dep
Diff	125	52	53	54	55	36	57	20	59	8	19	62	63	64	9	्रि		02	80	69	70	71	7.7	7.3	3.4	1	वि	70	72	70	-	श	NI C	27	83	\$ 0	2	98	87	000	68	8	16	92	93	94	95	96	97	86	66	8	
Dep 1	9.00	01.3	6.10	02.5	03.2	03.8	04.4	05.1	05.7	80.3	0.40	9-20	08.2	0.80	00.5	13	10	0.0	-	12.0	12.7	13.3	14.0	14.6	16.2	1		10.5	17.1	17.0	10.4	श	19-7	20.3	20.0	21.0	22.2	22.8	23.5	24.I	24.7	25.4	26.0	26.6	27.3	27.9	28.5	20.5	29.8	30.4	31.1	31.7	Lat
Lat	8:00	01.5	02.3	03.1	63.9	04.0	4.50	3 00	02.0	07:7	08.5	09.3	IO.I	10.8	11.6	100	1	1.0.1	13.9	14.7	15.5	16.2	17.0	17.8	18.5	TO. 2	3 3	1.07	20.9	7.1.0	4.77	3	24.0	24.7	25.5	20.3	27.1		28.6	29.4	30.1	30.9	31.7	32.5	33.2	34.0	34.8	35.6	36.3	37.1	37.9	38.6	Dep
Diff	7	d	3	4	7	0	~~	olion-No.	_	थ	II	I.	13	14	15	15	1 1	70	1.0		20	2.1	22	23	24	25	3,0	2 5	70	0 0	7 6	न	31	32	33	40	श	30	37	-	39	위	41	42	43	4	4	46	47	48	49	2	

for 42 Points.

72 Difference of Latitude and Departure for 34 Points.

			2011							della desa												a.			8.66						GOG.	250				0000	11000			100	-	2000	1	10700	and the	79007	-	1000	p0; 5	-	Service .	00000	Way to	No.	10000	or ig	D.				00	4	150	ē4
Dep	03	108.5	169.2	£66.0	170.5	171.2		7	14.0	173.2	72.0	2	74.0	75.2	2	75.9	176.6		11.5	177.9	78.6		179.3	179.9	T80.6		181.3	181.0	18. 6		103.3	184.0	184.6	186	600	180.0	I86.7	187.3	188		188.7	189.3	190.c	190.7	IOI.		192.0	192.7	193.4	194.0	104.	TOF	2	7	190.	197.7	198.	198.	199.	200	200	20I.	15	
9 333355b				4	61		-	,	0.4	-	G		10.7	2.2 T	2.0	4.1 I	4.8 I	7	•	6.3 1	100	-		198.5		3	01	7		2	7	0	-		†	105.2	5.9	6.7	07.4			08.0	9.60	0.4		1:	6-1	7.0	3.3	4.1	14.8	9.3	, ,	0	200	7.0		19.3	20.0	20.7	21.5	27.2	Jen	
1	9200	10000	186	187	188.	188.0	100	6	61	191	TOT	226	192.	I TO 2		61/2	3 IO.		77	8 19	6 TO			61 8	60 ro	1000	7000	1 200.	200	2	3 202	4 203	5 203	100	3 1	7 20	8 20	0 20	Ro 20	1	13	82 20	3 20	4 21	5 21	12	0	7 7	88 21	89 21	90 21	0.1			93 2	94 2	95 21	96 21	97 23	4	99 2	00	19	Market
Diff	1 0	721	52	53	5.4	*	1	5,	2	3	- 60	2	5	26		0	9	×		65	266		0	9	9			127				1 7	7	1 0	7	1 7	7	8 7		1	1 28	∞ ∞	_4 ∞	×	00	18	5 40				Ser.	10						4	No.		ন	9 3	10	Manager of the last
Dep	200	13200	35.6	136.3	37.0	17.6	. 80	0 0	139.0	139-7	140.2		41.0	IAI.		144.3	143.0		143.	144.4	IACO		145.1	146-4	147.0		47.	148.	TAN		149	150	ISI.I	1:	-2-	I52.	153.1	152.8	FFA		155.	155.	156.	167.			150.	159-1	159.8			141	, ,			103.8	164.5	165.2	165.8	166	167	x67.	12	No.
Lat	280		19.61	50.4	SILI	5 I.O I	14		.3		00	×	2	156.2	5		2.00		2	59-3	60.0	100	$\overline{\mathbf{S}}$	61.5	62.2		103.0	162.7	6	-		62.0		1	4.70	108.2	689	160.6	92	ti	71.1	171.9	72.6	73.3	74.1	100	74.0	75.0	76.3	77.0	77.8	178.6	60/	5.6/1	180.0	180.7	181.5	182.2	183.0	183.7	184.4	185.2	Den	
		-14	02 14	03 15	04 IS	05 15	15	SOCIECUS.	-co-media	08 154	30 154	3	21	TI	宣誓	17 1	315		4	IS I) I y		17 1	18 1	Marie Marie	22	20 1	2 I I	MINOR I	,	23 1	24 I	2 5 I	14	DATE:	H	28 I				31 1	32 I	1 2 2	34 I	7 7 7	3	30 4	37 1	38 1	30 1	40	CONTRACTOR	references		43	44	45	245	47	48	49	2,50	10:0	į
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Sep.	LOT	101	102.1	102.7	103.4	104.			5	1001	roe.		707	TOS.	0	100.0	I00.		110.1	IIO.		i	112.	112.		6.67	114	27.71				116.8				118.	119.	120	50500		12I.	122.	122.			2000		125	126	126	127	10/11/2	NISSPAN		.m.25	130	13	131.	13	7 13	4 13	2 134	138	
Lat	0.11	- BERNOY	12.0	113-3	14.1	14.4	13	2	110.3	117.0	117.8		10.5	II0.2	2	120.0	120.7		61.5	122.2	T22.0		123.7	124.4	2 6.3	**0.**	125.9	126.7		* / "	179.7	128.9	129.6	100	130.4	131.1	131.9	122.6	000	200	134.1	134.8	135.6	136.2	127.0		137.0	138.5	139.3	140.0	140.7	TATE		744.	143.0	143.	144-7	145.	145.	146.	147.	148.	Lien	- Constant
ā.		211		53 1	54 I	1 55	13	1	57/1	58 1	50 T	-	3	reri	ORTON		63 1	Ma.		65 I	1991	W		12/200	Kol		707	71	-	1	73	74	75	1	0/1	77	78	70					83	-	00	10	100	87	000	80	00	15	100	7,6	93	4	95	961	97	98	66	200	Did	January S
Dep 10	(Sin	(a. 20	08.5	69.2	8.6	10.5	1.0	0	2	72.5	72.2		100	14.5	ARREST FORMER	75.4	6.5	, ,	?	17.2	17.0		000/	79.2	0.07	7	000	81.2	2r A	· · ·	82.0	83.3	83.0	7 7 8	7.40	85.3	85.9	86.6	87.0	3	88.0	88.6	89.3	0.00	00.7		61.3	92.0	92.7	93.4	04.0	04.7	1	200	0000	2006	97.4	98.0	98.7	99.4	1000	1001	134	Bunkane
	N N	0 '	9	•3	7.0 6	00	1,	2 0	2	0	4	ar	<u>ار</u>	.2	E	_	.7 7	à Ā	· +·	.2 7	0.2		.7	.4	2		5	19	ST SE		7	6	9	15	0		ו	9		4	0.76	00	5	7	0		form.		2.2	3.0	2.7		? :	105.2	6.5	0.7	7.4	108.2	108.9	9.6	4	H	Den	
La	"	74	7.5	26	77	77	la.	1	*	000	80.	0	0	82.	0	03	83.	8	90	85.	×	20	00	87.	8	3 6	000	80.	2	4	91.	91.	02.	15	3	94.	94	o	3 6	1	6	97	98	ŏ	100		100	101.5	IOZ.	103.0			1 1	2	3 105.9	00I	5 107.	01 9	7 10	8 109	OII 6	0 11	10	
Diff	101	101	.02	03	04	20	135	3	S	80	00		2	TIL	No.	77	II		‡	15	116		17	18	LIC	•	20	121		1	23	24	25	1	170	27	28	20	, ,	쉬	131	32	2.7	2/2	,	<u>a)</u>	130	37	38	3	3 6			+	4	4	4	14	4	4	4	H	É	9
Dep	0.10	34.7	34.9	33.6	36.3	36.9	12	200	2000	38.9	30.6		10.3	1.O	7 -	0.14	42-3		2.0	43.0	44.2		45.0	45.7	46.2		47.0	47.7	.8.	2	46.0	49.7	40.4	1:	31.0	51.7	52.4	52.0	200		54.4	55.1	55.7	26.4	27.7		57.7	58.4	59.1	50.8	600	1.3	7	5	02.4	63.1	63.8	64.	65.1	65.8	99	67.	1	ì
Lat	0 "	7.0	8.5	39-3	0.0	10.7			7.7	13.0	12.9		4-4	6.0	2	6.3	16.7		4.7.4	18.3	18.0	,	0-61	50.4			6.13	62.6		000	54.I	54.8	6.5	19.	50.3	57.0	57.8	8		2	0.09	60.7	61.5	62.2	60.00		03.7	64-4	65.2	65.0	66.7	6.11	100	000	08.0	9.69	70.4	71.1	71.0	72.6	73.3	74.1	Den	Common
Did (I	1:	513	52 3	53	54	22	17	2	57	584	60	27	00	67		02 4	63 2	, y	40,	65 4	99		07	89	y	3	70	71	313		73	74	75	140	2	77	78	70	80	31.	81	82	83	84	8	20	80	87	88	89	90	10	, ,	7	93	94	35	96	97	86	66	100	Did	Manager
Depil	13	200	51.3	02:0	52.7	32.4	100	4-5	04-7	5.4	0.90	3	00.7	27.4	1	1.90	28.7		4.60	IO.I	10.1		11.4	12.1	200	0.77	13.4	TAL	0	0.4.	15.4	1.91	8.91	1	17.5	1.81	18.8	TO. C	100	3	20.8	21.5	22.2	22.8	3.60		24.2	24.8	25.5	26.2	26.0	27.6	200	7.07	20.9	29.5	30.2	30.9	31.6	32.2	32.9	33.6	1.21	The second
Lat		00.7	2.5	12.2	53.0	32.7	1	24.4	2-50	05.90	16 90	•	27-4	12.80	300	08.9	00.00		4-01	11.1	0.17	7	17.0	13.3	1 2 1	14.1	14.8	14.6	2 47	6.01	17.0	17.8	18.4	1	19.3	20.0	20.7	2.T.	200	77.77	23.0	23.7	24.4	25.2	25.0	1	20.7	27.4	28.2	28.0	20.6	20.2	200	34.1	31.9	32.0	33.3	34.1	34.8	35.6	36.3	37.0	Den	
Dift	1	I	2	3 6	4		1	9	7	<u></u>	-	6	OI	L		12	IZ		14	IS	147		17	18	To	1	20	12		77	23	24	25	13	202	27	28	20	00	न	31	32	33	34	25	3	30	37	38	39	40	17		+	43	4	45	46	47	48	49	50	Diff	

for 44 Points.

00.7 02.1 02.8	51	26.I			-						The state of the s	-			
		0 7	30.1	IOI	71.4	71.4	ISI	2.901	106.8	64	142.I	[42.I	25 I	177.5	177.5
	3	30.00	30.0	5 6	72.8	72.8	5.2	10%2		0 0	142.5	144.0	5.4	178.0	170.2
- Puncing	54	38.2	38.2	6.0	73.5	73.5		100000	108.9		144.2	144.2	2 42	200	179.6
ä	55	38.9	38.9	05	-	74.2	55	109.6	109.6	S	144.0	144.9	55	I80.3	180.3
	56	39.6	9768	106	74-9	74.9		IIO.3	110.3	d	145-7	145.7	256		181.0
Sec.	57	40.3	4	07	-	75-7		III.0	III.0	000	146.4	146.4	.57	181.7	181.7
100000	50	41.0	41.0	8 8		70.4		111-7	7.11.	ô	147.1	147-1		102.4	162.4
1000	50	41./	42.4	5 2	17.00	17.8	200	116.1	112.1	5 5	T48.c	147.0	200	182.8	182.8
	3/3			TE		18.	T	× ;	1	1	140.2	140.5	261	184.6	184.6
		43.8	43.8	12	7 63	79.2		114.5	IIA.	12	149.0	140.0	62	184.3	185.3
	2 63	44.5	44-3	I3		79.9		118.3	IIS		150.6	150.6	63	186.0	186.0
	64	45.3	45.3	14		80.6	est.	116.	116.	4	15133	151.3	98	186.7	186.7
	65	46.0	46.0	13	81.3	Sr.3	335E.		116.7	15	152.0	152.0		187.4	187.4
	99	46.7	46.7	911		82.0	Bank!	PERMIT	117.4	216	152.7	152-7	366	1881	188.1
	67	47.4	47.4	17 10	82.7	82.7	67	110	118.1	17	153.4	153.4	67	188.8	188.8
	00	40.	0,00	0 5		03.4	1653				154.1	154-1	00 9	109.5	100.0
ALC: UNKNOWN		4 4	40.6	20		84.8				20	134.0	154.0	700	190.0	190.0
24.00	1 6	SPECIAL PROPERTY.	10.2	12.1		85.6	1 -			120	166.3	1.663	152	POT 5	FOLK
44/500	70		2 4			200			-	4.4	010	157	-1-	102.2	102.2
12227	1	, :	2 4	7 7	00	87.0	72			23.4	157.7	157.7	73		103.0
Block of	74	52.3	, "	1946		87.7		E	-	77	1,8.4	158.4	74	193.7	193.7
dulchi.	1 75	Christian Contract		gittă.		88.4		122	123.7	25	1.651	159.1	7.5	194.4	194.4
March 1	1 76	53.7	53.7	126		89.1	H	124.4	124.4	226	159.8	159.8	3276	195.2	195.2
CHARLES!	77	54.4	54.4	27	80.8	89.8	See all	125.0	1252	27	160.5	160.5	77	195.9	195.9
EUR S	8 78	55.2	55.2			1000	ST A	12	125.9	28	100000000	161.2		19	196.6
25000	200	55.9	55.9	29	91.2	91.2	29	120.0	120.0	29	101	H	200	197.3	197.3
	3)6	9,		न	66 366	O Barrie		3)3	2000	313	Com, Trest	Link		DAME TOWN	
1000 C	0 00	0 / 6	27.3	131	94.0	SHOP			128.7	431	The second	103	207	190	190-7
72855	00	8	58.7	2.00	Mark	04.0			120.0	2 2	Sept.	164	83	100.	200.I
108154	8	2 25	1.69.4	3.4		TO P		130	I 130.1	100	165.5	166	8	8	300.8
STANCES OF	7 85	9	1.09	35	95.5		85	130	8 130.8	35	H	166.2	85	4	201.5
	5 86	9.09	8.09	H	1000	10	186	131.	1000	5 236	166.9	166.6	286	202.2	202.2
1000	2	761.	5 61.5	3	96.9	6	00	.11	1132.		167.		6 87	202.9	202-9
83 23	8 6	8 62.2	2 62.2	3	97.6	9	88	H	132.	9 38	168.	3 168.	3 88	203.6	203.6
	9	6 62.0	5 62-9	39	NO.		89	described a	H	39	169	idar (6	68 0	204-3	204.3
0.00	3 9	0 63.0	6 63.6	4	0966	99.0	위	anamatalisa)	3 134	8	169:	169.	9	105.1	205.1
P. 365	6 0	I 64-	3 64-3	ITT	Annon, Inte	1.66-1	H	135	I 135-	1 241	170.	1700	4 291	205.8	205.8
S PARK	7 9	3	65.	42		100.4	Q.	35	.8 I35.	24.2	MOVE 1913	171.	1 92	7	200-5
STANS!	4	5	050		ioi		93	150	5 130.	5 43	171	171.	93	4	207-2
1000	1.1	4 00.5	00		ioi	Siois	MEGLE	2	-2 137		172	5 172.	2	4	207-9
100	7		3/2	1			3 5	801	75.7	45		173	2/3		
MED 2012	200	200	4 8 9 9	*	•	50			* 10000	4	6/1	4/3	6 × ×	60.0	2 0 0 1
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2025-3065A	H	00 70.	2	I		r roe	1 200	o ItI	4 141.	4 25	0176	8 176.	300	212,	212.
a 5.34	at Di	1	La	ā		Lat	ā	19	ep Lat	占	10	Lat	后一	1 Dep	Lat

may be wrought either by the Logarithms, or by the Scale and The method of Stating the feveral Cases in PLANE SAILING, which Compaffes.

PLANE SAILING.

CASE

When the Course and Distance are given-Say,

Is to the Distance, So is the Sine of the Course To the Departure.

and Soisthe Sine Complement of the Courfe
To the Difference of Latitude. As Radius

and So is Radius
To the Difference of Latitude, As Sine Com. of the Courfe When the Course and Difference of Latitude are given-Say, Is to the Difference of Latitude, As the Sine Com. of the Course So is the Sine of the Course

To the Departure.

When the Course and Departure are given-Say

As the Sine of the Course

Is to the Departure,
So is the Sine Com. of the Course

To the Difference of Latitude.

To the Difference of Latitude.

IĄ.

and So is the Sine of the Course To the Departure. When the Distance and Disference of Latitude are given-Say, As Radius To the Sine Com. of the Courfe. Is to Radius, So is the Difference of Latitude As the Diftance

. U

and Departure are given-Say When the Distance

To the Sine of the Course. So is the Departure As the Diftance Is to Radius,

and So is the Difference, of the Courfe To the Difference of Latitude. As Radius

S A

CA

When Difference of Latitude and Departure are given-Say,

To the Tangent of the Courfe. As the Difference of Latitude So is the Departure Is to Radius,

As the Sine of the Course

Is to the Departure,
So is Radius
To the Diffance.

The method of Working the Cases in Middle Latitude and MERCATOR'S SAILING.

ASE

When the Latitudes and Longitudes of two Places are given-Say

By Mercator's Sailing.

By Middle Latitude Sailing.

As the Meridional Diff. of Latitude So is the Difference of Longitude. To the Tangent of the Course. As the Sine Com. of the Course Is to the Proper Diff. of Latitude, Is to Radius.

So is the Sine of the Courfe To the Departure.

Is to the proper Difference of Latitude, As the Sine Com. of the Courfe To the Diffance. So is Rad

As Radius Is to the Difference of Longitude, So is the Sine Com. of Middle Latitude

So is the Departure
To the Tangent of the Course.
3. As the Sine of the Course To the Departure.
As the Difference of Latitude Is to Radius,

Is to the Departure, Te the Distance.

Ħ CASE

When the Course and Diff. of Lat. are given, to find the Dist. and Diff. of Long .- Say,

of Latitude As the Sine Com. of the Course Is to the proper Diff. of Lat So is the Sine of the Course To the Departure.

Is to the proper Diff. of Latitude, of the Course As the Sine Com.

Is to the Meridional Diff. of Latitude, As the Sine Com. of the Course So is the Sine of the Courfe . To the Distance.

To the Diff. of Longitude.

Is to the Difference of Latitude, As the Sine Com. of the Courfe As the Sine Com. of the Courle Is to the Difference of Latitude So is the Sine of the Course To the Departure.

To the Difference of Longitude. As Com. of Middle Latitude Is to the Departure, To the Distance. So is Radius

ASE III.

When the Course and Distance are given, to find the Diff. of Lat. and Long .- Say,

- Is to the Diffance,
 So is the Sine Com. of the Courle
 To the Difference of Latitude.
- Is to the Distance,
 So is the Sine of Course
 To the Departure.
 3. As Sine Com. of the Course
 Is to the Meridional Diff. of Latitude,
 So is the Sine of Course
 To the Distrence of Longitude.
- I. As Radius
 Is to the Distance,
 So is the Sine Com. of the Course
 To the Difference of Latitude.
 - 2. As Radius
 Is to the Diffance,
 So is the Sine of the Courfe
 To the Departure.
- 3. As the Sine Com. of Middle Latitude Is to the Departure, So is Radius To the Diff. of Longitude.

CASE IV.

When the Diff. of Lat. and Dep. are given, to find the Dift. and Diff. of Long .- Say,

- Is to Radius,
 So is the Departure
 To the Tangent of Courfe.
 - Is to the Departure,
 So is Radius
 To the Diffance.
- 3. As the Sine Com. of the Courfe
 Is to the Meridional Diff. of Latitude,
 So is the Sine of the Courfe
 To the Diff. of Longitude.
- As the Difference of Latitude 1s to Radius, So is the Departure To the Tangent of the Courfe. As the Sine of the Courfe.
 - 2. As the Sine of the Course Is to the Departure, So is Radius To the Diffance.
- 3. As the Sine Com. of Middle Latitude Is to the Departure, So is Radius
 To the Difference of Longitude.

Note. These are all the Cases that can happen at Sea, unless a Ship happens to sail due E. or W. in which Case, say, As the Sine Com. of the Latitude sailed in, Is to the Distance sailed, So is Radius, To the Difference of Longitude.

200 of 100

A TABLE shewing the Moon's Age to the nearest hour every day, at noon, according to her mean motion, for the 102 1780 year 1788.

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nearest hour every day, at noon, according to her mean motion, for the year 1789. A TABLE shewing the Moon's Age to the

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A TABLE shewing the Moon's Age to the nearest hour every day, at noon, according to her mean motion, for the year 1793.

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A TABLE shewing the Moon's Age to the nearest hour every day, at noon, according to her mean motion for the year 1794.

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A TABLE shewing the Moon's Age to the nearest hour every day, at noon, according to her mean motion, for the year 1795.

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A TABLE shewing the Moon's Age to the nearest hour every day, at noon, according to her mean motion, for the year 1796.

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A TABLE shewing the Moon's Age to the nearest hour every day, at noon, according to her mean motion, for the year 1797.

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To find the Moon's AGE by the foregoing TABLES.

E ACH page of the foregoing Tables shews the Moon's Age to the nearest thour every Day at Noon, according to her mean motion, for the Year with which it is marked at the top, and is divided into thirteen columns: The first of which, to the left hand, shews the Day of the Month, the other twelve the Months of the Year; so that if it were required to find the Moon's Age for any Day, suppose, for Example, on the 12th May, 1788, First, I look for that Table which has 1788 at the top of it, and then right against the 12th of the Moon's Age, on the given Day, at Noon.

To find the time of the Moon's Southing on a given day.

Multiply her age by 49, and divide the product by 60, the quotient will be the hours, and the remainder the minutes, when the fouths; that time, if lefs than 12 hours, is the time after midday, but, if greater, the excess is the time after last midnight.

Note. When her age confifts of days and hours, a proportional part of 49 must be taken for the hours, and added to the former product.

EX. I. Required the time of the Moon's | EX. II. At what time will the Moon outh on the 20th March, 1788.

South on the 30th May, 1790.

12 Moon's age. South on the 20th March, 1788.

13 M 49 117 53 60)637 Moon Souths fo h. 37 m. afternoon.

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784 36 45 Prop. parts for the 60)820 45 N. B. If, to the time of the Moon's Southing, you add the time of high-water on the day of New or Full Moon, the fum will shew the time of high-water on the given day.

The use of the following TABLE of TIMES in finding the TIME of HIGH-WATER.

ded to the time of high-water at New or Full Moon, give the times of high-water at the ages of the Moon to which they fland opposite. Thus, opposite to the Moon's age, 6 days, 18 hours, flands the time, 4 hours, 23 minutes, and, opposite to her age, 20 days, 3 hours, flands the time, 3 hours, 16 minutes, which times, added to the time of high-water at New or Full Moon, shew the days, 3 hours, therefore, having the time of high-water at any place on the day of New or Full Moon. The time of high-water at that THIS Table confilts of fix double columns: The first part of each column is titled Ages, and contains the Moon's age in days and hours, to every three hours of her age: The second part is titimes of high-water when the Moon's age is 6 days, 18 hours, and 20 tled Times, and shews the times in hours and minutes, which, adplace, on any given day, may be found by the following

R O L

will be the time of high-water at the place on the given day; but, if it should be more than 12 hours, then subtract 12 hours from it, and the remainder will be the time of high-water.

N. B. The time of high-water. Find the Moon's age, and time answering to it (as before taught) and to that time add the time of high-water at the given place, on the day of New or Full Moon, the fum, if it doth not exceed 12

N. B. The time of high water on the day of New or Full Moon, is fet opposite to the name of the place in a column, before the latitudes and longitudes of places.

EXAMPLE

At what time will it be High-Water at Aberdeen, the 15th January, 1788.

By the table of the Moon's age, for the year 1788, I find, that, on

the 15th January, the Moon is 7 days, 3 hours, old, with which age, entering the table of Times, I find the time answering to be 4 hours, 44 minutes, which, added to 0 hours, 45 minutes (the time of highwater at Aberdeen on the day of New or Full Moon) gives 5 hours, 29 minutes, for the time past noon, on the given day, when it is are adelien, office or high-water at Aberdeen.

the Sun and Moon.

E X A M P L E II.

Required the time when it will be High-Water at London, v. stb June, 1789.

By the table of the Moon's age, for the year 1789, I find, that, on the 5th June, the Moon is 12 days, 2 hours, old, the nearest age to which, in the table of Times, is 12 days, 3 hours, and against it stands 10 hours, 15 minutes, which, added to 3 hours, the time of high-water at London, at New Moon, gives 13 hours, 15 minutes, for the time past noon, on the given day, when it is high-water there, from which fubtract 12 hours, 25 minutes (the time answering to a tide, or half of a lunar day, at this time of the Moon's age) there remains o hours, 50 minutes, for the time past noon, when it is high-water there, on the given day.

EXAMPLE III.

At what time will it be High-Water at Leith, 4th November, 1792.

Having found the Moon's age (as before taught) to be 19 days, 19 hours, and the time answering to be 3 hours, 1 minute, which, added to 2 hours, 15 minutes (the time of high-water at Leith, at New Moon) gives 5 hours, 16 minutes, the time of high-water at Leith, on the evening of the given day.

difference, as the Table of Numbers frequently gives the Moon's Age will compare these examples with the methods In like manner may the time of high-water at any other place be used in the former Editions of this Book, will find a confiderable found. --- Whoever

whole days, and, confequently, the time of her fouthing, and of high-water, hours, wide of the truth.

rence being fometimes more, fometimes lefs, according as the waters are acted on, either by the fum, or difference of the attractive forces it is to be remarked, that the time of high-water does not alter 48 minutes every day, as is usually reckoned in Pilotage, the diffeof the Sun and Moon. But, the following TABLE of TIMES being ufed, at any given time of the Moon's age, will, in general, shew the time of high-water, within half an hour of the truth, if not greatly influenced by the winds.

A TABLE

The property of the state of th

the time of High-Water at any place on the day of New or Full Moon, shew the times of High-Water at that place on A TABLE of the TIMES, which, added to any other day of her age.

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every Day at Noon, under the Meridian of Greenwich, for the years 1790, 1794, and 1798, each being the fecond after leap year. A TABLE of the Sun's DECLINATION for

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Declination to every to Degrees of Longitude. A TABLE of the Variation of the Sun's

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To find the Sun's Declination by the foregoing TABLES.

for example, on the 20th of August, 1788: First I look for that Table that has 1788 at the top of it, and then right against the 20th day of the month, and under August, I find 12° 10' which shews the Sun's Le for the years that it is marked with at the top, and is divided not thirteen columns; the first of which to the left-hand, shews the day of the month, and the other twelve the months of the year, so that Declination to be 12 degrees 10 minutes north; according to the title ACH page of the foregoing Tables contains the Sun's Declination If it be required to find the Sun's Declination for any Day, as suppose

at the top of the column.

The Sun's Declination in these tables being calculated for the Meridian of Greenwich, if you should be confiderably to the eastward, or to the westward of Greenwich, it will cause some alteration in it; to correct which, the

Table of Variation of the Sun's Declination is to be used as follows:

for the day following it, and fubtract the lefs from the greater, the remainder is the daily variation. First, Look out the declination for the given day of the month, and

ing, which you may know thus; if the declination for the day following the given day be biggelt, then it is increasing; but, if it be leaft, it is decreasing. Second, Observe whether the declination be increasing or decreas-

least, it is decreasing.
Third, Look for the daily variation in the first column of the Table, and see what number stands right against it, and under the given

If the difference of longitude be eafterly, and the declination increasing, it must be subtracted from the declination found in the degrees of longitude, which number is to be used as follows.

Tables for the given day; but if the declination be decreafing, it must

If the difference of longitude be westerly, and the declination increasing, it must be added; but if the declination be decreasing, it must be subtracted; the sum in one case, and the remainder in the other, will be the Sun's Declination at noon in the longitude required. be added.

A TABLE of the Sun's RIGHT ASCENSION.

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This Table is fufficiently exact for finding when any Star comes to the Meridian, in order to find the Latitude; but, in all calculations for determining the Longitude by Celeftial Observations, the Sun's Right Aftension and Declination must be taken out of the Nautical Almanac, as they are there calculated to a greater degree of

in Time, the most	Right Decir-Afcen, nation H. M. D. M.	1 55 22 26N 2 54 40 8N	3 9 49 5N 4 24 16 4N	5 1 45 46N 5 4 8 28 S	5 13 28 25N 5 44 7 21 N	5 25 21 ON	5 14 6 8N	46,	6 36 16 25 S	7 28 5 46N 7 32 28 32N	~:	49 57 32	10 50 02 55 N	12 5 58 14N 12 44 67 8N	13 14 10 2 S	13 621 59 5	13 39 50 24 N	14 39 15 58
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A TABLE of the Fixed Stars.

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The Names of the Stars.	Bright Star of the Crown	The Scorpion's Heart, Antares ***	In the Head of Serpentarius	Bright Star in the Dragon's Head	Swan's Beak	Bright Star in the Eagle ** The Swan's Tail **	Pegafus' Mouth ** Fomelhaut - **	Pegafus' Wing, Marchab The Head of Andromeda	End of Pegafus' Wing, Algenib *

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7- 4-1-0	The Westermost of the two middle stars. The Eastermost. The Northermost, or highest Star. The Southermost, or lowest.
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The Stars marked with an Afterism are those from which the difance of the Moon is calculated in the Nautical Almanac.

The

The use of the Tables of the Sun and STARS' RIGHT ASCENSFON, in finding what time any known STAR will be upon the Meridian on any given day.

number of degrees of the Equinoctial that comes to the meridian N. B. The Right Afcention of the Sun, Moon, or Stars, is the with them, counted from the first point of Aries. If A. R.

apputing on nutrouRe an U. - Lound. to calbitrate out no 3d now and tenament bluewifthe sub-required live in Substitution

the Sun's right afcention be greateft, add 24 hours to the Star's right afcention, and then subtract the Sun's from it, the remainder will be Tables, and subtract the Sun's right ascension from the Star's; but, if Look for the right afcenfion of the Sun and Star in the preceding the time, of the Star's coming to the meridian.

When the Sun's right afcention is leaft, the Star comes to the meridian in the afternoon. but before noon when the Sun's is greateff.

E X A M P L E At what time will the gin's Spike be on the me London, Sept. 1?	24 o Spica Virginis right afcen	38 6 Sun's right afcention	z1 36 noon Iz o	So the Star Virgin's Spi to the Meridian at Londo nutes after two in the aft
EXAMPLEI. EXAMPLE E At what time will the Star Arc- turns be on the meridian of Lon- don. Dec. 1? H.M. London, Sept. 1?	Arcturus' right afcention 14 6	Sun's right afcention 15 30	Affer midnight 21 36	Morning - 9 36 to the Meridian at Londo That is, the Star Arcturus will nutes after two in the after be upon the meridian of London so minutes after nine o'clock in

H. M.

Star Vir-

To find what Star will come upon the Meridian at any given time.

THE TOTAL TO

Star's right afcention agrees with, or comes the nearest to it, and that Add the time from noon to the right afcention of the Sun, the fum will be the right afcention of the Star required to be known; with which enter the table of the Star's right afcention, and find what is the Star required.

Cond.	L CE	S	なり
T X A M P L E of the	be on the meridian of London a- ribout ten at night, January 25th?	Sun's right afcention Jan. 25. at noon - 20.31	And for 10 hours more 0.2 F

o at noon was a read of the same of the sa idian of London 20 minutes paft What Star will be upon the me-Siventime, 16th. 30 m. smitted And for 16 hours more conton EXAMPLEIL our in the morning, May 10? P. M. Morre True

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Arduna' right at To find the Latitude by Observation.

With a proper instrument take the meridian altitude, or zenith distance, of the Sun, or some known Star, to which apply the sol-

zon, 16 miles must be added for his semidiameter; but, if the upper limb is taken, 16 miles are to be subtracted: Except, when the lower limb is taken in a back observation, the 16 miles for the Sun's semidiameter must be subtracted.

II. The dip of the horizon is to be subtracted in the fore observalowing corrections.

I. If the Sun's lower limb be brought into contact with the hori-

tion, and to be added in the back observation.

III. The refraction is to be fubfracted both in the fore and back observation. These three corrections give the true altitude of the ad of Daysello esw 01 '2. Sun's centre.

Note. The corrections to be applied in taking the altitude of a Star are, Hirst, The dip to be applied as before. Secondly, The redip of the horizon forest feet elevation fraction to be fubtracted.

Theforwo corrections give the true altitude of a Star. I at the

of the object is from the point over your head, with which, and with the tables of the Sun and Stars'ideclination; the latitude of a place Having obtained the true meridian alritude of the Sun, or fome known Star, fubtract it from 90 degrees, and the remainder will be the true zenith distance, or the number of degrees, &c. the centre is found as follows.

hath fouth declination, or to the fouth, and hath north declination, the zenita distance, added to the declination, gives the latitude of the place of observation, and is of the same name with the declina-First, If the Sun or Star be to the South when observed, call the zenith distance fouth; but, if north, call it north.

Then, if the zenith distance and declination be of contrary names, that is, if the Sun or Star come to the meridian in the north, and tion, whether worth or fouth, mam s'ung act

Secondly, When the zenith distance and declination are of the the fouth, and hath fouth declination, or to the north, and hath north declination, fubtract the less from the greater, and the remainder is the latitude; and, to know whether it is north or fouth, observe same name, that is, when the Sun or Star comes to the meridian in

this general

When the declination is greater than the zenith distance, the latitude is of the fame name with the declination; but, if lefs, of a Demed contrary name.

First, When the Sun or Star is on the equator, or hath no declination, the zenith distance is the latitude of the place, and of a contrary name to the zenith distance.

Secondly, When the Sun or Star is in the zenith, the declination is the latitude, and of the fame name with the declination.

Remains the letterde in

Littude of the Sun's of the observer be- ude is required. is 18° 45' N. the	34° 10' N	34. 26	34 20	55 40 N 18 45 N	36 55 8 35 M	ide lower limb was being 40 feet above e Sun's declination,	-62° 9'S	62 25	62 181 69	27 41.8 12 47 8	14 54 N EXAMPLE
Being at fea July 29th, 1789, the meridian altitude of the Sun's ower limb was observed to be 34° 10' N. the eye of the observer being 25 feet above the level of the fea. The latitude is required. The Sun's declination for the 29th July, 1787, is 18° 45' N. the lip of the horizon for 25 feet elevation is 5 miles, the refraction for	mile, therefore, Altitude of the Sun's lower limb, Add femidiameter,	Sabtradi dip and refraction,	ic, 198-bill or of with it.	ogical to the second of the se	atitude,	October 26th, 1784, the Sun's meridian altitude lower limb was in 9. S. required the latitude: height of the eye being 40 feet above he furface of the feat 1784 is leap year, and the Sun's declination,	for 62° 9' is ; mile, therefore, Sun's apparent altitude, lower limb, Add the femidiameter,	Subtract dip and refraction,	de,	ce,	latitude in
Being at fea July 29th 29th 29th 29th 25 feet above the learn The Sun's declination ip of the horizon for 2	4 is 1 mile, therefore, mo Altitude of the Sur	iv III. Subtract dipa	di Esp. Correcte altitude,	Subtract declination,	Remains the latitude,	October 26th, 1784, 12° 9' S. required the he furface of the fea?	cfraction for 62° 9' is ‡ mile, the Sun's apparent altitude. Add the femidiameter,	Subtract dip :	Correct altitude,	Zenith distance, Subtract declination,	Remains the latitude in

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** THE PARTY

Being at fea in the year 1786, close weather prevented the meridian observation of the Sun, but, the night proving clear, the meridian altitude of the Great Dog, Sirius, was found to be 53° 35' fouth, required the latitude, the height of the eye being then 35 feet above the level of the sea?

53° 35'S	53 29	36 318	Ny or
raction,	7.	* 30 x 1 2 . 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-
Star's altitude, 53° 35'S. Subtract the dip and refraction, 6	Correct altitude, -	Zenith distance, 36 31 S Star's declination, 16 25 S	Latitude in.
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The foregoing Rules are for observing, by the Sun or Stars, when they are at their greatest altitude, or upon the meridian above the E c

veral days, and some Stars never let in that case, they may be observ-Pole; but, as in some parts of the Earth the Sun does not set for seed upon the meridian twice in the twenty-four hours, that is, once at their greatest height as before, and again when they are at their low-est, or upon the meridian below the Pole; to work which observations take the following

C. Levis Being land

Add the complement of the declination to the meridian altitude, the fum is the latitude of the fame name with the declination.

June 11th, 1784, the meridian altitude of the Sun's upper limb was observed to be 8° 20' N. below the Pole, the height of the observer's eye being then 16 sect above the furface of the sea, required the

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Sun's apparent altitude, upper limb, Subtract semidiameter, dip, and refraction,	Correct altitude, Sun's declination 23° 10', its complement is	Latitude in,
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Being at fea 4th Jan. 1786, I observed the meridian altitude of the Bright Star, Lyrae, to be 8° 33' N. below the Pole, required the latitude?

8 33'N	8 27 N 51 24 N	N 15 65
	Correct altitude, Star's declination 38° 36', its complement is	
de, refraction,	tude, nation 38°-36	
Star's altitude, Subtract the refraction,	Correct alti Star's declir	Sum is the latitude,

A TABLE of the REFRACTION of the HEAVENLY BODIES, to be fubtracted from the observed Altitude.

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Given the Declination, and two observed Altitudes of the Sun, with the Interval of Time between them, and the Latitude by Dead Reckoning, to find the true Latitude.

N. B. Thefe cautions are taken from Dr. Malkelyne's British Mariners' Guide.

Before giving precepts for the folving of this problem, it is necefary to attend to the following cautions, relating to the proper times

for making the observations.

First, That the two observations must be always taken between nine in the morning and three in the afternoon; but, the nearer they are to noon the better, provided there be a fufficient interval between

The following directions will shew what interval is proper. If both observations are in the forenoon, the interval of time between them must not be much less than half the distance of the first observation

If both observations are in the afternoon, the interval of time bevation from noon. If one observation is in the forenoon and the otween them must not be much less than the distance of the first obser-

ther in the afternoon, the interval must not exceed 44 hours.

If the Sun's meridian zenith distance be confiderably less than the latitude of the place, the observations must be taken proportionably nearer to noon.

before 9# A. M. nor the second before 10# A. M. Or, The first of the second after 2. P. M. And, If one observation be taken in the forenoon, and the other in the afternoon, that in the forenoon must Thus, If the latitude be double the Sun's meridian zenith distance, not be taken before 9. A. M. nor must the interval between that and the two taken in the afternoon must not be taken after 17 P. M. nor the first of the two observations taken in the forenoon must not

the afternoon's observation be above 34 hours.

If the latitude be three times the Sun's meridian zenith distance, other in the afternoon, that in the morning must not be before 10 A. M. and the interval between them must not be above three the first of two observations taken in the forenoon must not be before to A. M. nor the second before it A. M. Or, The first of two obervations taken in the afternoon must not be after r P. M. nor the fecond after 2 P. M. Or, If one be taken in the forenoon, and the

fecond after 14 P. M. Or, If one be taken in the forenoon, and the first of two taken in the afternoon must not be after of P. M. nor the tance, the first of two observations taken in the forenoon must not be before 10th A. M. nor the second before 11th A. Mr. Or, The hours. If the latitude be five times the Sun's meridian zenith dif. other in the afternoon, the morning one must not be before 10; A. M. nor the interval between them be above 2; hours.

If the latitude be twelve times the Sun's meridian zenith distance, the first of two observations taken in the forenoon must not be before 11 A. M. nor the second before 117 A. M. Or, The first of two taken in the afternoon must not be after of P. M. nor the second the afternoon, the morning one must not be before 11 A. M. nor the interval between them be above 1; hours. But, if the Sun's meridian zenith distance be still less in proportion to the latitude, it will be necessary to take the observations so much nearer to the noon, that after 1 P. M. Or, If one be taken in the forenoon, and the other in the advantage of the method will be very much diminished.

Precepts for making the Computation.

I. Add the logarithm fecant of the latitude by account, and the logarithm fecant of the declination together, strike out 20 (the index): call their fum the log. ratio.

II. From the natural fine of the greatest altitude subtract the natural fine of the leaft altitude, find the logarithm of their difference,

and write it under the log. ratio.

under log. ratio. It is fufficiently correct, for common use, to take the time to half minutes, but, if greater accuracy is required, the difference between the two nearest logarithms must be applied. titude by two altitudes, and, from the column of + the elapfed time, take out the logarithm answering thereto, which is also to be set down III. With half the elapfed time enter the table for finding the la-

IV. Add these three logarithms together, and, with their sum, enter the table in the column of middle-time, where, having found the greater, their difference will be the time from noon when the the logarithm nearest thereto, take out the time corresponding to it, and put it down under half the elapfed time. Subtract the leffer from

V. With this time enter the table, and, from the column of log. F f greatest altitude was taken.

garithm subtract the logarithim corresponding thereto, from this loof a natural number, which, being found in the common table of logarithms, and added to the natural sine of the greatest altitude, will give the natural sine of the meridian altitude of the Sun. From the meridian altitude of the Sun, the latitude of the place of observation

widely from the latitude by account, it will be proper to repeat the operation, using the latitude last found instead of the latitude by account, till the refult gives a latitude nearly agreeing with the latitude is to be found in the usual way.

N. B. If the latitude found by the above process, should differ

used in the computation.

E. X. A. M. P. L. E.

Being at sea in the latitude of 47° 19′ N. by account, when the Sun's declination was 12° 16′ N. at 10 h. 24 m. A. M. per watch, the Sun's altitude was found 49° 9′ and at 1 h. 14 m. P. M. per watch, his altitude was found 51° 59′: required the true latitude? Altit. Natural

Latitude 47 19 0.16880 S. Declin. 12 16 0.01003 Sines. Times.

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	1 14		65	51 59 78783	Log. ratio	0.17883
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	0 15	in col. of	f mid	l. time, o	o 15 in col. of mid. time, corresponding to 4.11667	4.11667
0 q	ime from noon 1 10 its	its logar.	4	n col. of	ime from noon 1 10 its logar. from col. of log. rifing is 3.66542 Jo. per watch 1 14 Log. ratio 9.17883	3.66542
	0		3066	nat. nun	3066 nat. num. of this log.	3.48659

Sun's mer. alt. 54 56 = 81849 nat. sine of the Sun's mer. alt. 35 4 12 16 N Declination Zenith dift.

47 20 N Latitude

[1111]

Here the latitude found by computation may be relied on as the true latitude of the place of observation, since it differs only one mile from the latitude used in the operation.

E X A M P L E

found 17° 13', and at 11 h. 17. A. M. per watch, it was found 19° 41': required the true latitude? Being at sea in 50° 40' N. by account, when the Sun's declination was 20° 0' S. at 10 h. 17 m. A. M. per watch, the Sun's altitude was

0.19803	0.22504 3.61098 0.88430	4.72032	2.96067	2.73563	
Latitude 50 40 0.19803 S. Declin. 20 0 0.02701	Log. ratio its logar.	responding to	Fime from noon o 31 its log. from col. of log. rifing is Do. per watch o 43 Log. ratio	this log.	
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34226 nat. fine of Sun's mer. alt. 200 1

98

Latitude 49 59 N

But, as this latitude differs 41 miles from that by account, it will be proper to repeat the operation, using the latitude last found instead of the latitude by account.

Lat.

0.19178	0.21879 3.61098 0.88430	4.71407	2.93223	2.71344		distance.	
Lat. 49 59 0.19178 Declin. 20 0 0.02701	Log. ratio	•	Log. ratio,	i. of this log.	•	70 o Sun's zenith distance. 20 o S	% o N
	7	I o in col. of mid. time,	o 30 its log. from col. rifing, o 43	517 nat. num. of this log. 33682	34199 = 20 0	70 20	The latitude 50
	H. M. o 30 its log.	r o in col.	o 30 its log.	0.13			The la
The State of the care in the state of the st	H. M. Elapfed time o 30 its log.		True time o 30 Do. per watch o 43	Watch flow 0 13			

The latitude last found differing only 1 mile from that used in the operation, may be depended on as the true latitude. It is evident that the operation is repeated with very little additional trouble, but few alterations being necessary.

EXAMPLE III.

Being at sea in the latitude of 60° o' N. by account, when the Sun was on the equator, and, confequently, had no declination, at I h. o m. P. M. per watch, his altitude was 28° 53' and at 3 h. o m. P. M. per watch, it was 20 42': required the trye latitude?

0.30103		3.53243 utio 0.30103 3.2314
Eatit. 60 0 0.30103 Sun's decl. 0 0 0.00000 Times. H. M. Alt. Nat. Sines. I 0 28 53 = 48303 log. ratio 0.30103 3 0 20 42 = 35348 3 0 20 42 = 35348	Elapfed time 1 o its log. in col. of # elapfed time is 2 o its log. in col. of mid. time	True time from noon. It is log. from col. of rifing log. ratio 0.30103

1703 nat. num.

48303

Nat. fine M. A. 50006 = 30 o Sun's mer. altitude. S.

60 o latitude. N.

Here the latitude by computation comes out the fame with the latitude by account, which shews that the latitude by account was right. From the foregoing examples it is plain, that the operation is the fame whether the Sun hath north or fouth declination; and it will be the same whether the ship is in north or south latitude; it is also evident that, when the Sun has no declination, the secant of the latitude is the log. ratio.

at the same place or station, but, as that can seldom be the case at sea, the necessary correction, for any alteration of station, may be rea-Hitherto it has been fupposed, that both the altitudes were taken dily made as follows.

be taken by compass (which call the Sun's bearing) and, when the second observation is taken, find how far the ship hath gone in the Let the bearing of the Sun, at the instant of the first observation,

if the ship hath gone farther from the said point, will reduce the first altitude to what it would have been found, if observed at the same statime between the observations, towards or farther from that point of This quantity added to the first observed altitude, if the ship hath moved towards the aforefaid point, or subtracted from the first altitude, the horizon in which the Sun was found at the first observation. tion where the fecond altitude was taken.

altitude was observed 18° 27' and, three hours after, it was observed 38° 23', the ship, in the mean time, having gone S. E. F. by compass, at the rate of fix knots per hour: required what the first altitude would have been found, if it had been observed at the same Thus, Suppose that when the Sun bore S. E. & E. by compass, his

to the first altitude, which will bring it to what it would have been found, if observed at the station where the second altitude was taken. Here the ship's course being directly towards that point of the horizon the Sun bore on, when the first altitude was taken, the whole So that the two afritudes for finding the latitude of the last station will distance run between the observations, viz. 18 miles, must be added

be 18° 45' and 38° 23'. Had the ship's course been N. W. W. W. or directly from the point that the Sun bore on at the time of the first observation, in that case, the 18 miles must have been subtracted from the first observed al-

horizon, may be readily found by help of the table of difference of When the ship's course makes an acute, or obtuse, angle with the Sun's bearing, the distance gone towards, or from, that point of the latitude and departure.

altitude was 26° 50', and, after failing 18 miles on a fouth course, by compass, his altitude was 37° 10': required what the first altitude would have been, if observed at the station where the last altitude Thus, Suppose that when the Sun bore S. E. by S. by compass, his

Here the ship's course making an angle of three points, or 33° 45' with the Sun's bearing, find in the table of difference of latitude and departure, what the difference of latitude will be, when the course is three points, and the distance 18 miles, and you will have 15 miles to be added to the first altitude, the ship baving gone so much towards the

titudes to be used for finding the latitude of the second station are point of the horizon that the Sun bore then on. So that the two al-27° 5' and 37° 10'.

opposite to the Sun's bearing, in that case, the T5 miles must have been subtracted from the first altitude. Had the ship's course been north, or three points from the

When the ship's course is at right angles to the Sun's bearing, or 8 points from it, in that case there is no correction necessary.

EXAMPLE IV.

Suppose a ship sailing 7 knots per hour, on an E. ; S. course, by compass, at 9 h. 55 m. 30 sec. A. M. per watch, observed the Sun's altitude 17° 33' bearing S. by E. ; E. by compass, and at 0 h. 54 m. 10 sec. P. M. per watch, observed the Sun's altitude 21° 55': required the latitude of the ship when the last altitude was taken, the latitude by account being then 47° 34' N. and the Sun's declination 19° 30' S.?

The ship's course makes an angle of 64 points with the Sun's bearing, and the distance run between the observations is 21 miles, therethe difference of latitude answering to that course and distance, which is 7 miles, to be added to the first observed altitude, the ship having gone so much towards the point of the horizon that the Sun then bore on; so the two altitudes to be used for finding the latitude of fore, from the table of difference of latitude and departure, take out the last station are 17° 40' and 21° 55'.

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47 25 N. Latitude

19

Sun's declination

Zenith dift.

Sun's bearing, by compass, being at the same time, S. by W. and at 2 h. 58 m. 20 f. P. M. per watch, the altitude of the Sun's lower limb was 16° 41° above the horizon, the eye being elevated as before, and the latitude, by account, at the time of the last observa-A ship failing N. E. F. by compass, at the rate of 9 knots an hour, at o h. 31 m. 40 f. P. M. per watch, I found the altitude of the Sun's lower limb 28° 20' above the horizon of the fea, the eye tion was 48° o' N. and the declination 13° 17' S.: required the true latitude at taking the last observation?

[117]

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Correction for the first Altitude.

The time of the first observation o h. 31 m. 40 f. P. M. of the second 2 h. 58 m. 20 f. P. M. so the elapsed time is 2 h. 26 m. 40 f. the rate of sailing is 9 miles per hour. Then, as 1 h.: 9 m:: 2 h. the Sun's bearing at the first observation is S. by W. the opposite point to which is N. by E. or 1 point. The ship's course during the elapsed time is N. E. ‡ E. or 4‡ points. So the angle the ship's course Again, 26 m. 40 f. : 22 miles, the diffance run in the elapfed time.

makes with the Sun's bearing is 3+ points.
In the table of difference of latitude and departure, to the course 3½ points, and distance 22 miles, the difference of latitude is 17 miles, while the ship sails from the Sun

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As the latitude found by computation differs but three miles from the latitude by account, it may be taken as the true latitude.

C. P.

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A TABLE for finding the LATITUDE by Two ALTITUDES.

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Riffing.	4-07595	4.08344	4-09087	4.09823	4.10188	4-10914	4.11275	4.11992	4.12348	4.13055	4.13406 4.12756	4.14104	4.14707	4.15140	4.15483	4.16163	4-16838	4.17173	4.17839	4.18171	4.18500	4.19156	4.19482	4.19800	4-20451	4-20771	4-21091	4.21725	4.22041	4-22355
Midale Time.		4-97969	4-98316	4-98660	4.98831 4.09000	4-99769	4-99337	4.99670	5-00000		5-00327	5-00650	5-00810		5.01287	-	5-01912	5.02066	5.02372	5-02524	5-02675	3-02976		5-03273				5.04004	5.04292	5.04425
Half Etapfed Time.		05/27/2003/27/2020	0.31787	0.31443	0.31272	0.30934	0.30766	0.30433	0.30103	0.29939	0.29776	0.29453	0.29133	0.28974	0.28659		0.28191	0.28037	0.27731	0-27579	0.27277	seds titored	0.26978	0.26682	0.26535	0.26389	0.26000			0.25668
<u>ب</u>		30	818	98	88	श	8 8		0 0	30	9 0		क्षि	and the last	9 6			30	a surface from	WARRIED STREET	88	30	8	30	30	8 8	श्ल	3 8	8	30
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Ħ	##	9 14	1	4 #	H A	4	H F	H	H 64	100	n n	a	त्र ।	3	9 9	" "	6	ct c	9 6	7	9 9	4	4	4 4		9 0	410	4 4	8	7
	3.88625	3,89567	3.90498	3-91420	3-91876	3-92782	3.93232	3.94123	3.94566	3-95443	3.95878	3-96742	3-97170	3.98021	3.98443	3-99280	4.00109	4.0052I	4-01337	.01743	4.02547	4-02947	4-03344	4.03740	4.04526	4.04916	4.05304	4.05090	4.06457	4.06838
Dental Company of the				St. See	20 6	3 001	3 4	3 63	3 3	0 10	3 2	3 63	3 6	3.6	40 %	40,	04	4	SECOND PROPERTY.	- PERSONAL PROPERTY.	4 4	4	MONTH MODES	Page 10 States of	MODELL STO					
Middle Time.	4-88615	4-89291	4-89513	STREET, STREET, STREET,	4-90173 3	CHECK-COM	4-90821 3	4-91247	4-91457	4-91876	4-92083	4-92494	4-92900 3-	4-93102	4-93302	-	4-93097	4.94287	4.94674	4.94865	4.95245 4	4-95434	4.95621	Pale Deposition	CONTRACTOR AND	de la la	4.90544	4.96906	4.97085	4.97264
Half Middl Etapled Time	7 7 7 7	TOP TO	4-89513	STREET, STREET, STREET,		4-90606	TOTAL STREET	4-91247	<u> </u>	4-91876	BURNESH STORY	0.37609 4-92494	0.37203 4-92900	0.37001 4-93102	0.3660z 4-9330z	0.36403 4-93700	0.360II 4.94092	0.35816 4.94287	0.35429 4.94674	0.35238 4.94865	0.35047 4.95056	0.34669 4.95434	0.34482 4.95621	0.34295 4.95808	0.33925 4.96178	0.33742 4	0.33559 4.90544	0.33376 4.90725	0.33018 4.97085	0.32839 4.97264
A PROPERTY OF THE PARTY OF THE	0.41488	0.41036	4-89513	0.40149 4-89954	4-90173	0.39497 4-90606	9282 4-90821	0.38856 4-91247	4-91457	0.38227 4-91876	4-92083	0.37609 4-92494	4-92998	0.37001 4-93102	4-93302	0.36403 4-93700	4-93097	0.35816 4.94287	4.94674	30 0.35238 4.94865	30 0.35047 4.95056	00 0.34669 4.95434	30 0.34482 4.95621	30 0-34295 4-95808	00 0-33925 4-96178	30 0.33742 4	20 0.33559 4.90544	30 0.33376 4.90725	30 0.33018 4.97085	00 0.32839 4.07264
Half Elapied Time.	30 0.41488	30 0.41036	30 0.40590 4-89513	30 0.40149 4-89954	0.39930 4-90173	0.39497 4-90606	0.39282 4.90821	30 0.38836 4-91247	0.38646 4-91457	00 0.38227 4.91876	0.38020 4-92083 0.37814 4-02280	30 0.37609 4-92494	0.37203 4-92900	00 0.37001 4-93102	0.3660z 4-9330z	30 0.36403 4-93700	0.360II 4.94092	00 0.35816 4.94287	0.35429 4.94674	30 0.35238 4.94865	0.35047 4.95056	00 0.34669 4.95434	47 30 0.34482 4.95621	0.34295 4.95808	49 00 0-33925 4-96178	30 0.33742 4	50 00 0.33559 4.90544	0.33376 4.90725	51 30 0.33018 4.97085	0.32839 4.97264

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*Kifing.	4.35865		4.36652	4-36913	4.37173	4.37432	4-37048			hi.di	4-36908	A COL	1	4	4-40225	4.40722	All and	4-41215	4.41706	4-41950	4.42193	4-42677	4	41	4	4-43874	4	4,	4.44583	4 4	4-45052		and the same of the same of	600000	4.46212	4-46671
Middle	5-10454	5.10683	5.10797	5.10910	5.11023	5.11135	7 ~	, 7			5.11797	MODEL BOX		-	5.12336		~	5.12759				5-13277		SVAN A		5.13884	-		5.14182		5.14476	ACMITMENT OF THE	100/000	5-14765		15.15052
Half Elapfed Time.	0.19648		0.19306	0.19193	0.19080	0.18867	0.18746			0.18415	0.18300		Section 1		0.17767			NAME OF TAXABLE	0.17135	100		0.16724	MANUAL VALUE OF THE PARTY OF TH	200000	COL	0.16219		0070200		- CONTRACT	0.15627	A COLUMN TO THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF T	110000			0.15051
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. . . .	00 00	39	39	9	40	41	42	42	43	43	44	45	45	46	46	47	48	40	4 6	30	50	51	52	52	53	5.45	54	55	-55	50	50	57	185	58	59	8 2
M	4 4	1 1	8	8	a	9 6	1 6	1 0	7	ď	2 10	1 61	63	6	8 6	1 8	7	9 9	4 4	8	d	4 4	8	7	7	1 H	7	4	લ	4 0	3 6	64	18	d	4	4 00
		n in the	véstilite Augusta		gapris.	ale some	196796 -13775																												(•
Riffing	4.22980	4.23599	4.23907	4.24214	4-24520	4.24825	4.25430	4-25731	4.26031	4.26330	4.26628	4.27220	4.27514	4-27807	Eco. 5253a	4.28681	1000000	4-29257	4-29830	4-30115	4-30398	4.30061	4	4-31523	4-3180I	4-32355	4-32631	4.	4 4	4.33452	4.33724		4	illo de	4-35069	4-35335
Middle Time.	5.04718	5-04059	.05130	5.05278			3-05090	.05962		5.06232	5-06365	.06621	fraction (see section		5.07025	5-07284	7413	5-07542	5.07070	5-07923	5.08049	5.08175	5.08424	-08548	3-08671	5-08794	5-09037	8-00158	5-09279	5-09399	5.09518	.09755	5.00872	5.09990	5.10107	5-10223
AE,	5.0	200	2.0	5.0	5.0	5.0	5	5.0	5.0	5.0	5.0	200	100	3.00	5.0	0	5.0741	5.0	010	3.0	5.0	5.0	5.0		5.0	5.0	5.0	अ	5.0	5	3.5	5.6	1:	3, 50	M	2
		0.25104 5.0		, 0	10000000	550	2000 HOL	171	. 2			0.23472 5.0	ALCOHOL:	Redu				3277 /	0.22306 5.0	MARKETS	Accept the	0.21802 5.0	-	40	(BESSARI)	0.21309 5-0	decided	0.20945 5.0	ALCOHOL: MARKET	TO STREET	0.20585	0.20148 5	0.20230	0.20113	0.19996 5	0.19880 3
70.0	CONTRACTOR OF THE PERSON NAMED IN CONTRA	0.25244	0.24964 5	0.24825 5	0.24687	550	0.24413	171	0.24006 5	0.23871	0.23738	CHARLISTIN	0.23340	0.23209	0.23078		0.22690	0.22561	COLUMN TO SERVICE	0.22180	0.22054	-	0.21679	0.21555 5	0.21432	STILL STORE	0.21066	ecultisass	0.20824	0.20704	COLUMN TO SERVICE SERV	0.20148 5	0.20230	0.20113	0.19996 5	2
Half Elapsed Time.	0.25385	30 0.25104	00 0.24964 5	30 0.24825 5	00 0.24687	30 0.24550	20 0:24413	0.24141	30 0.24006 5	00 0.23871	30 0.23738	0.21472	00 0.23340	30 0.23209	00 0.23078	0.22819	30 0.22690	00 0.22561	0.22306	30 0.22180	00 0.22054	0.21802	30 0.21679	00 0.21555 5	30 0.21432	0.21309	00 0.21066	30 0.20945	00 0.20824	30 0.20704	20 0.20585	0.20148 5	30 0.20220	00 0.20113	30 0.19996 5	0.19880 3

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Rifing.	444444444444444444444444444444444444444	4.64603
Middle Time.		5.21960
Half Elapfed Time.	0.11104 0.11027 0.10273 0.10273 0.10495 0.1049	0.08143
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Rifing.	4.46899 4.47127 4.47127 4.47127 4.47127 4.48926 4.48924 4.48926 4.48924 4.49145 4.50225 4.5	4 4
Middle Time.	5.15146 5.15344 5.15344 5.15334 5.15437 5.15436 5.16664 5.17663 5.17664 5.17663 5.17664 5.1	5.18766
Half Elapíed Time.	0.14498 0.14488 0.14488 0.14488 0.14488 0.14488 0.14488 0.13844 0.13848 0.13889	0.11337
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	CONTRACTOR OF STREET	(A.5.96) (A.5.179)	A STATE OF THE PARTY OF THE PAR	-							-	/	(D)/17(C) (17(C))	RESERVED AND THE		WATER STATE	100 miles	Helician	SOURCE R		V-200								
Riffing.	4-72471 4-72628 4-72786	State Black	4-73254	4-73565	4-73874	CHECK WINESES	4-74535	STATE OF THE PARTY.	4.74945	4 4	4	नं न	4	4.75997	14	4-70443	Sec. 18	2136	All and	(Solik	4.77471	1	4.7	in the	4.70194	29000			6 4.78909
Middle Time.	5-44697 5-44747		5-249945	5-25043	Maria Maria	AND DESCRIPTION OF THE PERSON NAMED IN	5-25329	-	5-25423		Accessed toward	5.25052		5.25707	Agent extracts			5-25048	-		5.26260			5.2638	8 5.20425	02005.50	7 5.26546		
Half Elapfed Time:	0.05406 0.05356 0.05306	0.05256		0-05060	A CONTRACTOR OF THE PARTY OF TH		0.04821		ASSESSMENT OF THE PARTY NAMED IN		20 Page 12 Co.	0.04451	0.0	0.04272	1000-0512	0.04184	1000	0.04055		NAME OF TAXABLE PARTY.	0.03885	PERSONAL PROPERTY.	MERCHANICA COM				0.03557		
	888		Cal X-	88			3000	200	8 %	8 8		3000	IN C	8 6	400	8 2		위 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전 전	el el		000					70	28 30		30 00
X	888	10 4	4 to 13	4 12 4		4 13	4 4	4	4 4 16	4 16	4 17	4 4 5 5 5 5	No. b	4 20		4 21 21	4 22	4 22	4 23		4 24	4 2 2		4 26	4 27	1	4 4		4 4
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lateral and an arrange party																													
Rifing	4-64957 4-65134 4-65110	4.65661	4.65806	4.66184	4-665.39	4.66874	4.67217	4.67388	4.67728	Standard	4.68235	4.68,71	STATE STREET,	4-69071	Mar. Sa	4.69403		4.69897	100	4	4.70550	14	Station in	De Jillie		MARKET	4.71837		
Middle Rifing.	5.22151 4 5.22214 4	5.22338 4	3.02462	5.22585 4	See the	A A	5-22886	3.23004	5.23063	5.23280	5.23295	5.23400	5-23466	5.23579	5.23635	5.23746	5.23801 A	5-23856	5.23965 4	5.24019	5.24073 4	5.24179 4	5.24232 4	5.24285	5-24337	3.24.300	5.24441	5-24544	5.24595
THE PARTY OF THE P	0.07889 3.42151 4 0.07889 3.42414 4	0.07765 5.22338	0.07641 5.22462 4 0.07579 5.22524 4	0.07318 3.22585 4	0.07397 5.22706	0.07337 5.22766	0.07217 5.22886 A	0.07099 3.23084	0.07040 5.23003	0.06923 5.23180	0.06808 5.23295 4	0.06751 5-23352	0.06637 5-23466	0.06524 5.23579	0.06468 5.23635	0.06257 5.23591	0.06302 5.23801	0.06247 5.23856 4	0.06138 5.23965 4	0.06084 5.24019	0.00030 5.24073 4	0.05924 5.24179 4	0.05871 5.24232 4	0.05818 5.24285 4	0.05760 5.24337	0.05714 5.24389	0.05602 5.24441	0.05559 5-24544	0.05508 5.24595
Middle Time.	5.22151 4 5.22214 4	30 0.07765 5.42338 4	3.02462	0.07518 5.22585 A	00 0.07397 5.42706	30 0.07337 5.22766 4	5-22886	30 0.07099 3.23004	5.23063	30 0.06923 5.23180 4	00 0.06808 5.23295	5.23400	300.06637 5.23466	5.23579	00 0.06468 5.23635	5.23746	30 0.06302 5.23801	00 0.06247 5.23856 4	5.23965 4	30 0.06084 5.240T9 4	5.24073 4	00 0.05924 5.24179 4	30 0.05871 5.24232 4	00 0.05818 5.24285 4	30 0.05760 5.24337	20 0.05714 5:24,369	5.24441	30 0.05559 5.24544	0.05508 5.24595

A TABLE for finding the LATITUDE by Two ALTITUDES.

Rifing.	•	4-85363	4.85490	4.850r7	8 8 8 7 4 4	4.85996	4.8612T.	4.86246	4.80371	4.86621	4-86745	4-86869	4-86993	4-87116	4-87262	4-87484	4.87606	4.07728	4.87971	4.88092	4-88213	4.8834	4-88574	4.88694	4.88672	4.89052	4.89171	4.89289	4.89407	4.89525	4.09043	4-89877	4.89994		4.90227	4-90343
Middle Time.	800	5-28249	S	5.28305	28260	5.28387	5.28414			5.28520	5-28546	5-28572	5-28598	5.28623	5-28672	5-28698	5-28722	5-20740	5-28794	5.28817	5.28840	5-28863	5.28909	5.28931	5.28953	No. of Concession, Name of Street, or other Persons, Name of Street, or ot	-	5-29040	5.29061	5.29082	5-29103	5.29143	MARKET STATE	Market Programmer	SECON STREET	5.29222
Half Elapfed Time.	90.0		0.01826	0.01798	001770	0.01716	0.01689	0.01662	0.01035	0.01009	0.01117	0.01531	0.01505	0.01480	0.01455	0.01405	0.01381	0.01357	0.01333	0.01286	0.01263	0.01240	0.01194	0.01172	0.01150	0.01100	(0.100)00	SEATO STATE	REGISCOSCORIO	Section 1	0.0100	SECTION SEC	No. of London	0.00920	MAN CONTRACT	0.00881
ď		3 %	00	30	318	38	30	8	क्ष	30 0	8	30	8	30	302	8	क्ष	8 8	2 8	30	위	30	30	8	श्र	3 6	8	30	8	30	3 6	2 8	30			8
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Riffing.		4-79334	4-79475	4.79016	4-79750	4.80036	4.80175	4.80314	4-80453	4.80591	4-80867	4.81004	4.81141	4.81278	4.81650	4.81686	4.81821	4.81950	4.82226	4.82360	4.82494	4.82028	4.82894	4.83027	4.83159	4.83423	4-83554	4	41	4	4	4.84337	4		4	named lad
Middle Time.		5.26743	5.26782	2500,00000	05002.5	5.26034	S.2697I	5.27008	5-27045	5.27082	5-27154	5.27190	5.27226	5.27262	5.27297	5.27367	5-27402	NEW COLUMN	5.27470	5-27538	5.27571	5.27604	5.27670		\$100 E-100 5.27700	5.27831	5.27862	5-27893	5.27924	5.27955	5.28015	STREET, ST		-	5.28134	
Half Elapfed Time.		0.03399		0.03283	0.03245	0.03170	0.03132	0.03095	Carle Co.	0.03021		0.02913	CASTORISMS	Charles States	0.02300	0.2017.000	manual be	-	0.02699	20000000	0000000000	0.02466	STREET, STATE		(Called Mark	0.02330	A CONTRACTOR	0.02241	0.02210	2001203	HE SHOP SEE	0.02110	National Control	-		696100
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×								STATE OF STREET	STATE OF THE PARTY.	STATE OF THE OWNER, WHEN		Continues of	The second second		CONTRACTOR OF	No. of Concession,	SECTION S	A STATE OF THE PARTY OF	COLUMN TWO IS NOT	CONTRACTOR OF THE PARTY OF	BERNSON TO	ALP SHAD	The same	-	7	er neggen	100000	GOVE THE	Ber T	A THE	200	1000	Walley Com	WEST STATE	TO SHIELD	4

Apparent Altitudes.

		1		-													Section 86	er telluzio				Little All									.6										
Rifing.		4.95624	4.95832	4-95936	4.96040	4.96143	4.96246	4	4.90452	4.905.54	4.067.8	4.06860	4.06061	4-07062	4.07162		4	4	4-97505	4-97005	4.97865	4-97964	4.98063	4.98162	4.98261	4.08359	1	dillo.		and the same	4	41	4	4		4	eren one Promite	PERIOD DA	4.99715		4-44403
Middle Time.		5.29903	5.29921			5-29945	5-29953	5.29961	5.29909	2 20082	5-20000	5.20007	5.20004	\$ 300IO	5.10016	Janua.		Back III.	5-3003	5.30043	5.3005	5.3005	2	5		5-30074	Alast.	All links	5.30086	5.30088	5	2	5	2	ο,	٠,	0	5	NAME OF	DESIGNATION OF	3.30103
Half Elapfed Time.		0.00200		0.00174	0.00166	0.00158	0.00150	4	STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL STEEL ST	0.00127	0.00120	0.00106	0.00000	0.00003	0.00087	0.00081	0.00075	0.00000	0.00065	0000000	0.00055	0.00045	0.00041	0.00037	0.00033	0.00029	0.00023	0.00020	0.00017	Elly Made	(Inches on the	Complete	NEW PROPERTY.	1000		a control	mars-and		0.00000	-	
ė.		8 8	8	-		30	8	30	8 8	श्ल	8 8	2 6	302	9 8	30	8	30	8	3	8 8	3 8	30	8	30	8	3 6	30	8	30	8	30	8				8			30		30
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A TABLE of Corrections to be added to the apparent Altitude of the Moon's Centre, for reducing it to the true Altitude.

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To find the Latitude at Sea from the Moon's Meridian Altitude.

The Moon's altitude may be taken either by a fore or back observation, exactly in the fame manner as the Sun's altitude, only, you must bring that edge of the Moon into contact with the horizon which is round and well defined, whether it be the upper or lower

limb. Then apply the following corrections.

I. The femi-diameter, to be found in the Nautical Almanac for every noon and midnight at Greenwich, to be added when the lower limb is taken, but fubtracted when the upper limb is taken.

II. The dip of the horizon is to be subtracted in the fore observaand to be added in the back observation. tion,

the Nautical Almanac for every noon and midnight at Greenwich, which being known, her parallax, at any altitude, may be readily found, to the nearest minute, by the preceding table of corrections, which are the differences between her parallax in altitude, and the re-These three corrections give the true altitude fraction corresponding to that altitude, and must be always added her observed altitude. of the Moon's centre. To find the Time of the Moon's passing over any Meridian, either to the East or West of Greenwich.

to, or fubtracted from, the time of the Moon's fouthing at Greenwich on the proposed day, according as the longitude is west or east, will give the Greenwich time of her southing at the ship. day following, or between her passing on the proposed day, and day preceding, if the ship be to the east of Greenwich; and, with this difference, and the ship's longitude in time by account from Greenminutes, which add to the ship's longitude in time, this sum added wich, take out of the following table the corresponding number of to the well of Greenwich, take the difference between the time of her passing over the meridian of Greenwich on the proposed day, and The time of the Moon's passing over the meridian of Greenwich, is given for every day in the Nautical Almanac; but, if the ship be

Daily

Daily Variation of the Moon's Southing in Minutes.

itude sruce.	Suod oH ai		H	1	2	3	4	5	9	7	∞	6	10	11	. 12
Var	70	1	M	3	9	∞	11	14	17	61	.22	25	28	31.	33
Var	65	1	M	3	5	∞	IO	13	91	18	2.1	23	26	29	31
ğ	99	1	M	d	5	7	01	12	14	17	61	22	24	- 36	29
, B	5.5	1	M	8	+	7	6	11	13	15	81	20	22	24	26
Yar	50	1	M	8	4	9	œ	IO	12	14	91	18	20	22	24
var	45	1	M	8	7	20	7	6	11	13	15	91	81	20	22
Ĕ	4	1	M	. 7	3	Ŋ	9	∞	10	11	13	15	91	18	61
itude grees.	Long n De	:	0	. r.5	30	45	9	7.5	8	105	120	135	150	165	180

To find the Moon's Declination at any given Time of her Southing.

two declinations, the one preceding, and the other following, the given time, fubtract the lefs from the greater, and fay, by the rule of proportion, if 12 hours give the difference, what will the time befor any intermediate time as follows. Take out of the Ephemeris The Moon's declination is computed in the Nautical Almanac for give: Now, this proportional part added to, or fubtracted from, the Moon's declination at the preceding noon, or midnight, as the declievery noon, and midnight, at Greenwich, and may be readily found tween the preceding noon (or midnight) and the Moon's fouthing nation is increafing or decreafing, will give her declination correspond-

ing to the given time. Note first. If the time between the Moon's fouthing and the fol-

lowing noon, or midnight, be taken, a proportional part may be found (as before) which added to her declination at the following noon, or midnight, if decreafing, or fubtracted, if increafing, will give her declination at the given time.

Note fecond. If the Moon's declination, taken out of the Epheneris for noon and midnight, change its name from north to fouth, or from fouth to north, the fum of the two declinations of contrary denominations is to be accounted the difference; and, in this cafe, the difference between the proportional part, and the preceding, or following declination (according as the intermediate time is counted from the preceding, or following, noon, or midnight) will give her declination at the given time, and of the fame name with the greater From the true meridian altitude and declination, the latitude of the place of observation is to be found in the usual way.

AMPLE

May 25th, 1787, in longitude, by account, 50° W. of Greenwich, the meridian altitude of the Moon's lower limb was observed to be 38° 14' S. the height of the eye being then 20 feet above the furface of the fea: required the ship's latitude?

and the ship's longitude 50° (equal to 3 h. 20 m. in time) the table gives 5 m. which added to the ship's longitude in time, makes 3 h. 25 m. and this added to 7 h. 26 m. the time of the Moon's southing at Greenwich May 25th, gives 10 h. 51 m. the Greenwich time of By the Nautical Almanac, the Moon fouths, May 25th, at 7 h. 26 m. May 26th, at 8 h. 9 m. the daily variation is 43 m. with which,

the Moon's fouthing at the ship.

The Moon's declination, May 25th, at noon, is 1° 21' S. and, at midnight, is 3° 58' the difference is 2° 37', therefore, fay, by proportion, as 12 h: 2° 37':: 10 h. 51 m.: to 2° 22', which, added to portion, as 12 h: 2° 37':: 10 h. 51 m.: to 2° 22', which, added to 1° 21' the Moon's declination, May 25th, at noon (because it is integral.) creafing) gives 3° 43' S. the Moon's declination at the time of her fouthing at the ship.

The Moon's horizontal parallax, May 25th, at midnight, is 56°, and her femidiameter 15', therefore,

Apparent

18 14 S.	38 29	38 25 43	39 8	50 52 S. 3 43 S.	47 9N.
		riz. paral. 56	•		
's lower limb	2 .	38° 25' and ho	•		
e of the Moon meter,	for 20 feet,	on to the altit.	idian altitude,	· • 'uo	
Apparent altitude of the Moon's lower limb - 38 14 S. Add the femidiameter,	Subtract the dip for 20 feet,	Add the correction to the altit. 38° 25' and horiz. paral. 56 43	Moon's true meridian altitude,	Zenith distance, Moon's declination,	Latitude, -

Ħ I I ч × 4

Suppose an artist, 16° E. of Greenwich, on the 3d January, 1790, by a back observation, with Hadley's quadrant, finds the meridian altitude of the Moon's upper limb to be 39° 30' N. the observer's eye being 16 feet above the horizon of the sea: required the observer.

er's latitude?

By the Ephemeris, the Moon fouths, January 2d, at 13 h. 33 m. January 3d, at 14 h. 27 m. the daily variation is 54 m. with which, and the silves 16° (equal to 1 h. 4 m. in time) the table gives 2 m. which, added to 1 h. 4 m. the ship's longitude in time, makes 1 h. 6 m. and this sum subtracted from 14 h. 27 m. the time of the Moon's southing at Greenwich, January 3d, 1790 (because the longitude is E. of Greenwich) leaves 13 h. 21 m. the Greenwich time of the Moon's southing at the ship.

The Moon's declination, January 3d, at midnight, is 10° 7' N. January 4th, at noon, is 7° 51' N. the difference is 2° 16'; therefore, as 12 h.: 1 h. 21 m. solve 12 h.)

:: 2° 16': 15', which subtracted from 10° 7' N. the Moon's declination, January 3d, at 13 h. 21 m.

The Moon's horizontal parallax, January 3d, at midnight, is 591, and her femidiameter 16 m. therefore,

ing the latitude at sea, to take out of the Ephemeris the Moon's horizontal parallax, and semidiameter to the nearest minute for the noon, or midnight, which is nearest the time of her fouthing at the N. B. It is fufficiently correct for the mariner's purpose, in find-

To reduce Degrees, Minutes, &c. into Time.

Multiply the degrees, minutes, &c. by 4, observing to carry one for every 60 to the next denomination, and place the remainder of each denomination orderly under the line, then divide the product of the degrees by 60, the quotient will give the hours, the remain-der will be the minutes, seconds, &c. to be affixed to the hours. EXAMPLE

[133]

EXAMPLEC,

Reduce 124, 9 into time.

60)496 36

8 16 36 makes 8 h. 16 m. 36 fec.

EXAMPLE IL

Reduce 35 39 into time.

60)142 36

2 23 36 makes 2 h. 23 m. 36 fec.

EXAMPLE III.

Reduce 32 54 45 into time.

60)131 39 0

2 11 39 makes 2 h. 11 m. 39 sec.

MB

A TABLE

the Longitude from the Meridian of London, with the Time of A TABLE of the LATITUDES and LONGITUDES of PLACES, reckoning High Water on the Day of New or Full Moon. Note, H. W. stands for High Water; R. for River; I. for Island; P. for Point; and C. for Cape.

	H.W.	Lat.	Long.	•	H.W.		Long.
	H.M		D.M.		H.M.	H.M. D.M.	D.M.
Berwick	2 30	55 48N		The Downs	I 30	SI 25 N	I 27 E
Holy Island		55	H	South Foreland	10 30	SI 10	₹ 30
Staples	2 30		. 80 €	Dover	11 30	51 6	I 22
Sunderland Point		55 35	I 33	Rye	II IS	5 T	0 50
Coquet Island		55 20	1 25	Dungennefs	9 45	50 52	0 54
Tinmouth	3 0	55 3	I I7	Haftings	IO IS	50 52	0 46
Sunderland	3 30	54 55	8	Beachy-head	12 0	50 44	0 70
Harrlepool	30	54 43	0.58	Arundel	9 45	50 50	0 34W
Stockton Bar, or			Separate Sep	Shoreham		50 55	0 17
Teefmouth	3 30	54 4I	0.55	The Owers	9 15	50 39	0 40
Whitby	3 45	54 30	0.50	Chichefter Harbour		50 47	0.55
Robinhood's Bay	いな	54 27	0 20	Portfmouth .	11 15	50 48	1 1
Scarborough Head	3 45	54 18	0 0	Spithead Road	9 30	50 48	I 13
Flamborough Head	4 30	54 9	OIIE	St. Helen's Road	0 6	50 43	0 55
Burlington Bay	3 45	54 7	4 0	Cowes, Ifle Wight	IO 45	50 48	91 1
Spurnhead Lights	\$ 30	53 38	0 27	Bembridge, Do.	10 15	50 40	0 H
Bolton Harbour	0 9	53 9		Dunnole		30 38	1 15
Lyon		52 55	200	Needles		50 41	1 34
Biackney		53 0	0.55	Feveral Point		50 30	77 I
Cromer		53 5		St. Alban's Head	m	50 35	
2000		52 57	0 58	Weymouth	0;		200
Varmonth	9 45	53	1	Fortiand Fymolith Don	6 15		30
Tentout	9 30	5.4	1 44	Torbon	2 4		300
Sole Bat	9 45	52 30	1.54	Lorday	9 4		3 6
Alderhoromoh	9 30		1 5.4	Grart Doing	200	20.00	
Orfordnefe	9 45	24 10	1 12	Plymouth	2 7	6	4 20
Harwich	7 45	52 11	81	Eddifton	9		
Ipfwich			1 15	Ramhead			4 25
The Nore	12 0	51 34	0 48	Falmouth	5 20	No. of Concession,	5 10
London	3 0	51 32	0 0	Lizard	7 30	BUSHINE	5 14
King's Channel a-		Constant of the Constant of th		Mount's Bay		20	5 48
long the Swin	12 0	\$1 38	1 16	St. Mary's Isle	3 45	49 58	0 40
Margate Road	II 45		1 20	Land's End	7 30	30 6	10000
See All	10 30	51 25	124	Scilly Illand	3 45	20	
Dentill Knock, a			1	Guerniey Illand			37.00
Pomfmos		51 42	I 45	Jeriey mand	0 30	49	200 00
Deal .	30	7.	77 1	Cameria St. Acres light house	**	149 30	

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nt 6 0 51 6 50 51 6 45 51 5 15 51 8 30 52 1 10 15 53 1 1 15 53 1 1 15 53	and v Ifland	3	15	SI	15	4	40
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nt 6 50 51 6 45 51 5 15 51 6 0 51 7 0 52 8 30 53 4 houfe 9 45 53 11 15 53	ort Point	•		51	12	4	40
6 50 51 6 45 51 5 15 51 6 0 51 8 30 52 8 30 52 10 15 53 11 15 53 11 15 53	reland Point			51	91	4	-
6 45 51 5 15 51 6 0 51 8 30 52 8 30 52 8 30 52 1 1 1 53 1 1 1 53	ng's Road		50	51	29	cł	50
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7 o 52 8 30 53 8 30 53 11 15 53 11 15 54	rdfev Iffe		30	52	44	2	0
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t house 9 45 53 53 11 15 54 11 15 54	rnarvon		30	53	9	4	30
11 15 53 11 15 54	erries light house		45	53	7.4	4	44
11 15 53 11 15 54	neffer _			53	10	7	2.5
11 15 54	verpool	11		53	7.7	7	30
	ancafter	11		54	42	4	36
11 15 54	hitehaven	11		54	25	3	30
111 15 54	arlifle	II		54	47	4	35

The Coast of Scotland.

Kirkendhright	II	0	54	AKN	•	\$ 2 W
Mall of Caloway	11	C		200	, ,	3 (
•	:)	+	37	?)
Arran IIIe	II	0	30	0	3	12
Mull of Cantire	01	30	55	17	9	٥
Rowri Point			58	14	3	54
,~	9	30	56	48	1	37
S		,	20	35	٥	37
Shy S. point	v	30	57	15	9	91
3	,	,	57	30	9	30
la islan			57	44	00	18
Faro Head, or Cape	٥		c			
Wrath	×	15	28	9	4	30
Dungfby Head	II	15	58	45	3	9
Tarbetness			57	50		36
Dornoch	12	0	500	3	3	46
Cromartie	12	0	57	44	3	45
Kynaird's Head	12	0	57	43	H	38
Peterhead	0	30	57	30	I	34
Aberdeen	0	45	57	9	1	45
Montrofe	H	45	56	34	7	0
Dundee	4	15	56	3.6	*	48
Fifeness	H	0	56	15	4	3
He of May				Io	4	37
Leith .	7	15		58	3	
Dunbar	17	0		58	d	19805
Eymouth	4	0	55	54	-	3

The Coast of England. | Orkney and the Shetland Isles.

H.W. Lat. Long. H.M. D.M. D.M.	0 58 44N 2 IIW	10 30 59 24 3 23	8	0 59 30 I 24 0 60 I2 I 20	3 0 59.54 I 3I	0 60 47 0 10	157 22 110 30
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Ise of Man.

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Calf of Man Douglafs	Ramíay Bay Point Ayre Peel Hill

The Coast of Ireland.

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The Coast of Ireland.

The Coast of France and Portugal.

	Rochelle	Nantz	Bourdeaux	Bayonne	Bilboa	Cape Ortegal	Cape Pinas	Cape Finnisterre	Oporto	Burlings	Bayonna Ifles	Lifton	Cape Roxent	Cape St Vincent
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The Coast of Holland and Flanders.

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The Coast of France and Portugal.

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The Coast of Hudson's Bay, and the Straits.

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The Coast of Iceland, Greenland, Nova Zembla, and the Northern

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The Coast of Iceland, Greenland, The Coast in the Sound and Baltic.

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land, 1 h. 30 m. Jutland Isles, oh. om. Friesland coast, 7 h. 30 m. Zealand coast, 1 h. 30 m. Flanders coast, oh. om. Reardy and Normandy coast, 1 oh. 30 m. Biscay, Gallician, and Portugal coasts, 3 h. o m. Irish W. coast, 3 h. o m. Irish S. coast, 5 h. 15 m. Africa ing times ferve for coasts of confiderable extent, and will serve nearly for the places on those coasts. Finmark, or N. W. coast of Lap-America E. coaft, Besides the times of high-water in the preceding table, the follow-America W. coast, 3 h. o m. W. coast, 3 h. o m. 4 h. 30 m.

The Latitude of any two places being given, to find the difference of Latitude between them.

If the latitudes are both north, or both fouth, fubtract the less from. the greater, the remainder will be the difference of latitude. T D

But, if one latitude be north, and the other fouth, then add then together, and their fum will be the difference of latitude.

What is the difference of latitude between the Lizard and Barbadoes?

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being multiplied by 60, and the odd 29 minutes 60 3149 miles. taken in, will give the difference of latitude in

The latitude failed from, and the difference of latitude being given, RULES FOR LATITUDE. to find what latitude the ship is come into,

latitude to the fouthward, add the difference of latitude (it being first brought into degrees, if need be, by dividing it by 60) to the latitude failed from, the sum will be the latitude you are come into, of the When you fail from north latitude to the northward, or from fouth

failed from, the jum win sailed from.

A ship from a place in the latitude 14° 10' N. fails to the northward till she make her difference of latitude 4° 21'. What latitude is she

14° 10' N. 18 31 N. Difference of latitude Latitude failed from Latitude come into

A ship from latitude 29° 17' S. fails to the southward till she make her difference of latitude 374 miles: What latitude is she come into?

Latitude sailed from Difference of lat. 374 miles, divided by 60 makes 6 14 S. XAMPLE

Latitude come into CASE II.

When you fail from north latitude to the fouthward, or from fouth

latitude to the northward, fubtract the difference of latitude, if leaft, from the latitude failed from, the remainder is the latitude come into,

of the fame name with the latitude you failed from.

But, if the difference of latitude be biggeft, then fubtract the latitude tude from the difference of latitude, the remainder will be the latitude

come into, of a contrary name to the latitude you failed from.

E X A M P L E I.

A ship from latitude 49° 14' N. fails to the fouthward till her difference of latitude be 521 miles. What latitude is the come into?

Latitude failed from - 40° 14' N.

Diff. of lat. 521 miles, divided by 60, makes 8

Latitude come into

A ship from latitude 4° 18' S. fails to the northward till her difference of latitude be 10° 24'. What latitude is she come into?

Difference of latitude Latitude failed from

18, OI

Latitude come into

RULES FOR LONGITUDE.

The longitudes of any two places being given, to find the difference of longitude between them.

T

If the longitudes be both eaft, or both west, subtract the lesser from the greater, the remainder will be the difference of longitude.

But, if one longitude be east, and the other west, then add them together, and their sum if less than 180 degrees, will be the difference of longitude; but, if it be more than 180 degrees, then fubtract it from 360, and the remainder will be the difference of longitude.

EXAMPLE

What is the difference of longitude between Cape Finisterre and

Cape Finisferre, in longitude Antigua, in longitude -

9° 12' W. 62 4 W.

The difference of longitude

52 52 W. EXAMPLE

What is the difference of longitude between Barcelona and the Rock of Lifton? EXAMPLE II.

2° 18' E. 9 25 W. Barcelona, in longitude Rock of Lifbon, in longitude

The difference of longitude

E X A M P L E III.

What is the difference of longitude between the S.E. Point of Jaand the Island of St. Christopher?

140° 30 E. 62 40 W. S. E. Point of Japan, in longitude St. Christopher, in longitude

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The longitude failed from, and the difference of longitude being given, to find what longitude the ship is come into.

CASE

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When you fail from east longitude to the eastward, or from west longitude to the westward, add the difference of longitude to the longitude failed from, the fum, if less than 180 degrees, is the longitude come into, of the same name with the longitude you sailed from.

But, if the fum should be more than 180 degrees, then subtract it

from 360, and the remainder will be the longitude you are come into, of a contrary name to the longitude you failed from.

E. X. A. M. P. L. E. I.

A flip from longitude of 48° 21' eaft, fails to the eaftward, till fle make her difference of longitude 287 miles. What longitude is the come into?

Difference of longitude 287 miles, or Longitude failed from

M P L Longitude come into

W. fails to the westward till What longitude is the come A ship from the longitude of 178° 47' her difference of longitude be 12° 17'.

Longitude

178° 47' W 12 17 191 4 360 0	56 E.
178° 47' 12 17 191 4 360 0	168 56 E.
Longitude failed from Difference of Longitude Exceeds 180 Subtract it from	Remains the Longitude come into

When you fail from east longitude to the westward, or, from west longitude to the eastward, subtract the difference of longitude (if it be least) from the longitude you failed from, and the remainder will be the longitude come into, of the same name with the longitude failed from.

But, if the difference of longitude be the biggest, then subtract the longitude from the difference of longitude, and the remainder will be the longitude come into, of a contrary name to the longitude failed

A ship, from longitude 98° 17' E. sails to the westward till she make her disference of longitude 14° 21'. What longitude is she come into?

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A ship, from longitude 44° 21' west, sails to the eastward till her ference of longitude be 81° 42'. What longitude is she come difference of longitude be 81°

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The Use of the Table of Meridional Parts.

De marked M, beginning at o, and the meridional parts, and Ä other mark'd 1d, 2d, &c. the degree of la the first ending at 59, contain the last column of every nutes answering to every the titude they fland under. of Latitude, this Table, answering to columns contain gree

36, fame for So that, if you would find Sid. the the meridional parts answering the latitude 51,32, liw nov the meridional the left-hand, and above any latitude, suppose 32 (in to which prefix in the column under the for minutes) E. that fland right against figures 3620, parts required example, 20, two towards column column ınakes look find and the 9

Two Latitudes being given, to find the Meridional Difference of Latitude.

105

Cafe 1st, If both latitudes be north or both fouth, fubtract the meridional parts of the leffer, from the meridional parts of the greater, the remainder will be the meridional difference of latitude.

303

310

Cafe 2d, If one fatitude be north and the other fouth, then add their meridional parts together, and the fum will be the meridional difference of latitude.

25509

078

24842

80

24215

23685

920

373 391 409 428

23226

[153]

A TABLE of Amplitudes, from the Latitude oo deg. oo min. to the Latitude 12 deg. either North or South.

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Declin					1		.4		1											

A TABLE of Amplitudes, from the Latitude 13 deg oo min. to the Latitude 24 deg. either North or South.

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7 4		182112	2 2 4 4 2	28572	4448 8844
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d		189888	28.28.8		78 60 12 24 2
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	2	18 48 51	34 36 45	28 28 2 9	
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		188282	1 4 4 8 H	488 44 50 5	22 20 20 22 2 2 4
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14 4 4 4 4 4 4 4	Z	18888	12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	18 48 4 4 4	7 4 7 1 2 8 2 1 1
8	a	189888	28,28 8	13 1 2 2 2 2 2	3 L 8 8 H 4 8 4
	2	182281	2 2 2 2 2 2	12888881	284 E 2 C 0 4 C
		182884	28 28 8	0 1 2 2 2 2 2	5 7 to 5 5 4 2 4
	2	188255		44666	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
2	0	89888	8 8 8 8	5 1 2 2 2 2 2	3228 6 6 4 4 5
		188488	11 22 77 61	1 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	22444442
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Degree Declina	s of	0 4 4 6 4	20 200	5 1 4 2 4 7	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

A TABLE of Amplitudes, from the Latitude 25 deg. oo min. to the Latitude 36 deg. either North or South.

98	Z	18	14	28	43	57	II	25	39	54	8	23	300	53	8	4	39	55	II	27	43	8	18	33	53	30
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	2	18	13	27	40	53	90	20	33	47	8	13	700	42	56	=	25	39	54	IO	2.5	40	36	13	29	90
8	À	18	10	62	03	8	90	5	000	6	=	12	13	14	15	ri,	18	61	20	77	23	24	25	27	780	29
	2	18	12	25	37	의	8	15	27	39	22	40	18	31	44	S	II	25	39	53	07	21	36	51	00	4
	•	8	IO	70	03	8	90	50	000	6	9	12	13	14	15	اء	18	61	20	7.1	23	24	2.5	50	500	200
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A TABLE of Amplitudes, from the Latitude tude 37 deg. oo min. to the Latitude 48 deg. either North or South.

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A TABLE of Amplitudes, from the Latitude tude 49 deg. oo min. to the Latitude 60 deg. either North or South.

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tude 61 deg. oo min. to the Latitude 66 deg. either North or South. A TABLE of Amplitudes, from the Lati-

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The Use of the TABLES of Amplitudes.

horizon, either northerly or The amplitude of the Sun, or any star, is so many degrees distance as they rise or set from the east or west points of the foutherly

the east toward the north at their rifing, or from the west toward the north at their fet-Note. When the Sun or stars the amplitude found by thefe tables must be reckoned from have north declination, then

toward the fouth at their rif-But, if they have fouth declination, then the amplitude must be reckoned from the east ing, or from the west toward the fouth at their fetting.

To find the true Amplitude by the Tables.

at the top of the table, and the declination in the first column to the left-hand, and in the common angle of meeting you will find the amplitude requir-Look for the given latitude ed, in degrees and minutes.

When the latitude and declination are both given in even degrees, as for example. Suppose I would know the Sun's true amplitude at his rifing, in the latitude of 40° o' his declination being 17° o' N. Under latitude 40°, and right against declination 17°, I find 22°

26', which is the Sun's true amplitude, to be counted from the east towards the north, because it is at his rising, and the declination is north, that is, east 22° 26' north.

When the latitude is given in even degrees, and the declination in degrees and minutes, as for example. Suppose I would know the Sun's true amplitude at his fetting, in the latitude of 57° o' his declination being 11° 33' fouth. Find his amplitude as before, for the latitude 57°, and for the

Declination { 11 deg. } which will be } 22 25 then

subtract the lesser from the greater, the dist. is 1 56 or 116 minutes, to which put two cyphers, and it makes 11600, which number must be divided by the number standing against the odd minutes of declination (in the following table) which, in this cafe, is 181, and the quotient gives the proportional parts in minutes, which parts are always to be added to the leffer of the two amplitudes that you took the difference of, and the fum gives the true amplitude as follows.

181)11600(64 proportional parts in minutes. makes 1 degree 4 minutes.

Proportional parts to be added Leffer of the amplitudes

because at Sun-setting, and the declination south. True amplitude

CASE III.

When the declination is given in even degrees, and the latitude in

degrees and minutes, as for example. Suppose I would know the Sun's true amplitude at his rifing, in the latitude 51° 14', his declination being 14° o' fouth.

Find his amplitude as before, to 14 degrees declination, and for

The latitude \{ \frac{51}{52} \deg. \} which will be \{ \frac{22}{23} \frac{37}{8} \} and fubtract

is o 3r minutes. the leffer from the greater, the difference

To the difference of amplitudes found, which is 31, put two cyphers, and make it 3100, which must be divided by the number flanding against the odd minutes of latitude (in the following table) which, in this case, is 428, and the quotient gives the proportional parts in minutes, to be added to the lesser of the two amplitudes, as in Case II.

428) 2100(7 proportional parts in minutes.

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104 Leffer of the amplitudes			

When the latitude and declination are both given in degrees and minutes, as for example. Suppose I would know the Sun's true amplitude at his setting, in the latitude 49° 18' his declination being

First, find his amplitude for latitude 49 degrees, and declination

19° 41' (as in Cafe II.) which will be 30° 53' In the same manner, find his amplitude for latitude 50 degrees, and declination 19° 41', which will be 31° 35'

Then, from the greater amplitude, Subtract the lesser

Put two cyphers to this difference, it makes 4200, which must be divided by the numbers standing right against the odd minutes of the given latitude (in the following table) which, in this case, is 333, the quotient 42 minutes. 0 Remains the difference

quotient gives the proportional parts in minutes, to be added to the leffer of the two amplitudes, &c.

333)4200(12 proportional parts.

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			Proportional parts to be added -	E	Iruc amp, for lat, 49 '16', and deci. 19' 41' N. W. 31 5 N.

tional Parts to the odd. Minutes of Latitude or A TABLE of Numbers for finding the propor-. Declination, in finding the Sun's true Amplitude.

Num- bers.	130	127	125	122		811	1115	113	111	100	107	105	103	IOI	
Odd Minutes	4	47	48	49	50	51	52	53	- 54	55	26	27	, &	20,	
ė s		87			7.1	99	62	8.5	54	0,5	94	13	30	20,	33
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Num- bers.	375	353	333	316	300	285	273	192	250	240	230	222	214	207	200
Minutes.	91	17	18	19	20	21	22	23	24	25	56	27	28	29	1 30
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The use of the foregoing Table is to find a number to divide the difference of amplitudes by, in order to find the proportional parts, when the amplitude is required for any latitude or declination that is given in degrees and minutes (as in the foregoing Cafes) to find which number, look in fome of the columns under the title of odd minutes for your given minutes of latitude or declination; as suppose for 37 minutes, and right against that you will find 162, which is the number required.

To find the Variation of the Compass by an Amplitude.

To do this, you must have given both the true and magnetical amplitudes.

The magnetical amplitude is to be found by the compass, at the time of the Sun's rising or setting, and is so many degrees or minutes as you see it rise from the east, or to set from the west either to the northward or to the southward: As sor example, Suppose, being at sea, I find, by setting the Sun with my compass, that he rises to deg. 15 min. to the northward of the east, then the magnetical amplitude is east to deg. 15 min. north; or, suppose I find by the compass, that he sets 14 deg. 12 min. to the southward of the west, then the magnetical amplitude is west 14 deg. 12 min. south.

Then, if your true amplitude and magnetical amplitude are both The true amplitude is to be found by the tables as before taught.

to the northward, or both to the fouthward, fubtract the leffer from the greater, the remainder is the variation.

But, if one be to the northward, and the other to the fouthward, add them together, and the fum will be the variation.

A. M. P

E. 18 34 N. E. 22 37 N.	3 Eaft	11 S.
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amplitude	1 2	True amplitude Magnetical amplitude
True amplitude Magnetical amplitude	, k	nplitude ical amp
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9 17 Westerly. Variation

And thus having found how much the variation is, it remains, in the next place, to find which way it is, that is, whether it be callerly or westerly.

R U L E.

tude be farther from the north than the true amplitude is, then the If the amplitude be taken at Sun-rifing, and the magnetical ampli-

variation is westerly; but, if it be nearer to the no th, it is easterly. If it be taken at Sun-setting, if the magnetical amplitude be farther from the north than the true amplitude is, then the variation is eafferly, but, if nearer to the north, it is wellerly, as may be feen by the two foregoing examples. The bearing of any Celeftial Object may be found by calculation, if its declination, altitude, and latitude of the place of observation be known.

The bearing is called its amplitude, or true amplitude, when the object itself is in the horizon; but, if it be clevated above the hori-

zon, the bearing is called its azimuth, or true azimuth. The word true is prefixed to the amplitude, or azimuth, thus found, in order to distinguish them from the amplitude, or azimuth, taken by

the compass, which are termed magnetical. It is evident, that if the magnetical bearing agree with the true, the compass has no variation, but, if they disagree, then the difference between the true and magnetical amplitude, or azimuth, is the variation. The variation is always reckoned from the north; and, consequently, if the true amplitude, or azimuth, of the object be to the right-hand of the observed, the variation is easterly, but, if it be to Given the latitude of the place, and the declination of a Celeftial Object.

it must be added to 90°, and this difference, or sum, will be the true amplitude reckoned from the north. To the fecant, less radius of the latitude, add the fine of the declination, the fum is the log. fine of the true amplitude, reckoned from the east or west, and of the same name as the declinanorth point of the horizon, this amplitude from the eaft or well, if the declination be north, must be taken from 90°, but, if south, tion. But, as it is generally required to have the amplitude from the SOLUTION.

THE THE POST E.

Sun was observed to rise by the compass N. 70° 30' E. Required the In latitude 28° 10' N. the Sun's declination being 18° 59' N. the variation of the compass?

28 10 = 0.05474 18 59 = 9.51227 Secant, lefs radius of the lat. Sine of the Sun's declination

21 39 = 9.56701 00 Sine of the true amplitude,

68 21 E. becaufe the Sun is rifing. Magnetic amplitude N. 70 30 E. True amplitude N. 68 21 E. Or true amp. from the north, True amplitude

to the left of the observed. 9 W. because the true amplitude Difference is the variation 2

To work an Azimuth.

The true azimuth of a celestial object is its bearing, when above usually reckoned from the fouth, when to the fouthward of the east or west points of the horizon; and, when to the northward of those points, it is reckoned from the north; but, it is generally more conthe horizon, from the north or fouth points thereof. venient to reckon it always from the north.

opposite to the four lines in the compass box; hold the box in this of the card, will give the magnetical azimuth required. If the Sun does not fhine frong enough to give a diffinct shadow, look through The magnetical azimuth of a celeftial object, is its bearing by the compass when above the horizon, and is found in the following manly along the middle of the index; then the degrees in the arch intercepted between that end of the index next the Sun and north point one of the fights, and move the index till the string cut the Sun's centre; and then the intercepted arch, as before, shews the Sun's azitre of the Sun) the shadow of the string joining the sights fall directposition, and move the index till (the fights being directed to the cen-

thus: Let one observer look through the fights, and turn them till the thread cut the centre of the Sun, while the second observer attends to muth, and in like manner may the azimuth of a flar be found. When there is a rough sea, the observation is best made by three persons cide with the cardinal points. If the card should vibrate very much, take the middle degree between the limits to which the vibration reaches. The third observer constantly attends to the Sun's altitude the position of the card, and, by moving the index, causes the first observer to move the box, so that the cross lines in the box may coinwith Hadley's quadrant.

The amplitude is taken in the fame manner as the azimuth.

of azimuths, for example, five or fix, and find the variation from The mean of all these will be nearer the truth than any fin-It is necessary that the navigator should take a considerable number

Those who have the charge of ships ought to be aware, that the quantity of refraction disfers very much in low altitudes, and that it is, therefore, very abfurd to make any confrant allowance, as too many observers do. The refraction ought to be taken out of the table for every altitude. It is likewise to be remarked, that the proper time to take the amplitude is when the Sun's lower limb is a little then really in the horizon, as may be eafily understood from the table more than a femi-diameter above the horizon, because his centre

Having the latitude of the place of observation, and the Sun or Star's declination, with the altitude at the time of observation, the true azimuth is found as follows.

vated pole. Find the fum of the co. latitude, the co. altitude, and the polar diffance. Take half this fum. Find the difference between SOLUTION. If the latitude and declination be of the fame name, the declination taken from 90°, but, if they be of different names, the declination added to 90°, will be the polar distance from the elethe polar distance and the half sum: Then find the sum of the four

following logarithms, viz.

The fecant lefs radius of the latitude.

The fecant lefs radius of the altitude.

The log. fine of the above-named half fum.

The log. fine of the above-named difference.

the true azimuth, which doubled is the true azimuth reckoned from the north, if the latitude be north; but, if the latitude be fouth, take those degrees from 180°, and the remainder will give the true azimuth from the north. Note. The secant less radius of an arc being equal to the arithmetical complement of the co. fine of that arc is here used, as being cafier understood, and is found in the table of secants by inspection, only omitting the first figure in the fecants' index.

EXAMPLE I

A STATE SOOT STATE

In latitude 43° 39' N. the Sun's declination being 16° 37' N. his observed altitude 39° 28' and his magnetical azimuth N. 120° 30' E. Required the variation of the compass?

To find the true Azimuth.

90 0 90 0 90 0 43 39 Alt. 39 28 Decl. 16 37	Secant less radius of the lat. 43 39 = 0.14052	Sine of the half fun, 85 8 = 9.99843 Sine of the difference, 11 45 = 9.30887	Sum 19.56021	52 56 co. fine = 9.78010	Sun's true azimuth from the north 105 52 ° ' Nagnetical azimuth, N. 120 30 E. True azimuth, N. 105 52 E.
90 0 43 39	332	9 1	23 8	45	1
8 5	46 21 50 32 73 23	91 041	73 %	1	azir
Lat	Co. alt. 50 32 Co. alt. 50 32 Polar dift. 73 23	Sum	Sub.P. dift. 73 23	Difference 11 45	Sun's true

14 38 W. Which

Difference is the variation,

Which is westerly, because the true azimuth is to the left of the 911.10 8BH observed.

OF THE X A M P L E T HE IN THE

In lat. 0° 11' N. the Sun's declination being 4° 6' S. and his observed altitude 6° 7', his magnetical azimuth was N. 96° 9' W. and his magnetical amplitude, at fetting, was N. 96° 6' W. Required the variation, both from the azimuth and amplitude?

To find the true Azimuth.

• 00 4	94 6	33 54 = 9.85766 39 48 = 9.80625	9.83319	
90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Polar dift.	the alt. 6 7 1, *133 54 ce, 39 48	47 4 co. fine = 9.83319	04 8 W.
90 o Alt. 6. 7	Co. alt. 83 53 Secant lefs radius of	Sine of the half fuin, *133 \$4 = 9.85766 Sine of the difference, 39 48 = 9.80625		Sun's true azimuth from the N. o4 8 W.
• 00 0	89 49 83 53 94 6	133 54	rence 39 48	true azi
Ľt.	Co. lat. 89 49 Co. alt. 83 53 Polar diff. 94 6	Sum 267 48 Half fum 133 54	Difference 39 48	Sun's

N.96 9 W. Magnetical azimuth,

Which is eafterly, because the true azimuth is to the right-hand of 2 FE. Difference is the variation, the observed.

OFF THE CHARGE STATE

^{*} When the half fum exceeds 90°, subtract it from 180°, and take the log. fine of the remainder.

o 11 = 0.00000 4 6 = 8.85429	W. 4 6 S. = 8.85429	= 94 6 W. becaufe the declination is fouth.
Secant lefs radius of the latitude, Sine of the Sun's declination,	Sine of the rrue amplitude,	Or true amplitude from the north,

Which is eaflerly, because the true amplitude is on the right of the 6 W. o E. Difference is the variation, Observed amplitude, True amplitude,

In latitude 13° 10° N. the Sun's declination being 16° 59′ S. his obferved altitude 17° 50′ and his magnetical azimuth N. 90° 10′ E. Required the variation of the compass? observed.

To find the true Azimuth.

90 00 17 50	ar dift. 1	Sine of the difference, 21 0 = 9.55432	r lo	56 30 co. fine = 9.74r95
90.80	76 50 72 10 ft.106 59	255-59	Polardift. 106 59	Difference 21 - o
00000	Co. lat. Co. alt. Polardiff.	Sum	Polar d	Differe

Sun's true azimuth, N. 113 o E. Sun's magnetic azimuth, N. 90 10 E.

The difference is the variation, 22

22 50 E.

the brund eine Erre X a And We P Le Le East IV. erre String arrange of salibest

In latitude 16° o' S. the Sun's declination being 22° 58' S. his observed altitude 30° 22', and his magnetical azimuth N. 120° 43' E. It is required to find the variation of the compass?

Answer, 13° 7' W.

To work an Azimuth by the Gunter's Scale.

did before); there fix it, and open the compaffes till the other point the half fum, extend the other point to the co. lat. observing whether the second point falls to the right or left of the first, and take the co. alt. and let the fecond point fall where it will (the fame way it point to the left, and observe what degrees and minutes, in the versed Sor. Find the co. lat. the co. alt. the half fum and difference, as above. tent; then fet one point of the compasses on the brass pin at the beginning of the scale of versed sines (marked V. S.) turn the other fines, it falls on; those degrees, &c. will be the azimuth from the Then, on the scale of log. sines, set one point of the compasses on compasses off, without altering their extent. Set one point on the north, if the lat. be north, but from the fouth, if the lat. be fouth. fall on the difference, then take them off, without altering their

fometimes happen, then hold the Gunter flat on a board, and there, on let the over-point rest, and thence take the extent to the difference, If the extent, when applied from the co. alt. to a fourth num. should reach beyond the right-hand end of the scale, as it will

N. B. If the half fum be more than 90°, fubtrack it from 180°, and work with the remainder.

Of the Log-Line and Half-Minute-Glafs.

scription of them here; therefore, I shall only make a few remarks The log and log-line by which a ship's run is measured, are so well known to every mariner that it would be unnecessary to give any deon the manner of dividing the log-line, and trying the half-minute-

From several very exact mensurations that have been made on different

hour, and 42 feet the 120th part of 5000 feet (nearly). This mea-fure is, therefore, put for the length of a knot; and, although many mariners find, by experience, that this length of the knot is too thort, yet, rather than quit the old way, they use glasses, for half-minute between knot and knot, and answers to a glass that runs 30 seconds: This 50 seet being divided by 10, gives 5 seet to every fathom, therefore, in cashing up the log-book, in the column of fathoms, each fathom answers to rith of a knot, and 10 sathoms make a knot, an ancient custom, and is still too much used, to measure only 42 feet between each knot, which is grounded on the supposition that 5000 feet make a mile; and because half a minute is the 120th part of an ones, that run but 25 feconds, which is but correcting one error by which is certainly the best method for practice. But, it hath been nutes in an hour) gives is feet for the distance between knot and knot. But, as it is fafer to have the reckoning rather before the ship than after it, therefore, 50 feet may be taken as the proper distance parts of the earth's furface, by able mathematicians, it is found, that a fea mile contains about 6120 feet, this divided by 120 (the half mi-

The length of the knots on the log-line may be examined by applying a known meafure to them: And, to know how many feconds the glafs runs, you may try it by this eafy

R U L E

is 9.8 inches long, at the other end, let there be a loop, to hang it on a small pin, or nail, fastened in any place so that the bullet may swing freely. Then, the loop of the string being hung on the pin, and the string 9.8 inches long, from the end of the loop to the middle of the bullet, and the bullet caused to swing, each of those swings shall be half a true second of time, and 60 of them the just length Let a bullet he fastened to one end of a thread, or filk string, that of an half-minute-glafs.

Rules for keeping a Journal.

By keeping a journal is meant, keeping fuch an account of the ship's way, that, at any time, you may be able to know what latitude and longitude the ship is in.

When any ship is bound from any one place to another, that lies so

from; and, at the time of taking fuch departure, the captain or mate generally takes the bearing and diffance of that land, according to his time she leaves the land, she is said to take her departure, and that part of the land she then leaves, as suppose the Start, the Lizard, the Land's End, &c. is faid to be the place they take their departure judgement, and fets it down on the log-board, or in the log-book, afar from it that she is obliged to go out of fight of the land for any confiderable time, as suppose from England to Madeira, then, at the gainst the time it was taken, thus,

Lizard, N. by W. distance 5 leagues. Or, Start, N. N. E. distance 6 leagues, &c.

And, in the fame manner, for any other place, bearing, and diftance, as you will fee in the first day's log, in the following journal.

The log-book being marked as follows, with columns for courfe, distance, northing or fouthing, easting or westing, latitude by observation, meridian distance, diff. of longitude,

and longitude in, you are to take notice,

That, in the column for course, you are always to set down the course you have made by your reckoning for that 24 hours (that is, from the noon of the day before, to the noon of the day you work on) the sea account being always kept from noon to noon.

In the column for distance, you are to set down the distance made

by your reckoning for that 24 hours.

In the column of northing or fouthing, you are to fet down the difference of latitude made that 24 hours, marking the column with N. if the difference of latitude be northerly, or with S. if it be fouthIn the column of easting or westing, you are to set down the departure made that 24 hours, marking the column with E. if the departure be easterly, or with W. if it be westerly.

you are to fet down the lati-In the column marked Lat. by D. R.

tude you reckon yourfelf in on that day.

In the column marked Lat. by Obf. you are to fet down the lati-tude you find yourfelf to be in by observation, if you have one, if then let it fland open. not,

In the column for Mer. Dist. you are to set down (in degrees and minutes) how much departure you have made in all, from the place you took your departure from. In the column marked Diff. Long. you are to fet down the difference of longitude made in the 24 hours.

In the column of Long. in, you are to fet down what longitude you find yourfelf to be in on that day by your reckoning.

In the last column, you are to set down the bearing and distance of

Note. The bearing and distance is seldom wrought, except when the land is supposed to be near.

And now, having (I think) given a fufficient account of things that are to be fet down in the different columns, I shall lay down these sew necessary rules following, and then proceed to shew how they are all to be found, or the method of working a day's work at fea.

allowed upon all courses steered, and upon all bearings, &c. that are taken by the compass; that is, if it be easterly variation, it must be R U L E I. Variation, if there be any (as most commonly there is) must be allowed to the right-hand; but, if westerly variation, then to the lefthand of the course or bearing: Supposing yourself placed in the centre of the compass, and looking directly sorward to the point you are to allow the variation from.

Suppose I steer S. W. and there be one point westerly variation, then my true course will be S. W. by S. or, suppose I set a point of land, and find it to bear, by my compass, E. S. E. and I know there is half a point easterly variation, then the true bearing is S. E. by E. ‡ E.

Ω

Lee-way (which I shall not here describe, because sufficiently known to every seaman) must be allowed to the right-hand of the course when the larboard tacks are aboard, and, to the left-hand, when the starboard tacks are aboard.

EXAMPLE.

Suppose I steer N. E. by E. with my larboard tacks aboard, and make one point lec-way, then my course made good is E. N. E.

R U L E

Lee-way and variation, when they are both to be allowed one way,

that is, both to the right-hand, or both to the left, add them together, and allow their fum the fame way they were to be allowed.

ther to the left, fubtract the leffer from the greater, and allow the remainder the fame way as the greater of them was to be allowed. But, if they are to be allowed, one to the right-hand, and the o-

EXAMPLE

make one point lee-way, there being at the fame time half a point Suppose I steer N. N. W. with my starboard tacks aboard, and westerly variation, I would know my true course?

Variation to the left-hand . o + Point I o Points Lee-way to the left-hand

The fum to be allowed to the left-hand I : Point makes the true course N. W. by N. W. W.

EXAMPLEIL

Suppose I steer S. W. by W. with my larboard tacks aboard, and make 2 t points lee-way, and I have I t points wellerly variation, what is my true course?

Lee-way to the right-hand Variation to the left-hand

2 + Points

The remainder to be allowed to the right-hand 1 & points, makes true course W. S. W. & W.

RULE

When a ship is lying-to, under a main-sail, mizen, &c. then obferve how she comes up and falls off, and take the middle between the two points, and from that allow the lee-way and variation, as in

E X A M P L E.

Suppose a ship lying-to, under a main-sail, with the starboard tacks aboard, come up E. by S. and fall off to N. E. by E. there being one point westerly variation, and she make since points lee-way, what course does she make good?

The

allowing fix points to the left-hand (by rule III.) the true will be N. by E. The middle between E. by S. and N. E. by E. is E. by N. from

Currents, the way they fet you, and the diffance you suppose you are driven by them, is to be fet down in the traverse-table for the day, THE PARTY as any other course or distance.

E X A M P L E.

I mile per hour, the variation being one point eafterly, then, if pais, 1 mile per nour, une variation come, in the traverse-table, as Suppose I try the current, and find it to set W. by N. per coma courle, W. N. W. distant 24 miles.

M. R U L

by my compais, there being ; point westerly variation, I then set down, in my traverse-table, S. W. by S. ; W. with so much dif-Heave of the fea is to be accounted for in the fame manner as currents: As, suppose there is a great sea heaving toward the S. W. down, in my traverse-table, S. W. by S. tance as I judge the sea has heaved the ship.

VII. UL

At leaving the land, the opposite point to the bearing (with the variation allowed upon it) and the distance you judge yourfelf from it, must be set down in the traverse-table, as a course and distance.

E X A M P L E.

Suppose, having 1 4 point W. variation, the Start bear, by my compass, N. N. E. distant 4 leagues. The opposite point to N. N. E. is S. S. W. which, with the variation, makes S. & W. for the course to be fet in the traverse-table, distant 12 miles.

Rules to find the Meridian Distance. G. A. S. E. L.

GASE. I. If the meridian diffance on the day you work from be eaft, and, if

if you have failed to the eastward; or, if it be west, and you have tance, and the fum will be the meridian distance you have made, of ed to the westward, then add the departure to the meridian dis THE WAR CALL the same name with that you wrought from.

EXAMPLE

Meridian distance made in all 5 55 W. Meridian distance, - 4° 18'
Departure, westerly, 97 miles, or 1 37

CASE II.

If your meridian distance be east, and the departure be westerly; or, if the meridian distance be west, and departure easterly, then subdistance you have made, of the same name with the greater of the two. tract the leffer from the greater, the remainder will be the meridian

E X A M P L E I.

Meridian distance - 7° 34' W.

Departure easterly - 1 16 Meridian distance made in all 6 18 W.

Howard of

Signer of

Meridian distance 3 17

Departure easterly 3 17 Meridian distance made in all 1 43 E.

Rules to correct the Dead-Reckoning by an Observation.

variation, lee way, currents, &c. and still find that your latitude, by dead-reckoning, will not agree with the latitude by observation, then When you have made all proper allowances you can, fuch as, for the reckoning must be yet farther corrected. It must be acknowledged, that the correcting of a sea-reckoning is a very precarious operation, and, at best, is little more than a probable guess, since nothing now appears whereby the mariner can know afforedly whether he be to the caftward or westward of the point where his reckoning places him: However, the following are the common, and feem to be the most rational, methods.

CASE

If the course sound by dead-reckoning be less than 33 degrees.

R U L E.

course; to this course, and the difference of latitude by observation, find the true distance and departure; and, to this course, and the To the difference of latitude and departure by account, find a meridional difference of latitude between the observations, difference of longitude.

CASE

If the course found by dead-reckoning be more than 33 degrees, and less than 56 degrees.

U. L. E.

the departure by account, for the true departure, with which, and the difference of latitude by observation, find the true course and distance, and to this course, and the meridional difference of latitude by ob-fervation, find the difference of longitude. With the difference of latitude, and departure by account, find the tion, find another departure; take half the fum of this departure, and distance; with this distance, and the difference of latitude by observa-

CASE III.

If the course found by dead-reckoning be more than 56 degrees.

R C L

the meridonial difference of latitude by observation, find the diffe-With the difference of latitude, and departure by account, find the tion, find the true course and departure, and, with this course, and distance, with this distance, and the difference of latitude by observarence of longitude.

20 DOM

[177]

To correct for several Days.

By the help of the three preceeding rules the longitude may always be corrected for a fingle day; but, if an observation has been wanted for several days, then mark the latitude and longitude at last observation; or, if this be your first observation since leaving the land, mark the latitude and longitude of the land you left; this is the only latitude and longitude you can call certain; all the following part of the reckoning must undergo a correction, which is made as follows.

CASEL

Reckoning from the last certain latitude and longitude, when the course given by the meridional difference of latitude and difference of longitude by account, taken as a difference of latitude and departure, is less than 33 degrees.

R U L -

To the meridional difference of latitude, and difference of longitude by account, find a course, with this course, and the meridional difference of latitude by observation, find a corresponding departure, which will be the correct difference of longitude.

CASE IL

When the course given by the meridional difference of latitude, and difference of longitude by account (taken as in the first Case) is more than 33 degrees, and lefs than 56 degrees.

RTUE

To the meridional difference of latitude, and difference of longitude by account, taken as a difference of latitude and departure, find a distance; with this distance, and the meridional difference of latitude by observation, find a corresponding departure, half the of this departure, and the difference of longitude by account, of this departure, and the difference be the correct difference of longitude.

CASE III.

When the course given by the meridional difference of latitude, and

and difference of longitude by account (taken as before) is more than

R U L E

servation, find a corresponding departure; this departure will be the correct difference of longitude. To the meridional difference of latitude, and difference of longitude by account, taken as a difference of latitude and departure, find a distance; to this distance, and meridional difference of latitude by ob-

the fame opposite courses she went outward, her meridional distance will not be the same, but will differ, less or more, according to her different courses in croffing different meridians and parallels; whereas, the difference of longitude between any two meridians remains always It may be here remarked, that the diffance between any two meridians on the globe, varies according to the parallel of latitude on which it is meafured, confequently, if a ship fail not homeward on

For these reasons, the three rules for correcting the dead-reckoning ferted, instead of the method commonly used in the former editions of this book.

JANA PAR

V O Y A G E

ENGLAND TO MADEIRA

HAPPY JANET OF LONDON,

A. B. COMMANDER, KEPT BY T. W. MATE.

Departure taken from the Lizard, in Latitude 49° 57' N. Longitude 5° 44' W. bound for Funchal, in Madeira, in Latitude 32° 38" N. Longitude 17° 6' W.

Bearing from the Lizard S. 26° 59' W.-Distant 1166 Miles.

K. F. Courfes. Winds. Leeway. Remarks on board, Monday May 5th.	fair weather. At 6 P. M. the Lizard bore N. by E. diftance 6 leagues, from which I take my departure. Variation 1 point wefterly.	Dif. Diff. Depar-Lat.by Lat.by Mer. Diff. Long. Bearing and tance Lat. ture. D. R. Obser. dift. Lon. in. distance.	o 48 75 6 29W Diff. 1059 miles
Leeway.	4	at.by Lat.	21
Winds.	N. E.	Depar-L ture.	48 W. 48
Courfes.	S. W. by W. N. E.	Dif. Diff.	diles 107 96 S.
H. K.F.	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Courfe E	S.27 oW. 107 96 S. 48 W. 48 21

The Lizard bearing N. by E. dift. 6 leagues from the ship, is the same as if the ship had sailed from the Lizard 6 leagues or 18 miles upon the opposite, or S. by W. point of the compais, and allowing for the variation, as before taught, makes it S. half E. dist. 18 miles, which is to be set down as the first course and distance in the following Traverse Table.

The first course shall we have some state of the same state of the course shall we have some states.

W. by S. half W. and the sum of all the distances sailed on that course till two o'clock, when it alters, is 18 miles an half, which being doubled, because the log. is heaved every two hours, gives 37 miles, so the second course and dist. to be set down in the traverse table is S. W. by S. half W. 37 miles. In like manner, the second course seed is S. W. and the variation allowed makes it S. S. W. half W. and the dist. on that course summed up and doubled, gives 56 miles; therefore, the third course and distance to be set down in the traverse table is S. S. W. half W. 56 miles. Having found the whole difference of latitude and departure made upon the several courses, I then mark down upon my state or paper what every thing that is to be found comes to, and afterwards set them down in their proper columns as above.

E 18 17.9 .by S. tw. 37 28.6 . W. tw. 56 49.4 95.9	E. W.
26	100
4.00	
	\$ - \$ -

than .5, or a half, you must call that side I mile more than you find it to be; but, when they are less than .5, then you need take no notice of them. But, when you take the diff. of lat, and departure to find the course, take them in miles and tenths. When the tenths on any .fide are more NoTE.

1250 6° 29' W. our to diff. of let. 95.9 S. and dep. 48.1 W. course is S. 27° W. diff. 107 miles; then ailed from, or Lizard's MER. PARTS. en, to course 270 and mer. diff. lat. 147 Long. in, or hip's long. 6 29 W. To find the courfe and distance to the in-5° 14' Ψ. MER. PARTS. 57' N. 3470 2073 17 fo Ship's long. 6 36 S. liff. of longitude is 75 miles. Funchal long. ailed from, or Lizard's or fhip's lat. 48 Long. failed from Ship's lat. 48 21 N. Funchal, 32 38 N. Diff. long. diff. lat. 943 tended port. of lat. Diff, lat. In miles

The course and distance is found as above by Case I. of Mercator's failing.

Courses Winds Leeway Remarks on board, Tuesday, May 6th.	weather a little thick. At 4 P. M. spoke with the Charming Nancy, bound from Caroling to London. Variation 1 point westerly.	Dif. Diff. Depar-Lat.by Lat.by Mer. Diff. Long. Bearing and tance Lat. ture D. R. Obfer. diff. Lon. in diffance	1 41 79 7 48W Diff. 952 miles.
Leeway		R. Dy Lat.	48
Winds N.	N. W.	Depar-Lature D	53 W 46
R. Courfes W. S. W. by W. N.	S. W. by S. W. N. W.	Dif. Diff. Depar-Lat.by Lat.by Mer. I tance Lat. ture D. R. Obfer. diff.	Miles 107 93 S
H. K. F.	408 0 4 4 4 0 8 0 7 7 7 7 8 8 8 4 4 7 4 4 7 7 4 4 7 0 7	Courfe L	S 30 0 W 107 93 S 53 W 46 48

The variation being allowed, and the distances summed up, as in the preceding page, the traverse table, and other work will be as follows.

. 93.4, and depar	MER. PAR	33.2 27.3 Lat. in yesterday 48° 21' N. 3323 34.4 Diff.lat. 93 miles, or 1 · 33 S. 25.8 T.8 Lat. in, or ship's lat. 46 48 3185 93.4 52.5
w to diff. of la	303, the court	in yesterday lat-93 miles, or in, or ship's lat.
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TRAVERSE TABLE.	1	39
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Then to course 30° and mer. diff. lat. 138, the diff. long. is 79 miles.

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To find the course and distance from the ship to Funchal.

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42	Diff. lat.
Ship's lat. Funchal's lat.	

So, from the ship to Funchal, the course is S. 26° 40' W dist. 952 miles

ednefd. May 7th. lerate gales and ip to the north-	1. first reef both	efterly.	Fuochals.28°46'W
H. K. F. Courfes. Winds Leeway. Remarks on board, Wednefd. May 7th. 2 4 4 4 6 4 6 4 Courfes. Winds Leeway. Remarks on board, Wednefd. May 7th. fair weather. At 6 P. M. faw a fhip to the north-	ward. At 2 A. M. took in first reef both topsails.	S 4	S 30W 97 96S 14W 45 12 45 23 155 21 8 2W Dift. 873 miles.
Winds Leeway.		Dif. Diff. Depart Lat.by Lat.b	4W 45 12 45 23
H. K. F. Courfes. Winds Leeway.	5 0 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Dif. Diff. ID	S 8 30W 97 96.S
H 2 49	* 0 " u 40 a	12 4 12 4 Courfe	S 8 30V

Allowance being made for the variation on each course, as before, and for the lee-way on the two last courses, the traverse table and other work will be as follows.

Now to diff. lat. 96, and is S. 8° 20' diff. 07 miles.	46.4	1 3	rfe 89	Long, failed from	Long. in by account
iff. lat.	from	D. R.	the cou	failed f	ong. in by a
So to d	failed	Lat. in by D. R.	ien to	Long	Long.
Is S.	Lat.	Lat.	F.	•	
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TRAVERSE TABLE.	Dift. N.	24	40		
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the course. R. PARTS. 3187	3047	t miles.	W 21 W 8
Now to diff. lat. 96, and dep. 14, the course is S. 8° 30' dift. 97 miles. MER. PARTS. Lat. failed from 46° 48' N. 3187 Diff. of lat. 136 S.	5 12 N.	ong. is 2	nt .
diff. lat. 96, diff. 97 mil from 40	D.R. 4	rdo, the diff. of land.	Diff. long Long. in by account
Now to diff is S. 8" 30' di Lat. failed fra Diff. of lat.	Lat. in by D. R. Mer. diff. lat.	lat. 140, t Long.	Diff

Here the lat. by dead-reckoning differing 11 miles from the lat. by obser. I correct for the ic long. And as this is the sire observation got since leaving the land I work as follows.

Mer. Parts.

3470 3047 423	3470	3° 14' W. 8 9 W. 2 55 175 mi	o minte (nagrila)
	1	Ship's long. by account, Diff. of long. by account, 2 55 175 mi	at all and a the
R. 49° 57' N. B. 45 12 N. by D. R.	Lizard's lat. 49° 57' N. Ship's lat. by obf. 45° 25 N. Mer. diff. lat. by obf. 59.	account,	The her over
Lizard's lat. 49° 57' N. Ship's lat. by D. R. 45 12 N. Mer. diff. lat. by D. R.	Lizard's lat. Ship's lat. by ob Mer. diff. lat.	Lizard's long. Ship's long. by Diff. of long. t	THE LESS ASSET

To mer. diff. lat. 423, and diff. long. by acc. 174, the course is 2 points (nearly): And because it is less than 33° I correct by Case I.

Therefore, to course, 2 points, and half mer, diff. lat. by obs. 2035.5 (because the whole is too large to be found in the table) the diff. of long. is 84.2, which doubled, because the other was halfed, gives 168 miles.

Ship's true long.

The course and distance to the intended port is found as above. 2 48 W. 8 W. W. Lizard long.
True diff. long. 168, or
Shin's true long.

M wwwwwwwwww	F. Courfes Winds Leeway Remarks on board, Thursday May 8th.	Thefe 24 hours moderate gales, with fone rain. Handed main top-fail.	Variation 17 point westerly.	obf. dift. Lon, in diffance	1 4317E. 7 45W Diff. 817 miles.
K. F. Courfes 3 5 S. by W. 2 W. 3 5 S. by W. 3 5 S. by W. 3 5 5 5 5 5 5 5 5	Winds Le	W. by s.		e D.R.	£ 44 8
Source Sassassassassassassassassassassassassass	Courfes	S. by W.		if. Diff. Depince Lat. tur	illes 76 75 S 12]
	K. F.	######################################	12 0 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	Courfe ta	o CE

The variation and lee-way being allowed on each course, as before, the traverse table will be as follows.

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and depart-ne is S. 9° E. and Mer. Parts. 13° N 3062

2957 N 8

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Then to the course 9°, and the mer, diff. lat. 106, the diff. of long. is 17 miles.

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To find the course and distance from the ship to Funchal.

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Ship's	Funchal's lat-	Diff. la	

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So, from the ship to Funchal, the course is S. 32° 23' W. dift. 817 miles.

Friday May 9th.	gales and fqually,				efterly.	Bearing and distance	Funchal S 31° W Diff. 800 miles.
H. K. F. Courfes Winds Leeway Remarks on board, Friday May 9th.	Thefe 24 hours hard gales and fqually, with rain.	• (-4,4			Variation 17 point westerly.	Course Diff. Diff. Depar-Lat.by Lat.by Mer. Diff. Long. Bearing and tance Lat. ture D.R. Obs. diff. Lon. in distance	2 8 40 8 25 W Diff. 800 miles.
Winds Leeway	S. S. W. 3	off N. by E. 5. hour.	٠,	N.W.b.W.E.W.		epar-Lat.by Lat.by	5 W 44 4
F. Courfes	٠ ١	8 Lay to np n.w.by n. off N. by E. 5	2 Up N. W. of N.	S. W.		e Dif- Diff. D	S 81. 30 W 25 4 S 25 W 44 4
H. K.	14 41 w w	8 Lay	2 Up	-0 00 C	12 5	Courfe	\$ 81.30

Taking the middle point between the point on which the ship comes up, and the point which she falls off, for the second and third courses, as taught in the rules for lying to, and then allowing, as before, for the variation and lee-way, the traverse table will stand as under.

Now to diff. of lat. 3.8 S. and dep.	MER. PARTS.	44° 8' N. 2957.	44 4 N. 2951	°	
Now to diff.	W. 25 miles.	9.8 Lat, failed from 44° 8' N. Diff, lat, 4 S.	12.8 Lat, in	lat.	12
-	M	-	12	5 32	2
	E.	4.6	3.	7.	
BLE.	S.		27.1	27.1	3.8
E TAI	N.	7.7	8.2	23.3	
TRAVERSE TABLE.	Diff.	16	0 0	1	
T	Courfes	W.N.W. ‡ W.	S. S. W. T. W.		

Note. When there are odd miles in the courfe, as in this day's work, take the degrees next above and below the minutes, and the half of what the meridional difference of latitude gives, at these degrees, will be the difference of longitude.

Therefore, to the course 81° 30' and the mer. diff. lat. 6 miles, the diff. of long. is 40 miles.

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The course and distance to Funchal is found as above.

	representational of the Paper of the Control of the		
H. IK. F. Courfes. Winds. Leeway. Remarks on board, Saturd May 10th.	The first 8 of these 24 hours dead calm and sogy; the rest stiff gales and clear. A current all day setting N. W. by N. one mile per hour. Variation 15 point westerly.	Courfe Diff. Diff. Depar- Lat.by Lat.by Mer. Diff. Long. Bearing and tance Lat. Lure D R Obser. diff. Lon in distance	S 81 oW 94 15 S 93 W 43 40 43 34 34 1 126 10 20 W Dift. 730 miles.
Winds. Leev		epar-Lat.by	3 W 43 49
Courfes.	W.S.W. FW S.	Dif. Diff. Diff. and	611cs 94 15 S 9
H. K. F.	2 40 8 0 2 4 40 8 0 4 2 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 8 6 8 8 2 2 2 4 6 8 6 8 2 2 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Courfe L	Wo 188

The fetting of the current, and its drift in 24 hours, being made a course and distance, as has been raught, and the variation and leeway allowed for, as before, the traverse table and other work will stand as follows.

Now to diff. lat. 14.9 S. and dep. 92.6 W.	W. duft. 94 miles.	44° 4'N. 2951	43 45 N. 203E	Then to the course 819 and mer. diff.	rom 8° 25'W
Now to diff. lat.	the courie 18 5. 81	V Lat. failed from	74.8 Ship's lat.	2.6 Then to the co	Long. failed f
1000	í	E. V	2	10	
	BLE.	Dift N: S E.	31.0	31.0	16.4
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ASSESSES A	TRAVERSE TABLE.	Dift	24	- A	
	T	rles.	W S.W.		

But the latitude by observation differing from the latitude by dead-reckoning, I correct for e true longitude. And, as our last observation was three days ago, I correct a follows. the true longitude.

21 Takes 20

3063 132 3063	8° 2° W 153 W 10 31 W
23' N.	34 N.
Laft obfer, lat. 45° 23' N. Ship's lat. by D. R. 43 49 N. Mer. diff. lat. by D. R. Laft obfer. lat. 45° 23' N.	Ship's lat. by obf. 43. Mer. diff. lat. by obf. Long at laft obfer. Ship's long. by D. R.
obfer. lat slat. by I diff. lat obfer. lat	's lat. by . diff. lat g at laft 's long. b
Laft Ship Mer Laft	Ship Mer Lon Ship

Diff. of long. by D. R.

To mer. diff. lat. by D. R. 132, and diff. long. by D. R. 149, the courfe is 48° 30' diffance 199: And because the course is more than 33°, and lefs than 56°, I correct by Case II.

To the diff. 199, and mer. diff. lat. by obser. 153, the departure is 127. Then 127 added to 149, the sum is 276: half this sum, namely 138, is the true diff. of longitude.

Now long. at last obser.

True diff. long. 138, or

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Ship's true long. - 10 . 0 W. The course and distance from the ship to Funchal is found to be as above.

ceway Remarks on board, Sunday May 11th.	Thefe 24 hours moderate gales with flowers of rain. 10 4 5 8 4 5 10 4 12 4 2 3 5 5 5 10 4 1 1 1 2 3 5 5 10 3 5 10 3 5 10 3 5 10 3 5 10 3 5 10 3 5 10 3 5 10 3 5 10 3 6 5 10 4 6 6 10 5 7 10 6 7 10 7 10 8 10 8 10 9 11 10 W	Course Dif. Diff. Depar-Lat.by Lat.by Mer. Diff. Long. Bearing and distance Lat. ture D.R. Obs. diff. Lon. in distance Miles S 53 30 W 84 50 S 67 W 42 44 48 92 17 52 W Diff. 655 miles.
Winds	S. by E.	bepar- Lat.b ture D.R.
Courfes	2 4 5 W. S. W. S. W. S. W. S. W. S. W. S. W. S. W. S. by E. 12 3 5 S. W. by W. S. by E. 12 3 10 3	Dif. Diff. Lance Lat. Miles So S 6
H. K. F.		Courfe tance Miles S 5 3 50 W 84

In this day's work the swell is to be considered as a current, whose drift, in the 24 hours, is equal to 6 miles, the allowance made for the swell, as it comes from the S. W. it heaves the ship towards the N. E. and the variation allowed upon it makes the last course N. E. by N.

. 07.5 %	Mer.	34 N.	44 N. 2841	•
Now to diff. of la	49.0 w. the course 84 miles.	48.2 Lat, failed from 43° 34' N. 2910 22.6 Diff. lat. 50 S.	Ship'slat.by D.R. 42	Mer diff. lat.
	W.	48.2	70.8	2 2
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LE.	S. E.	32.3	54.8 3.3	<u>د</u> اد
TABLE.	N. S. E.	32-3	5.0 54.8 3.3	
TRAVERSE TABLE.	Diff. N. S. E.	S. W. by W. 58 32.2 48.2 Lat, failed from 43° 34' N. 291 S. W. W. E. by N. 6 5.0 22.6 22.6 Diff. lat. 50 S.	5.0 54.8 3.3	

Then, to the course 53° 30', and the mer. diff. lat. 69 miles, the diff. of long. is

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Long. failed from	-		42	

The course and distance to Funchal is found (by Case I. of Mercator's) as above.

onday May 12th.	gales, and clear	Bearing and diffance	Funchals 12 W
K. F. Courses Winds Leeway Remarks on brard. Monday May 12th.	These 24 hours fresh gales, and elear weather. Variation I point westerly.	Dif. Diff. Depar-Lat.by Lat.by Mer. Diff. Long.	120W 42 44 42 30 648 164 14 30W Diff. 605 miles.
Winds Leeway	who	Dif. Diff. Depar-Lat.by Lat.by Mer. tance Lat ture D. R. Obfer. diff.	20W 42 44 42 30
F. Courfes	5 W.by N. S. W.by S. S. W. 3 W. 3 W. 3 W. 3 W. 3 W. 3 W.		Miles 120
H K.	4 4 4 ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	Courfe	Weft

The variation being allowed upon both courses, and the seeway upon the second it will be found that the ship has sailed all the day due west, or on a parallel; and

by fumming up the distances, her distance is found to be 120 miles, which is also her departure, and she has made no distrence of latitude, consequently, her latitude, by dead reckoning, is the same as yesterday, or 42° 44' N.

As the ship has sailed on a parallel, her disterence of longitude must be found by Parallel Sailing; thus, subtract the lat. 42° 44' from 90° 0', and there remains 47' 16' with this as a course, and the dep. 120 miles, the distance is 164 miles, which is the diff. of long.

Diff. of long. Long. in by D. R.

But the latitude by observation differing from the latitude by D. R. 1 correct for the true longitude. And, as it is two days since the last observation, I work as follows.

37 W 20 W 2910 1+82 88 2910 60 2822 Ship's lat. by D.R. 42 44 N 30 N 43° 34° N Mer. diff. lat. by D. R. Long. at last obf. Ship's long. by D. R. Ship's lat. by obf. 42 Mer. diff. lat, by obf. Laft obf. lat.

and the diff. long. by D. K. 257, the course is 75°, and the diff. 266. And, because the course is more than 56°, I correct by Cafe III. To the dilt, 266, and the mer. diff. lat. by obf. 88, the dep. is 250, the 10° 20 W Now long. at last obf. True diff. long. true diff. of long. Ship's true long. The course and distance are found as per column.

17

257

Diff. long. by D. R.

Fuelday May + 3th.	if gales and showers till path mid- night, from 2 P. M. fair weather and moderate gales. 4 A. M. handed the fore top-fail, riation 1 point westerly.	Bearing and distance	r4 30W Diff. 441 miles.
Winds Leeway Remarks on board, Tuefday May + 3th.	Stiff gales and showers till past midnight, from 2 P. M. fair weather and moderate gales. At 4 A. M. handed the fore top-fail, Variation 1 point westerly.	Course Diff. Diff. Depar Lat.by Lat.by Mer. Diff. Long. Bearing and tance Lat. ture D. R. Obf. diff. Long in distance	B
ds Leeway	.w. ‡ .w.	Lat-by Lat.by	39 45 39 40 6 48
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K. F. Courfes	8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8. 8	urfe Dif- Di	South 170 170 S
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1. S	110 15.7 23.0 Open the ta	164.5 2
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83	S. S. E. F.	

first course and seeway, and variation upon the second, it appears from the traverse table that the ship has, this day, made 164 miles of diff. of lat, southward, and no departure, therefore, her course has been fouth, and her distance, by D. R. 164 miles. As the shas no departure, her longitude

nd mer. distance are the same as yesterday, and to find the latitude,

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But as, by observation, the ship is found to be in latitude 39° 40° N. it is evident she has got 6 miles a head of the D. R. which 6 miles being added to the distance by D. R. the true course, difference of latitude, and longitude in, will be as in their respective columns.

The course and distance from the ship to Funchal are found to be as in their re-

A A Mand Mill

y 14th.	6 5 6 4 A A	100 0 5 H	ring and flance ils.r6°33'W
duef. Markt. tours.	a a ma	r e	Bearing and diffance Funchals. 16"33" Dift. 248 mile
oard, Words thefe		Wed.	Long.
Remarks on board, Wed Hard gales for thefe 24 Handed both top-fails.	(C) (C)	Variation & point westerly.	iff. Lon.
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found to be latitude 35° 46' N. which differs from the latitude by D. R. 6 miles; and, fince I had an observation yesterday, and that the course sound by D. R. is more than 56°, I, therefore, correct by Case III. for a single day.

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Courses Winds Leeway Remarks on board, Friday May 16th.	Thefe 24 hours moderate gales, and fair weather.	Dif. Diff. Depar-Lat.by Lat. by Mer. Diff. Long. Bearing and tance Lat. ture D. R. Obfer. diff. Long. diffance Miles 136 8 14 95 16 19 W Diff. 88 miles.
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fering 5 miles from the latitude by D. R. and that the course, by D. R. is more than 33°; and less than 56°, I correct for the true course, distance, departure, and difference of longitude by Case II.

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To dift. 133, and proper diff. lat. 110, the dep. is 75.3 miles; then, 75.3 added to 81.7, the lum is 157; half this fum is 78.5, which is the true departure. Then, to this true departure, 78.5, and proper diff. lat. by obf. 110, the course is 8. 35. 30 E. diffance, 135 miles: And, to the course 35° 30' and the mer. diff. lat. 134. the diff. long. in at laft obf.

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MINE SE

H. K. F. Courfes Winds Leeway Remarks on board, Saturd. May 12th.	Thefe 24 hours brilk gules, and for the most part foggy.	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	faw Funchal bearing S. S. W. 4 W.	4 O IV	Variation 3 point wefterly.
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Having, in the preceding Journal, shewn how to find what latitude and longitude the ship is in on any day, I shall, in the next place, how

Laistude and Longitude in, to prick off the place of the Ship

Lay a scale across the chart in the latitude your ship is in, and draw a line with a black lead pencil, then lay the scale a-cross the longitude the ship is in, to cut the sormer line at right angles, the point of interfection-will be the ship's place required.

But this will only do when the longitude marked on the chart, and your reckoning of longitude in, are both counted from the same meridian; therefore, for a general rule, take the following:

By the Longitude and Latitude made, to mark off the Ship's Place.

R. U. E. E.

from where that line falls upon the equinoctial, or line marked with the degrees of longitude, fet off that distance the fame way as the place lies from it (that is, to the right-hand, if the place lye to the right-hand of the north and south line, or to the left-hand, if it lye to the left) and make a mark with a black-lead pencil; this mark will ferve to mark off by, until you come to take a new departure, and Set one foot of your compasses in the place you take your departure from, and take the nearest distance to some north and south line, and then you rub it out, and make a new one, as before.

Then lay a ruler a-cross the chart in the latitude you are in, and taking so many degrees in your compasses (from the line of longitude) as your longitude made comes to, fet them off from your black lead mark, to the eastward, if the longitude made be east, or to the west-ward, if it be west; where this falls will be the longitude the ship is in by the chart, from which take the nearest distance to some north and south line, and from where that line, &c. as in the first case.

EXAMPLE.

Required the ship's place on the chart when her latitude is 39° 40' N. and longitude 14° 30' W.

Lay a scale from 39° 40' on the right-hand side of the chart to the same degrees on the left-hand side, and draw a line; then lay the fcale on the given longitude, 14° ‡, at the top and bottom of the chart, the point of interfection (B) will be the ship's place.

A place being given on the Chart to find its latitude and longitude.

With a pair of compasses, take the nearest distance between the given places and the nearest parallel of latitude; this distance applied to the graduated meridian, from the faid parallel the fame way the place lies, will give the latitude fought.

Thus, the distance from St. Mary's to the parallel of 40° applied from 40°, fouthward, gives 37° o' North, for the latitude fought. In like manner, the shortest distance taken between the given place

and the nearest meridian, being applied to the equator, or longitude line, from the faid meridian the fame way the place lies, will shew the

longitude required.

Thus, the diltance from St. Mary's, to the parallel through 20°, applied from 20 westward, will give 25° west longitude.

To find the Course, or Bearing, from one Place to another.

this position slide one point along the ruler, and observe what point of Lay a ruler on the two given places, and take the nearest distance the compass the other comes nearest to, which will be the bearing refrom the centre of any compass on the chart to the ruler's edge, in

I demand the course from the Lizard to the island of Madeira?

flide the compasses along by the ruler, keeping one foot perpendicular to it, and it sheweth among the rhumbs the course to be S. S. W. # W. Laying a ruler's edge on the Lizard and Madeira, take the nearest distance from the centre of a compass to the edge of the ruler, then

from the Lizard to Madeira, and the opposite course, viz. N. N. E. & E. is the course from the island of Madeira to the Lizard.

To find the Distance of any two Places in the Chart.

In this problem are four Cafes.

CASE

Two places under one meridian (that is, differing only in latitude) being given, to find their diftance.

Find the difference of latitude between the two given places and it is the distance fought.

CASE IL

Two places in the equator being given to find their distance.

R U L E.

Find the difference of longitude between them, and it is the dif-

CASE INTE

Two places in one parallel (that is, differing only in longitude) being given to find their diffance.

Take half the distance between the two places in the compasses, and set one foot in the latitude of the place, and apply the other foot upwards and downwards on the same meridian; observe the degrees of latitude the said point falls upon: then the difference of these latitudes will be the distance fought.

EXAMPLE.

I demand the distance from the island of Madeira to the island of

Bermudas, both being nearly in latitude 32° ± N. Half the distance between Madeira and Bermudas will reach from latitude 32° ±, to about 49° 40' above, and to 10° 40' below, the difference of these is 39°, or 2340 miles, the distance required.

195 J

C A S E IV. Two places differing both in latitude and longitude being given, to find their distance.

latitude in degrees and miles from the equator, or graduated parallel, lay the edge of a ruler over the two places, apply that distance so to faid ruler's edge, then take the distance along the edge of the ruler, from the place where the compasses rested, to the place where the Find the latitudes of the two places, and take their difference of the ruler's edge, that, when one foot is placed close to the ruler, and the other, pointing directly north or south (that is, parallel to one of the meridians) may just touch some cast and west line, crossed by the ruler croffed the faid east and west line, that distance measured on the equator, or degrees of longitude, will give the distance required.

EXAMP

I demand the distance from the island Madeira to the Lizard? 40 N. Lizard's latitude

Madeira's latitude

parallel, and laying a ruler on both places, apply one foot of the compasses so to the ruler's edge, that the other, pointing north, may touch an east and west line crossed by the ruler (in E) then the diffeance, by the ruler's edge, from the place where the compasses rested Then take their difference 17° 17' from the equator, or graduated (in D) to the place where the ruler croffed the aforefaid eaft and weft line, meafured on the equator, or graduated parallel, is about 19° 4, or 1160 miles, which is nearly the distance between the two places. Their difference

I demand the course and distance from the island St. Marg's,

latitude 37° o' N. longituue 25° 6' W. to the island Barbadoes, in latitude 13° 5' N. longitude 59° 59' W.?

By taking the difference of latitude between the two places, and applying the scale, as in the preceding example, the course from the island St. Mary's, to the island Barbadoes, is found to be S. W. & W. distance 39°, or 2340 miles.

The peak in human of the Change of the State Series S

102

Page 104, line 1, for 1789, read 1787.

Page 136, long. of Rouen, for W. read E.

Page 141, long. of Dantzic, for 17° 36, read 18° 36'.

Ibid. line 13, for Reardy, read Picardy.

Page 182, line 7 from bottom, for 2035 5, read 203.5.

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